

## Bescheid

über die Änderung der  
allgemeinen bauaufsichtlichen Zulassung  
vom 15. September 2008

Zulassungsstelle für Bauproducte und Bauarten

Bautechnisches Prüfamt

Eine vom Bund und den Ländern  
gemeinsam getragene Anstalt des öffentlichen Rechts

Mitglied der EOTA, der UEAtc und der WFTAO

Datum: Geschäftszichen:

25.11.2011 I 36-1.14.1-95/11

**Zulassungsnummer:**  
**Z-14.1-537**

**Geltungsdauer**  
vom: **25. November 2011**  
bis: **30. September 2013**

**Antragsteller:**  
**Gesamtverband der Aluminiumindustrie e.V.**  
Am Bonneshof 5  
40474 Düsseldorf

**Zulassungsgegenstand:**  
**Mechanische Verbindungselemente zur Verbindung von Bauteilen aus Aluminium miteinander  
oder mit Unterkonstruktionen aus Aluminium, Stahl oder Holz**

Dieser Bescheid ändert und ergänzt die allgemeine bauaufsichtliche Zulassung Nr. Z-14.1-537 vom 15. September 2008, geändert und ergänzt durch Bescheide vom 12. Januar 2009, 17. Februar 2010 und 12. August 2011.

Dieser Bescheid umfasst zwei Seiten und acht Anlagen. Er gilt nur in Verbindung mit der oben genannten allgemeinen bauaufsichtlichen Zulassung und darf nur zusammen mit dieser verwendet werden.



**Bescheid über die Änderung der  
allgemeinen bauaufsichtlichen Zulassung**

Nr. Z-14.1-537

Seite 2 von 2 | 25. November 2011

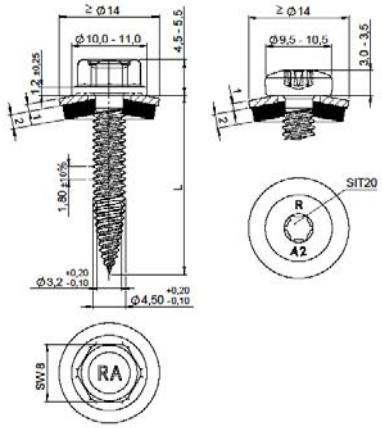
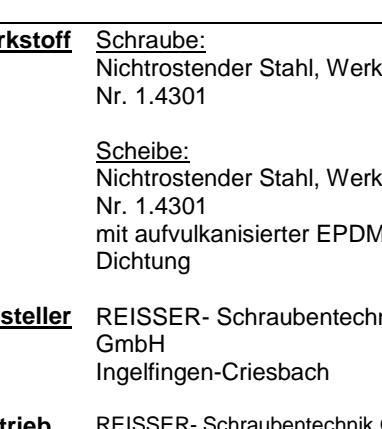
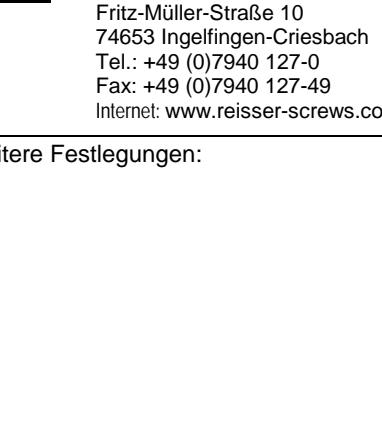
**ZU II BESONDERE BESTIMMUNGEN**

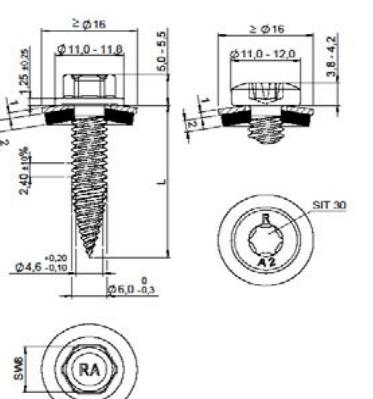
Die Besonderen Bestimmungen der allgemeinen bauaufsichtlichen Zulassung werden wie folgt geändert und ergänzt:

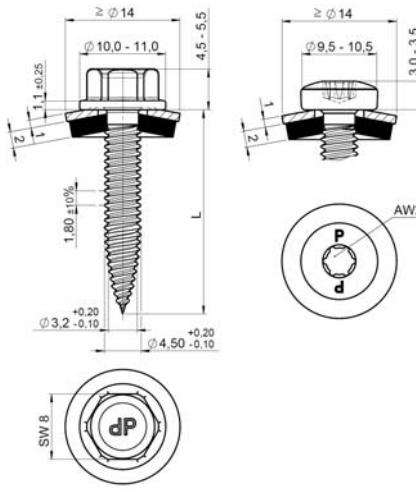
1. Die Anlagen 3.1.30, 3.1.31, 3.2.21 und 3.2.22 werden durch die Anlagen 3.1.30a, 3.1.31a, 3.2.21a und 3.2.22a ersetzt.
3. Die Anlagen werden um die Anlagen 3.1.32, 3.1.33, 3.2.23 und 3.2.24 ergänzt.

