

# **European Technical Approval ETA-09/0078**

Handelsbezeichnung Trade name	G&B Fissaggi Injektionssystem GEBOFIX PRO VE-SF für Beton G&B Fissaggi Injection System GEBOFIX PRO VE-SF for concrete
Zulassungsinhaber Holder of approval	G&B FISSAGGI Corso Savona, 22 10029 Villatellone (TO) ITALIEN
Zulassungsgegenstand und Verwendungszweck Generic type and use of construction product	Verbunddübel mit Ankerstange zur Verankerung im Beton Bonded Anchor with Anchor rod for use in concrete
Geltungsdauer: von <i>Validity: fron</i> bis <i>to</i>	21 June 2013
Herstellwerk Manufacturing plant	G&B Fissaggi S.R.L., Plant4

English translation prepared by DIBt - Original version in German language

Diese Zulassung umfasst	33 Seiten einschließlich 24 Anhänge
This Approval contains	33 pages including 24 annexes
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Diese Zulassung ersetzt This Approval replaces



Europäische Organisation für Technische Zulassungen European Organisation for Technical Approvals



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## I LEGAL BASES AND GENERAL CONDITIONS

- 1 This European technical approval is issued by Deutsches Institut für Bautechnik in accordance with:
  - Council Directive 89/106/EEC of 21 December 1988 on the approximation of laws, regulations and administrative provisions of Member States relating to construction products<sup>1</sup>, modified by Council Directive 93/68/EEC<sup>2</sup> and Regulation (EC) N° 1882/2003 of the European Parliament and of the Council<sup>3</sup>;
  - Gesetz über das In-Verkehr-Bringen von und den freien Warenverkehr mit Bauprodukten zur Umsetzung der Richtlinie 89/106/EWG des Rates vom 21. Dezember 1988 zur Angleichung der Rechts- und Verwaltungsvorschriften der Mitgliedstaaten über Bauprodukte und anderer Rechtsakte der Europäischen Gemeinschaften (Bauproduktengesetz - BauPG) vom 28. April 1998<sup>4</sup>, as amended by Article 2 of the law of 8 November 2011<sup>5</sup>;
  - Common Procedural Rules for Requesting, Preparing and the Granting of European technical approvals set out in the Annex to Commission Decision 94/23/EC<sup>6</sup>;
  - Guideline for European technical approval of "Metal anchors for use in concrete Part 5: Bonded anchors", ETAG 001-05.
- 2 Deutsches Institut für Bautechnik is authorized to check whether the provisions of this European technical approval are met. Checking may take place in the manufacturing plant. Nevertheless, the responsibility for the conformity of the products to the European technical approval and for their fitness for the intended use remains with the holder of the European technical approval.
- 3 This European technical approval is not to be transferred to manufacturers or agents of manufacturers other than those indicated on page 1, or manufacturing plants other than those indicated on page 1 of this European technical approval.
- 4 This European technical approval may be withdrawn by Deutsches Institut für Bautechnik, in particular pursuant to information by the Commission according to Article 5(1) of Council Directive 89/106/EEC.
- 5 Reproduction of this European technical approval including transmission by electronic means shall be in full. However, partial reproduction can be made with the written consent of Deutsches Institut für Bautechnik. In this case partial reproduction has to be designated as such. Texts and drawings of advertising brochures shall not contradict or misuse the European technical approval.
- 6 The European technical approval is issued by the approval body in its official language. This version corresponds fully to the version circulated within EOTA. Translations into other languages have to be designated as such.
- <sup>1</sup> Official Journal of the European Communities L 40, 11 February 1989, p. 12
- Official Journal of the European Communities L 220, 30 August 1993, p. 1
- <sup>3</sup> Official Journal of the European Union L 284, 31 October 2003, p. 25
- <sup>4</sup> Bundesgesetzblatt Teil I 1998, p. 812
  - *Bundesgesetzblatt Teil I 2011*, p. 2178

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Official Journal of the European Communities L 17, 20 January 1994, p. 34



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## II SPECIFIC CONDITIONS OF THE EUROPEAN TECHNICAL APPROVAL

#### 1 Definition of product and intended use

#### 1.1 Definition of the construction product

The "G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete" is a bonded anchor consisting of a cartridge with G&B Fissaggi injection mortar GEBOFIX PRO VE-SF and a steel element. The steel elements are commercial threaded rods according to Annex 3 in the range of M8 to M30 or reinforcing bar according to Annex 4 in the range of diameter 8 to 32 mm.

The steel element is placed into a drilled hole filled with injection mortar and is anchored via the bond between metal part, injection mortar and concrete.

An illustration of the product and intended use is given in Annexes 1 and 2.