Georg Feistel  
Abteilungsleiter

Begläubigt

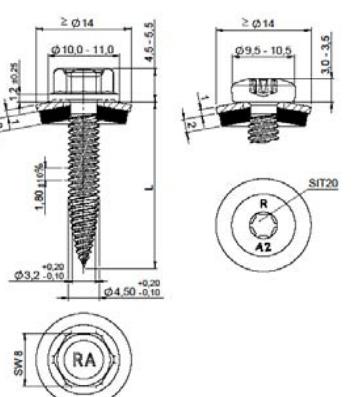
| Bohrschauben |                   |    | Max. Bohrleistung $\Sigma t_i$<br>3,20 mm | Bauteil II: $t_{II}$ in [mm]<br>Aluminium mit Zugfestigkeit $R_m \geq 165 \text{ N/mm}^2$ |      |      |      |      |      |      |      |      |                                      | Bauteil II aus Holz Sortierkl. $\geq \text{S10}$ |
|--------------|-------------------|---|---|---|------|------|------|------|------|------|------|------|--------------------------------------|--|
|              |                   |   |   | 0,50  | 0,60 | 0,70 | 0,80 | 0,90 | 1,00 | 1,20 | 1,50 | 2,00 | Versagen von Bauteil I (Lochleibung) | Versagen von Bauteil II siehe Abs. 3.2.3         |
|              | <b>Werkstoff</b>  | Schraube:<br>Nichtrostender Stahl, Werkstoff-Nr. 1.4301   | 0,5                                       | 0,39  | —    | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39 | —                                    | 0,39   |
|              |                   | Scheibe:<br>Nichtrostender Stahl, Werkstoff-Nr. 1.4301<br>mit aufvulkanisierter EPDM-Dichtung   | 0,6                                       | 0,39  | —    | 0,55 | —    | 0,55 | —    | 0,55 | —    | 0,55 | —                                    | 0,55   |
|              | <b>Hersteller</b> | REISSER- Schraubentechnik GmbH<br>Ingelfingen-Criesbach   | 0,7                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,72 | —    | 0,72 | —                                    | 0,72   |
|              |                   | REISSER- Schraubentechnik GmbH<br>Fritz-Müller-Straße 10<br>74653 Ingelfingen-Criesbach<br>Tel.: +49 (0)7940 127-0<br>Fax: +49 (0)7940 127-49<br>Internet: <a href="http://www.reisser-screws.com">www.reisser-screws.com</a> | 0,8                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 0,88 | —                                    | 0,88   |
|              | <b>Vertrieb</b>   | Weitere Festlegungen:   | 0,9                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   | Anlage 3.1.30a<br>zur allgemeinen<br>bauaufsichtlichen<br>Zulassung Nr. Z-14.1-537<br>vom 25. November 2011   | 1,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |    | 1,2                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,5                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 2,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 0,5                                       | 0,39  | —    | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39 | —                                    | 0,39   |
|              |                   |    | 0,6                                       | 0,39  | —    | 0,55 | —    | 0,55 | —    | 0,55 | —    | 0,55 | —                                    | 0,55   |
|              |                   |   | 0,7                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,72 | —    | 0,72 | —                                    | 0,72   |
|              |                   |  | 0,8                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 0,88 | —                                    | 0,88   |
|              |                   |   | 0,9                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 1,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,2                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 1,5                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 2,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 0,5                                       | 0,39  | —    | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39 | —                                    | 0,39   |
|              |                   |   | 0,6                                       | 0,39  | —    | 0,55 | —    | 0,55 | —    | 0,55 | —    | 0,55 | —                                    | 0,55   |
|              |                   |  | 0,7                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,72 | —    | 0,72 | —                                    | 0,72   |
|              |                   |   | 0,8                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 0,88 | —                                    | 0,88   |
|              |                   |  | 0,9                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 1,2                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,5                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 2,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 0,5                                       | 0,39  | —    | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39 | —                                    | 0,39   |
|              |                   |  | 0,6                                       | 0,39  | —    | 0,55 | —    | 0,55 | —    | 0,55 | —    | 0,55 | —                                    | 0,55   |
|              |                   |   | 0,7                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,72 | —    | 0,72 | —                                    | 0,72   |
|              |                   |  | 0,8                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 0,88 | —                                    | 0,88   |
|              |                   |   | 0,9                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 1,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,2                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 1,5                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 2,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 0,5                                       | 0,39  | —    | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39 | —                                    | 0,39   |
|              |                   |   | 0,6                                       | 0,39  | —    | 0,55 | —    | 0,55 | —    | 0,55 | —    | 0,55 | —                                    | 0,55   |
|              |                   |  | 0,7                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,72 | —    | 0,72 | —                                    | 0,72   |
|              |                   |   | 0,8                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 0,88 | —                                    | 0,88   |
|              |                   |  | 0,9                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 1,2                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,5                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |  | 2,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 0,5                                       | 0,39  | —    | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39 | —                                    | 0,39   |
|              |                   |   | 0,6                                       | 0,39  | —    | 0,55 | —    | 0,55 | —    | 0,55 | —    | 0,55 | —                                    | 0,55   |
|              |                   |   | 0,7                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,72 | —    | 0,72 | —                                    | 0,72   |
|              |                   |   | 0,8                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 0,88 | —                                    | 0,88   |
|              |                   |   | 0,9                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,2                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 1,5                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 2,0                                       | 0,39  | —    | 0,55 | —    | 0,72 | —    | 0,88 | —    | 1,28 | —                                    | 1,28   |
|              |                   |   | 0,5                                       | 0,39  |      |      |      |      |      |      |      |      |                                      |  |

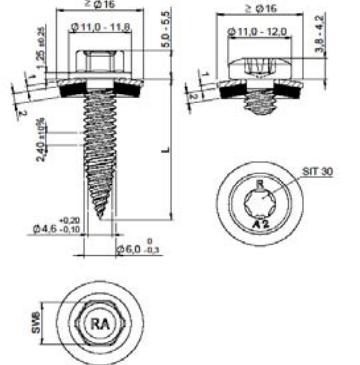
| Bohrschauben  |      | Werkstoff                    | Schraube:<br>Nichtrostender Stahl, Werkstoff-Nr. 1.4301<br><br>Scheibe:<br>Nichtrostender Stahl, Werkstoff-Nr. 1.4301 mit aufvulkanisierter EPDM-Dichtung | Hersteller | REISSER- Schraubentechnik GmbH<br>Ingelfingen-Criesbach | Vertrieb | REISSER- Schraubentechnik GmbH<br>Fritz-Müller-Straße 10<br>74653 Ingelfingen-Criesbach<br>Tel.: +49 (0)7940 127-0<br>Fax: +49 (0)7940 127-49<br>Internet: www.reisser-screws.com | Weitere Festlegungen: | Max. Bohrleistung $\Sigma t_i$<br>3,50 mm | Bauteil II: $t_{II}$ in [mm]<br>Aluminium mit Zugfestigkeit $R_m \geq 165 \text{ N/mm}^2$ |      |  |      |      |      |      |      |                                      |                                       | Bauteil II aus Holz Sortierkl. $\geq S10$ |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
|---|------|------------------------------|---|------------|---|----------|---|-----------------------|---|---|------|--|------|------|------|------|------|--------------------------------------|---------------------------------------|---|---|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|--------|-----|------|---|------|---|------|---|------|---|--------|-----|------|---|------|---|------|---|------|---|--------|-----|------|---|------|---|------|---|------|---|--------|--|------|------|------|------|------|------|------|------|------|
|   |      |                              |   |            |   |          |   |                       | 0,50                                      | 0,60  | 0,70 | 0,80   | 0,90 | 1,00 | 1,20 | 1,50 | 2,00 | Versagen von Bauteil I (Lochleibung) | Versagen von Bauteil II (Lochleibung) | Bauteil II aus Holz Sortierkl. $\geq S10$ |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
|  <p>Max. Bohrleistung <math>\Sigma t_i</math><br/>3,50 mm</p> <table border="1"> <thead> <tr> <th>Bauteil II: <math>t_{II}</math> in [mm]</th> <th>0,50</th> <th>0,60</th> <th>0,70</th> <th>0,80</th> <th>0,90</th> <th>1,00</th> <th>1,20</th> <th>1,50</th> <th>2,00</th> </tr> </thead> <tbody> <tr> <td>Zugfestigkeit <math>R_m \geq 165 \text{ N/mm}^2</math> Aluminium mit <math>t_{II} \leq 165 \text{ N/mm}^2</math></td> <td>0,5</td> <td>0,63</td> <td>—</td> <td>0,63</td> <td>—</td> <td>0,63</td> <td>—</td> <td>0,63</td> <td>—</td> </tr> <tr> <td>0,6</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,77</td> </tr> <tr> <td>0,7</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,90</td> <td>—</td> <td>0,90</td> <td>—</td> <td>0,90</td> </tr> <tr> <td>0,8</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,90</td> <td>—</td> <td>1,04</td> <td>—</td> <td>1,04</td> </tr> <tr> <td>0,9</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,90</td> <td>—</td> <td>1,36</td> <td>—</td> <td>1,36</td> </tr> <tr> <td>1,0</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,90</td> <td>—</td> <td>1,36</td> <td>—</td> <td>1,68 a</td> </tr> <tr> <td>1,2</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,90</td> <td>—</td> <td>1,36</td> <td>—</td> <td>1,68 a</td> </tr> <tr> <td>1,5</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,90</td> <td>—</td> <td>1,36</td> <td>—</td> <td>1,94 a</td> </tr> <tr> <td>2,0</td> <td>0,63</td> <td>—</td> <td>0,77</td> <td>—</td> <td>0,90</td> <td>—</td> <td>1,36</td> <td>—</td> <td>1,94 a</td> </tr> </tbody> </table> <p>Drehmoment <math>V_{R,k}</math> in [kNm]</p> <table border="1"> <thead> <tr> <th>Auszugs-Auswirkungskraft <math>N_{R,k}</math> in [kN]</th> <th>0,39</th> <th>0,51</th> <th>0,64</th> <th>0,76</th> <th>0,85</th> <th>0,94</th> <th>1,13</th> <th>1,49</th> <th>1,49</th> </tr> </thead> </table> |      | Bauteil II: $t_{II}$ in [mm] | 0,50  | 0,60       | 0,70  | 0,80     | 0,90  | 1,00                  | 1,20                                      | 1,50  | 2,00 | Zugfestigkeit $R_m \geq 165 \text{ N/mm}^2$ Aluminium mit $t_{II} \leq 165 \text{ N/mm}^2$ | 0,5  | 0,63 | —    | 0,63 | —    | 0,63                                 | —                                     | 0,63                                      | — | 0,6 | 0,63 | — | 0,77 | — | 0,77 | — | 0,77 | — | 0,77 | 0,7 | 0,63 | — | 0,77 | — | 0,90 | — | 0,90 | — | 0,90 | 0,8 | 0,63 | — | 0,77 | — | 0,90 | — | 1,04 | — | 1,04 | 0,9 | 0,63 | — | 0,77 | — | 0,90 | — | 1,36 | — | 1,36 | 1,0 | 0,63 | — | 0,77 | — | 0,90 | — | 1,36 | — | 1,68 a | 1,2 | 0,63 | — | 0,77 | — | 0,90 | — | 1,36 | — | 1,68 a | 1,5 | 0,63 | — | 0,77 | — | 0,90 | — | 1,36 | — | 1,94 a | 2,0 | 0,63 | — | 0,77 | — | 0,90 | — | 1,36 | — | 1,94 a | Auszugs-Auswirkungskraft $N_{R,k}$ in [kN] | 0,39 | 0,51 | 0,64 | 0,76 | 0,85 | 0,94 | 1,13 | 1,49 | 1,49 |