#### 1.2 Intended use

The anchor is intended to be used for anchorages for which requirements for mechanical resistance and stability and safety in use in the sense of the Essential Requirements 1 and 4 of Council Directive 89/106 EEC shall be fulfilled and failure of anchorages made with these products would cause risk to human life and/or lead to considerable economic consequences. Safety in case of fire (Essential Requirement 2) is not covered in this European technical approval.

The anchor is to be used only for anchorages subject to static or quasi-static loading in reinforced or unreinforced normal weight concrete of strength classes C20/25 at minimum and C50/60 at most according to EN 206:2000-12.

The anchor may be used in cracked and non-cracked concrete.

The anchor may also be used under seismic action for performance category C1 according to Annex 23.

The anchor may be installed in dry or wet concrete.

The anchor sizes diameter 8 mm to 16 mm may also be installed in flooded holes.

The anchor may be used in the following temperature ranges:

Temperature range I:	-40 °C to +40 °C	(max long term temperature +24 °C and
		max short term temperature +40 °C)
Temperature range II:	-40 °C to +80 °C	(max long term temperature +50 °C and
		max short term temperature +80 °C)
Temperature range III:	-40 °C to +120 °C	(max long term temperature +72 °C and
		max short term temperature +120 °C)

#### Elements made of zinc coated steel:

The element made of zinc plated or hot dip galvanised steel may only be used in structures subject to dry internal conditions.

#### Elements made of stainless steel:

The element made of stainless steel 1.4401, 1.4404 or 1.4571 may be used in structures subject to dry internal conditions and also in structures subject to external atmospheric exposure (including industrial and marine environment), or exposure to permanently damp internal conditions, if no particular aggressive conditions exist. Such particular aggressive conditions are e. g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with extreme chemical pollution (e. g. in desulphurization plants or road tunnels where de-icing materials are used).



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Elements made of high corrosion resistant steel:

The element made of high corrosion resistant steel 1.4529 or 1.4565 may be used in structures subject to dry internal conditions and also in structures subject to external atmospheric exposure, in permanently damp internal conditions or in other particular aggressive conditions. Such particular aggressive conditions are e.g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with chemical pollution (e.g. in desulphurization plants or road tunnels where de-icing materials are used).

#### Elements made of reinforcing bars:

Post-installed reinforcing bars may be used as anchor designed in accordance with the EOTA Technical Report TR 029 or CEN/TS 1992-4:2009. Such applications are e.g. concrete overlay or shear dowel connections or the connections of a wall predominantly loaded by shear and compression forces with the foundation, where the reinforcing bars act as dowels to take up shear forces. Connections with post-installed reinforcing bars in concrete structures designed in accordance with EN 1992-1-1: 2004 are not covered by this European technical approval.

The provisions made in this European technical approval are based on an assumed working life of the anchor of 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

#### 2 Characteristics of the product and methods of verification

#### 2.1 Characteristics of the product

The anchor corresponds to the drawings and provisions given in the Annexes. The characteristic material values, dimensions and tolerances of the anchor not indicated in the Annexes shall correspond to the respective values laid down in the technical documentation<sup>7</sup> of this European technical approval.

The characteristic values for the design of anchorages are given in the Annexes.

The two components of the injection mortar are delivered in unmixed condition in coaxial cartridges of sizes 150 ml, 280 ml, 300 ml, 310 ml, 330 ml, 380 ml, 410 ml or 420 ml, in side-by side-cartridges of sizes 235 ml, 345 ml or 825 ml or in foil tube cartridges of sizes 165 ml or 300 ml according to Annex 2. Each cartridge is marked with the imprint "GEBOFIX PRO VE-SF", with processing notes, charge code, storage life, hazard code and curing- and processing time depending on temperature.

Elements made of reinforcing bars shall comply with the specifications given in Annex 4.

The marking of embedment depth may be done on jobsite.

#### 2.2 Methods of verification

The assessment of fitness of the anchor for the intended use in relation to the requirements for mechanical resistance and stability and safety in use in the sense of the Essential Requirements 1 and 4 has been made in accordance with the "Guideline for European technical approval of Metal Anchors for Use in Concrete", Part 1 "Anchors in general" and Part 5 "Bonded anchors", on the basis of Option 1 and ETAG 001 Annex E "Assessment of Metal Anchors under Seismic Action".

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The technical documentation of this European technical approval is deposited at the Deutsches Institut für Bautechnik and, as far as relevant for the tasks of the approved bodies involved in the attestation of conformity procedure, is handed over to the approved bodies.



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In addition to the specific clauses relating to dangerous substances contained in this European technical approval, there may be other requirements applicable to the products falling within its scope (e.g. transposed European legislation and national laws, regulations and administrative provisions). In order to meet the provisions of the Construction Products Directive, these requirements need also to be complied with, when and where they apply.