| Bauteil II: $t_{II}$ in [mm]  | 0,50 | 0,60                         | 0,70  | 0,80       | 0,90  | 1,00     | 1,20  | 1,50                  | 2,00                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| Zugfestigkeit $R_m \geq 165 \text{ N/mm}^2$ Aluminium mit $t_{II} \leq 165 \text{ N/mm}^2$  | 0,5  | 0,63                         | —   | 0,63       | —   | 0,63     | —   | 0,63                  | —   |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,6   | 0,63 | —                            | 0,77  | —          | 0,77  | —        | 0,77  | —                     | 0,77                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,7   | 0,63 | —                            | 0,77  | —          | 0,90  | —        | 0,90  | —                     | 0,90                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,8   | 0,63 | —                            | 0,77  | —          | 0,90  | —        | 1,04  | —                     | 1,04                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,9   | 0,63 | —                            | 0,77  | —          | 0,90  | —        | 1,36  | —                     | 1,36                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 1,0   | 0,63 | —                            | 0,77  | —          | 0,90  | —        | 1,36  | —                     | 1,68 a                                    |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 1,2   | 0,63 | —                            | 0,77  | —          | 0,90  | —        | 1,36  | —                     | 1,68 a                                    |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 1,5   | 0,63 | —                            | 0,77  | —          | 0,90  | —        | 1,36  | —                     | 1,94 a                                    |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 2,0   | 0,63 | —                            | 0,77  | —          | 0,90  | —        | 1,36  | —                     | 1,94 a                                    |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| Auszugs-Auswirkungskraft $N_{R,k}$ in [kN]  | 0,39 | 0,51                         | 0,64  | 0,76       | 0,85  | 0,94     | 1,13  | 1,49                  | 1,49                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| <p>Charakteristische Tragfähigkeitswerte für das Verbindungsselement RP – T2 – 6,0 x L</p> <table border="1"> <thead> <tr> <th>Bauteil II: <math>t_{II}</math> in [mm]</th> <th>0,50</th> <th>0,60</th> <th>0,70</th> <th>0,80</th> <th>0,90</th> <th>1,00</th> <th>1,20</th> <th>1,50</th> <th>2,00</th> </tr> </thead> <tbody> <tr> <td>Zugfestigkeit <math>R_m \geq 215 \text{ N/mm}^2</math> Aluminium mit <math>t_{II} \leq 215 \text{ N/mm}^2</math></td> <td>0,5</td> <td>0,82</td> <td>—</td> <td>0,82</td> <td>—</td> <td>0,82</td> <td>—</td> <td>0,82</td> <td>—</td> </tr> <tr> <td>0,6</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,00</td> </tr> <tr> <td>0,7</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,18</td> </tr> <tr> <td>0,8</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,36</td> <td>—</td> <td>1,36</td> </tr> <tr> <td>0,9</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,36</td> <td>—</td> <td>1,36</td> </tr> <tr> <td>1,0</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,78</td> <td>—</td> <td>1,78</td> </tr> <tr> <td>1,2</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,78</td> <td>—</td> <td>2,53 a</td> </tr> <tr> <td>1,5</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,78</td> <td>—</td> <td>3,05 a</td> </tr> <tr> <td>2,0</td> <td>0,82</td> <td>—</td> <td>1,00</td> <td>—</td> <td>1,18</td> <td>—</td> <td>1,78</td> <td>—</td> <td>3,05 a</td> </tr> </tbody> </table> <p>Drehmoment <math>V_{R,k}</math> in [kNm]</p> <table border="1"> <thead> <tr> <th>Auszugs-Auswirkungskraft <math>N_{R,k}</math> in [kN]</th> <th>0,51</th> <th>0,67</th> <th>0,83</th> <th>0,99</th> <th>1,11</th> <th>1,22</th> <th>1,47</th> <th>1,95</th> <th>1,95</th> </tr> </thead> </table>   |      | Bauteil II: $t_{II}$ in [mm] | 0,50  | 0,60       | 0,70  | 0,80     | 0,90  | 1,00                  | 1,20                                      | 1,50  | 2,00 | Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ Aluminium mit $t_{II} \leq 215 \text{ N/mm}^2$ | 0,5  | 0,82 | —    | 0,82 | —    | 0,82                                 | —                                     | 0,82                                      | — | 0,6 | 0,82 | — | 1,00 | — | 1,00 | — | 1,00 | — | 1,00 | 0,7 | 0,82 | — | 1,00 | — | 1,18 | — | 1,18 | — | 1,18 | 0,8 | 0,82 | — | 1,00 | — | 1,18 | — | 1,36 | — | 1,36 | 0,9 | 0,82 | — | 1,00 | — | 1,18 | — | 1,36 | — | 1,36 | 1,0 | 0,82 | — | 1,00 | — | 1,18 | — | 1,78 | — | 1,78   | 1,2 | 0,82 | — | 1,00 | — | 1,18 | — | 1,78 | — | 2,53 a | 1,5 | 0,82 | — | 1,00 | — | 1,18 | — | 1,78 | — | 3,05 a | 2,0 | 0,82 | — | 1,00 | — | 1,18 | — | 1,78 | — | 3,05 a | Auszugs-Auswirkungskraft $N_{R,k}$ in [kN] | 0,51 | 0,67 | 0,83 | 0,99 | 1,11 | 1,22 | 1,47 | 1,95 | 1,95 |
| Bauteil II: $t_{II}$ in [mm]  | 0,50 | 0,60                         | 0,70  | 0,80       | 0,90  | 1,00     | 1,20  | 1,50                  | 2,00                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ Aluminium mit $t_{II} \leq 215 \text{ N/mm}^2$  | 0,5  | 0,82                         | —   | 0,82       | —   | 0,82     | —   | 0,82                  | —   |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,6   | 0,82 | —                            | 1,00  | —          | 1,00  | —        | 1,00  | —                     | 1,00                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,7   | 0,82 | —                            | 1,00  | —          | 1,18  | —        | 1,18  | —                     | 1,18                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,8   | 0,82 | —                            | 1,00  | —          | 1,18  | —        | 1,36  | —                     | 1,36                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 0,9   | 0,82 | —                            | 1,00  | —          | 1,18  | —        | 1,36  | —                     | 1,36                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 1,0   | 0,82 | —                            | 1,00  | —          | 1,18  | —        | 1,78  | —                     | 1,78                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 1,2   | 0,82 | —                            | 1,00  | —          | 1,18  | —        | 1,78  | —                     | 2,53 a                                    |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 1,5   | 0,82 | —                            | 1,00  | —          | 1,18  | —        | 1,78  | —                     | 3,05 a                                    |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| 2,0   | 0,82 | —                            | 1,00  | —          | 1,18  | —        | 1,78  | —                     | 3,05 a                                    |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| Auszugs-Auswirkungskraft $N_{R,k}$ in [kN]  | 0,51 | 0,67                         | 0,83  | 0,99       | 1,11  | 1,22     | 1,47  | 1,95                  | 1,95                                      |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |
| <p>Anlage 3.1.31 a<br/>zur allgemeinen<br/>bauaufsichtlichen Zulassung<br/>Nr. Z-14.1-537<br/>vom 25. November 2011</p>   |      |                              |   |            |   |          |   |                       |   |   |      |  |      |      |      |      |      |                                      |                                       |   |   |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |     |      |   |      |   |      |   |      |   |        |  |      |      |      |      |      |      |      |      |      |