### 3 Evaluation and attestation of conformity and CE marking

### 3.1 System of attestation of conformity

According to the Decision 96/582/EG of the European Commission<sup>8</sup> system 2(i) (referred to as System 1) of the attestation of conformity applies.

This system of attestation of conformity is defined as follows:

System 1: Certification of the conformity of the product by an approved certification body on the basis of:

- (a) Tasks for the manufacturer:
  - (1) factory production control;
  - (2) further testing of samples taken at the factory by the manufacturer in accordance with a control plan;
- (b) Tasks for the approved body:
  - (3) initial type-testing of the product;
  - (4) initial inspection of factory and of factory production control;
  - (5) continuous surveillance, assessment and approval of factory production control.

Note: Approved bodies are also referred to as "notified bodies".

#### 3.2 Responsibilities

#### 3.2.1 Tasks for the manufacturer

3.2.1.1 Factory production control

The manufacturer shall exercise permanent internal control of production. All the elements, requirements and provisions adopted by the manufacturer shall be documented in a systematic manner in the form of written policies and procedures, including records of results performed. This production control system shall insure that the product is in conformity with this European technical approval.

The manufacturer may only use initial/raw/constituent materials stated in the technical documentation of this European technical approval.

The factory production control shall be in accordance with the control plan which is part of the technical documentation of this European technical approval. The control plan is laid down in the context of the factory production control system operated by the manufacturer and deposited at Deutsches Institut für Bautechnik.<sup>9</sup>

The results of factory production control shall be recorded and evaluated in accordance with the provisions of the control plan.

The control plan is a confidential part of the European technical approval and only handed over to the approved body involved in the procedure of attestation of conformity. See section 3.2.2.



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#### 3.2.1.2 Other tasks for the manufacturer

The manufacturer shall, on the basis of a contract, involve a body which is approved for the tasks referred to in section 3.1 in the field of anchors in order to undertake the actions laid down in section 3.2.2 For this purpose, the control plan referred to in sections 3.2.1.1 and 3.2.2 shall be handed over by the manufacturer to the approved body involved.

The manufacturer shall make a declaration of conformity, stating that the construction product is in conformity with the provisions of this European technical approval.

#### 3.2.2 Tasks for the approved bodies

The approved body shall perform the

- initial type-testing of the product,
- initial inspection of factory and of factory production control,
- continuous surveillance, assessment and approval of factory production control, in accordance with the provisions laid down in the control plan.

The approved body shall retain the essential points of its actions referred to above and state the results obtained and conclusions drawn in a written report.

The approved certification body involved by the manufacturer shall issue an EC certificate of conformity of the product stating the conformity with the provisions of this European technical approval.

In cases where the provisions of the European technical approval and its control plan are no longer fulfilled the certification body shall withdraw the certificate of conformity and inform Deutsches Institut für Bautechnik without delay.

#### 3.3 CE marking

The CE marking shall be affixed on each packaging of the anchor. The letters "CE" shall be followed by the identification number of the approved certification body, where relevant, and be accompanied by the following additional information:

- the name and address of the holder of the approval (legal entity responsible for the manufacture),
- the last two digits of the year in which the CE marking was affixed,
- the number of the EC certificate of conformity for the product,
- the number of the European technical approval,
- the number of the guideline for European technical approval,
- use category (ETAG 001, Option 1, seismic anchor performance category C1),
- size.

# 4 Assumptions under which the fitness of the product for the intended use was favourably assessed

#### 4.1 Manufacturing

The European technical approval is issued for the product on the basis of agreed data/information, deposited at Deutsches Institut für Bautechnik, which identifies the product that has been assessed and judged. Changes to the product or production process, which could result in this deposited data/information being incorrect, should be notified to Deutsches Institut für Bautechnik before the changes are introduced. Deutsches Institut für Bautechnik will decide whether or not such changes affect the approval and consequently the validity of the CE marking on the basis of the approval and if so whether further assessment or alterations to the approval shall be necessary.



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#### 4.2 Design of anchorages

The fitness of the anchor for the intended use is given under the following conditions:

The anchorages are designed either in accordance with the

The anchorages are designed in accordance with the

- EOTA Technical Report TR 029 "Design of bonded anchors"<sup>10</sup>
- or in accordance with the
- CEN/TS 1992-4:2009

and EOTA Technical Report TR 045 "Design of Metal Anchors under Seismic Action" under the responsibility of an engineer experienced in anchorages and concrete work.

Anchorages shall be positioned outside of critical regions (e.g. plastic hinges) of the concrete structure. Fastenings in stand-off installation or with a grout layer under seismic action are not covered by this European technical approval.