| Bohrschauben                             | <b>Werkstoff</b><br>Schraube:<br>Nichtrostender Stahl, Werkstoff-Nr. 1.4301<br><br>Scheibe:<br>Nichtrostender Stahl, Werkstoff-Nr. 1.4301 mit aufvulkanisierter EPDM-Dichtung<br><br><b>Hersteller</b> Würth Group<br>Reinhold Würth Straße 12 – 17<br>D- 74653 Künzelsau<br><br><b>Vertrieb</b> Adolf Würth GmbH & Co. KG<br>Postfach<br>D-74650 Künzelsau<br>Tel.: +49 (0) 7940 15 – 0<br>Fax.: +49 (0) 7940 15 – 1000<br>Internet: <a href="http://www.wuerth.de">www.wuerth.de</a> |  <p>Max. Bohrleistung <math>\Sigma t_i</math> in [mm]<br/>3,20 mm</p> <p>Bauteil II: <math>t_{ii}</math> in [mm] Aluminium mit Zugfestigkeit <math>R_m \geq 165 \text{ N/mm}^2</math></p> <table border="1"> <thead> <tr> <th><math>t_{ii}</math> in [mm]</th> <th>0,50</th> <th>0,60</th> <th>0,70</th> <th>0,80</th> <th>0,90</th> <th>1,00</th> <th>1,20</th> <th>1,50</th> <th>2,00</th> </tr> </thead> <tbody> <tr><td>0,5</td><td>0,39</td><td>—</td><td>0,39</td><td>—</td><td>0,39</td><td>—</td><td>0,39</td><td>—</td><td>0,39</td></tr> <tr><td>0,6</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,55</td><td>—</td><td>0,55</td><td>—</td><td>0,55</td></tr> <tr><td>0,7</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,72</td><td>—</td><td>0,72</td><td>—</td><td>0,72</td></tr> <tr><td>0,8</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,72</td><td>—</td><td>0,88</td><td>—</td><td>0,88</td></tr> <tr><td>0,9</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,72</td><td>—</td><td>0,88</td><td>—</td><td>1,00</td></tr> <tr><td>1,0</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,72</td><td>—</td><td>0,88</td><td>—</td><td>1,20</td></tr> <tr><td>1,2</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,72</td><td>—</td><td>0,88</td><td>—</td><td>1,50</td></tr> <tr><td>1,5</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,72</td><td>—</td><td>0,88</td><td>—</td><td>2,00</td></tr> <tr><td>2,0</td><td>0,39</td><td>—</td><td>0,55</td><td>—</td><td>0,72</td><td>—</td><td>0,88</td><td>—</td><td>—</td></tr> </tbody> </table> <p>Auswirkung Querkraft <math>V_{Rd,i}</math> in [kN]</p> | $t_{ii}$ in [mm] | 0,50 | 0,60 | 0,70 | 0,80 | 0,90 | 1,00 | 1,20 | 1,50 | 2,00 | 0,5 | 0,39 | — | 0,39 | — | 0,39 | — | 0,39 | — | 0,39 | 0,6 | 0,39 | — | 0,55 | — | 0,55 | — | 0,55 | — | 0,55 | 0,7 | 0,39 | — | 0,55 | — | 0,72 | — | 0,72 | — | 0,72 | 0,8 | 0,39 | — | 0,55 | — | 0,72 | — | 0,88 | — | 0,88 | 0,9 | 0,39 | — | 0,55 | — | 0,72 | — | 0,88 | — | 1,00 | 1,0 | 0,39 | — | 0,55 | — | 0,72 | — | 0,88 | — | 1,20 | 1,2 | 0,39 | — | 0,55 | — | 0,72 | — | 0,88 | — | 1,50 | 1,5 | 0,39 | — | 0,55 | — | 0,72 | — | 0,88 | — | 2,00 | 2,0 | 0,39 | — | 0,55 | — | 0,72 | — | 0,88 | — | — | Versagen von Bauteil I (Lochreibung) |  |  |  |  |  |  |  |  |  |
|--|--|--|------------------|------|------|------|------|------|------|------|------|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|------|-----|------|---|------|---|------|---|------|---|---|--------------------------------------|--|--|--|--|--|--|--|--|--|
| $t_{ii}$ in [mm]                         | 0,50   | 0,60   | 0,70             | 0,80 | 0,90 | 1,00 | 1,20 | 1,50 | 2,00 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 0,5                                      | 0,39   | —  | 0,39             | —    | 0,39 | —    | 0,39 | —    | 0,39 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 0,6                                      | 0,39   | —  | 0,55             | —    | 0,55 | —    | 0,55 | —    | 0,55 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 0,7                                      | 0,39   | —  | 0,55             | —    | 0,72 | —    | 0,72 | —    | 0,72 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 0,8                                      | 0,39   | —  | 0,55             | —    | 0,72 | —    | 0,88 | —    | 0,88 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 0,9                                      | 0,39   | —  | 0,55             | —    | 0,72 | —    | 0,88 | —    | 1,00 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 1,0                                      | 0,39   | —  | 0,55             | —    | 0,72 | —    | 0,88 | —    | 1,20 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 1,2                                      | 0,39   | —  | 0,55             | —    | 0,72 | —    | 0,88 | —    | 1,50 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 1,5                                      | 0,39   | —  | 0,55             | —    | 0,72 | —    | 0,88 | —    | 2,00 |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| 2,0                                      | 0,39   | —  | 0,55             | —    | 0,72 | —    | 0,88 | —    | —    |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
|  |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |
| Versagen von Bauteil II siehe Abs. 3.2.3 |  |  |                  |      |      |      |      |      |      |      |      |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |      |     |      |   |      |   |      |   |      |   |   |                                      |  |  |  |  |  |  |  |  |  |

Anlage 3.1.32  
 zur allgemeinen bauaufsichtlichen  
 Zulassung Nr. Z-14.1-537  
 vom 25. November 2011



| Bohrschauben  | Werkstoff Schraube:<br>Nichtrostender Stahl,<br>Werkstoff-Nr. 1.4301<br><br>Scheibe:<br>Nichtrostender Stahl,<br>Werkstoff-Nr. 1.4301<br>mit aufvulkanisierter<br>EPDM-Dichtung  |    | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,00 mm   | <b>Bauteil II: <math>t_{ii}</math> in [mm]</b><br>S235 nach DIN EN 10025-1, S280GD oder S320GD nach DIN EN 10346 |      |      |      |      |      |      |      |      |      | <b>Bauteil II aus Holz Sortierkl. <math>\geq S10</math></b> |      |   |
|---|--|---|---|--|------|------|------|------|------|------|------|------|------|---|------|---|
|   |  |   |   | 0,50   | 0,55 | 0,63 | 0,75 | 0,88 | 1,00 | 1,13 | 1,25 | 1,50 | 2,00 | Versagen von Bauteil I (Lochleibung)                        |      |   |
| <b>Charakteristische Tragfähigkeitswerte<br/>für das Verbindungselement</b><br><br><b>RP – T2 – 4,5 x L</b> | <b>Hersteller</b> REISSER-<br>Schraubentechnik GmbH<br>Ingelfingen-Criesbach<br><br><b>Vertrieb</b> REISSER- Schraubentechnik<br>GmbH<br>Fritz-Müller-Straße 10<br>74653 Ingelfingen-Criesbach<br>Tel.: +49 (0)7940 127-0<br>Fax: +49 (0)7940 127-49<br>Internet: www.reisser-<br>screws.com |    | <b>Querkraft <math>V_{R,k}</math> in [kN]</b>                 | <b>Bauteil I: <math>t_i</math> in [mm]</b> , Aluminium mit<br>Zugfestigkeit $R_m \geq 165 \text{ N/mm}^2$        | 0,50 | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39 | —    | 0,39  | —    | <b>Bauteil II aus Holz Sortierkl. <math>\geq S10</math></b> |
|   |  |   | <b>Auszugs-<br/>kraft <math>N_{R,ii,k}</math> in<br/>[kN]</b> | 0,60   | 0,39 | —    | 0,47 | —    | 0,55 | —    | 0,55 | —    | 0,55 | —   | 0,55 | —   |
| <b>Charakteristische Tragfähigkeitswerte<br/>für das Verbindungselement</b><br><br><b>RP – T2 – 4,5 x L</b> | Weitere Festlegungen:  |   | <b>Querkraft <math>V_{R,k}</math> in [kN]</b>                 | <b>Bauteil I: <math>t_i</math> in [mm]</b> , Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$        | 0,50 | 0,50 | —    | 0,50 | —    | 0,50 | —    | 0,50 | —    | 0,50  | —    | <b>Bauteil II aus Holz Sortierkl. <math>\geq S10</math></b> |
|   |  |   | <b>Auszugs-<br/>kraft <math>N_{R,ii,k}</math> in<br/>[kN]</b> | 0,60   | 0,50 | —    | 0,61 | —    | 0,71 | —    | 0,71 | —    | 0,71 | —   | 0,71 | —   |
| <b>Charakteristische Tragfähigkeitswerte<br/>für das Verbindungselement</b><br><br><b>RP – T2 – 4,5 x L</b> | Anlage 3.2.21a<br>zur allgemeinen<br>bauaufsichtlichen<br>Zulassung Nr. Z-14.1-537<br>vom 25. November 2011  |  | <b>Querkraft <math>V_{R,k}</math> in [kN]</b>                 | <b>Bauteil I: <math>t_i</math> in [mm]</b> , Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$        | 0,50 | 0,50 | —    | 0,50 | —    | 0,50 | —    | 0,50 | —    | 0,50  | —    | <b>Bauteil II aus Holz Sortierkl. <math>\geq S10</math></b> |
|   |  |   | <b>Auszugs-<br/>kraft <math>N_{R,ii,k}</math> in<br/>[kN]</b> | 0,60   | 0,50 | —    | 0,61 | —    | 0,78 | —    | 0,90 | —    | 0,90 | —   | 0,90 | —   |

| Bohrschauben  |  <p><b>Werkstoff</b> Schraube:<br/>Nichtrostender Stahl,<br/>Werkstoff-Nr. 1.4301<br/><br/><b>Scheibe:</b><br/>Nichtrostender Stahl,<br/>Werkstoff-Nr. 1.4301<br/>mit aufvulkanisierter<br/>EPDM-Dichtung</p> <p><b>Hersteller</b> REISSER-<br/>Schraubentechnik GmbH<br/>Ingelfingen-Criesbach</p> <p><b>Vertrieb</b> REISSER- Schraubentechnik<br/>GmbH<br/>Fritz-Müller-Straße 10<br/>74653 Ingelfingen-Criesbach<br/>Tel.: +49 (0)7940 127-0<br/>Fax: +49 (0)7940 127-49<br/>Internet: <a href="http://www.reisser-screws.com">www.reisser-screws.com</a></p> <p>Weitere Festlegungen:</p> | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | <b>Bauteil II: <math>t_{II}</math> in [mm]</b><br>S235 nach DIN EN 10025-1, S280GD oder S320GD nach DIN EN 10346 |      |      |      |      |      |        |        |        |        | <b>Bauteil II</b><br>aus Holz<br>Sortierkl.<br>≥ S10 |
|---|---|---|--|------|------|------|------|------|--------|--------|--------|--------|--|
|   |   |   | 0,50   | 0,55 | 0,63 | 0,75 | 0,88 | 1,00 | 1,13   | 1,25   | 1,50   | 2,00   |  |
| <b>Charakteristische Tragfähigkeitswerte<br/>für das Verbindungselement</b><br><br><b>RP – T2 – 6,0 x L</b>                             | <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 165 \text{ N/mm}^2$   | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b> | 0,50   | 0,63 | 0,63 | 0,63 | 0,63 | 0,63 | 0,63   | 0,63   | 0,63   | —      | —  |
|   |   |   | 0,60   | 0,63 | 0,70 | 0,77 | 0,77 | 0,77 | 0,77   | 0,77   | 0,77   | 0,77   | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 165 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 0,70   | 0,63 | 0,70 | 0,81 | 0,90 | 0,90 | 0,90   | 0,90   | 0,90   | 0,90   | —  |
|   |   |   | 0,80   | 0,63 | 0,70 | 0,81 | 0,97 | 1,04 | 1,04   | 1,04   | 1,04   | 1,04   | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 0,90   | 0,63 | 0,70 | 0,81 | 0,97 | 1,30 | 1,36   | 1,36   | 1,36   | 1,36   | —  |
|   |   |   | 1,00   | 0,63 | 0,70 | 0,81 | 0,97 | 1,30 | 1,68 a | 1,68 a | 1,68 a | 1,68 a | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 1,20   | 0,63 | 0,70 | 0,81 | 0,97 | 1,30 | 1,68 a | 1,85 a | 1,94 a | 1,94 a | —  |
|   |   |   | 1,50   | 0,63 | 0,70 | 0,81 | 0,97 | 1,30 | 1,68 a | 1,85 a | 2,00 a | —      | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 2,00   | 0,63 | 0,70 | 0,81 | 0,97 | 1,30 | 1,68 a | —      | —      | —      | —  |
|   |   |   | 0,87   | 0,99 | 1,18 | 1,47 | 1,87 | 2,23 | 2,40   | 2,55   | 2,55   | —      | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 0,50   | 0,82 | 0,82 | 0,82 | 0,82 | 0,82 | 0,82   | 0,82   | 0,82   | 0,82   | —  |
|   |   |   | 0,60   | 0,82 | 0,91 | 1,00 | 1,00 | 1,00 | 1,00   | 1,00   | 1,00   | 1,00   | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 0,70   | 0,82 | 0,91 | 1,05 | 1,18 | 1,18 | 1,18   | 1,18   | 1,18   | 1,18   | —  |
|   |   |   | 0,80   | 0,82 | 0,91 | 1,05 | 1,27 | 1,36 | 1,36   | 1,36   | 1,36   | 1,36   | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 0,90   | 0,82 | 0,91 | 1,05 | 1,27 | 1,70 | 1,78   | 1,78   | 1,78   | 1,78   | —  |
|   |   |   | 1,00   | 0,82 | 0,91 | 1,05 | 1,27 | 1,70 | 2,19 a | 2,19 a | 2,19 a | 2,19 a | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 1,20   | 0,82 | 0,91 | 1,05 | 1,27 | 1,70 | 2,19 a | 2,41 a | 2,53 a | 2,53 a | —  |
|   |   |   | 1,50   | 0,82 | 0,91 | 1,05 | 1,27 | 1,70 | 2,19 a | 2,41 a | 2,62 a | —      | —  |
| <b>Querkraft <math>V_{R,k}</math> in [kN]</b><br>Bauteil I: $t_i$ in [mm], Aluminium mit<br>Zugfestigkeit $R_m \geq 215 \text{ N/mm}^2$ | <b>Auszugs-<br/>kraft <math>N_{R,k,II}</math> in<br/>[kN]</b>   | <b>Max. Bohrleistung <math>\Sigma t_i</math></b><br>3,90 mm   | 2,00   | 0,82 | 0,91 | 1,05 | 1,27 | 1,70 | 2,19 a | —      | —      | —      | —  |
|   |   |   | 0,87   | 0,99 | 1,18 | 1,47 | 1,87 | 2,23 | 2,40   | 2,55   | 2,55   | —      | —  |