Post-installed reinforcing bars may be used as anchor designed in accordance with the EOTA Technical Report TR 029 or CEN/TS 1992-4:2009. The basic assumptions for the design according to anchor theory shall be observed. This includes the consideration of tension and shear loads and the corresponding failure modes as well as the assumption that the base material (concrete structural element) remains essentially in the serviceability limit state (either non-cracked or cracked) when the connection is loaded to failure. Such applications are e.g. concrete overlay or shear dowel connections or the connections of a wall predominantly loaded by shear and compression forces with the foundation, where the rebars act as dowels to take up shear forces. Connections with reinforcing bars in concrete structures designed in accordance with EN 1992-1-1:2004 (e.g. connection of a wall loaded with tension forces in one layer of the reinforcement with the foundation) are not covered by this European technical approval.

Verifiable calculation notes and drawings are prepared taking account of the loads to be anchored.

The position of the anchor is indicated on the design drawings (e.g. position of the anchor relative to reinforcement or to supports, etc.).

#### 4.3 Installation of anchors

The fitness for use of the anchor can only be assumed if the anchor is installed as follows:

- anchor installation carried out by appropriately qualified personnel and under the supervision
  of the person responsible for technical matters of the site,
- anchor installation in accordance with the manufacturer's specifications and drawings using the tools indicated in the technical documentation of this European technical approval,
- use of the anchor only as supplied by the manufacturer without exchanging the components,
- commercial standard threaded rods, washers and hexagon nuts may be used if the following requirements are fulfilled:
  - material, dimensions and mechanical properties of the metal parts according to the specifications given in Annex 3,
  - confirmation of material and mechanical properties of the metal parts by inspection certificate 3.1 according to EN 10204:2004, the documents should be stored,
  - marking of the threaded rod with the envisage embedment depth. This may be done by the manufacturer of the rod or the person on jobsite.
- embedded reinforcing bars shall comply with specifications given in Annex 4,

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- checks before placing the anchor to ensure that the strength class of the concrete in which the anchor is to be placed is in the range given and is not lower than that of the concrete to which the characteristic loads apply,
- check of concrete being well compacted, e.g. without significant voids,
- marking and keeping the effective anchorage depth,
- edge distance and spacing not less than the specified values without minus tolerances,
- positioning of the drill holes without damaging the reinforcement,
- drilling by hammer-drilling only,
- in case of aborted drill hole: the drill hole shall be filled with mortar,
- cleaning the drill hole in accordance with Annexes 6 to 8,
- during installation and curing of the chemical mortar the anchor component installation temperature shall be at least -10 °C; the temperature; observing the curing time according to Annex 7, Table 4 until the anchor may be loaded,
- for injection of the mortar in bore holes of diameter  $d_0 > 20$  mm piston plugs according to Annex 8 shall be used for overhead or horizontal injection,
- installation torque moments are not required for functioning of the anchor. However, the torque moments given in Annex 5 must not be exceeded.

### 5 Indications to the manufacturer

#### 5.1 Responsibility of the manufacturer

The manufacturer is responsible to ensure that the information on the specific conditions according to 1 and 2 including Annexes referred to as well as sections 4.2, 4.3 and 5.2 is given to those who are concerned. This information may be made by reproduction of the respective parts of the European technical approval.

In addition all installation data shall be shown clearly on the package and/or on an enclosed instruction sheet, preferably using illustration(s).

The minimum data required are:

- drill bit diameter,
- hole depth,
- diameter of anchor rod,
- minimum effective anchorage depth,
- information on the installation procedure, including cleaning of the hole with the cleaning equipments, preferably by means of an illustration,
- anchor component installation temperature,
- ambient temperature of the concrete during installation of the anchor,
- admissible processing time (open time) of the mortar,
- curing time until the anchor may be loaded as a function of the ambient temperature in the concrete during installation,
- maximum torque moment,
- identification of the manufacturing batch,

All data shall be presented in a clear and explicit form.



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#### 5.2 Packaging, transport and storage

The cartridges shall be protected against sun radiation and shall be stored according to the manufacturer's installation instructions in dry condition at temperatures of at least +5 °C to not more than +25 °C.

Cartridges with expired shelf life must no longer be used.

The anchor shall only be packaged and supplied as a complete unit. Cartridges may be packed separately from metal parts.

Andreas Kummerow p.p. Head of Department *beglaubigt:* Baderschneider

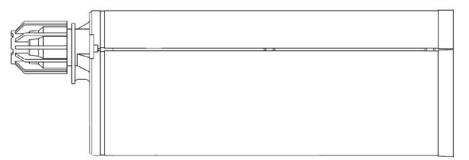


## Injection mortar: GEBOFIX PRO VE-SF

150 ml, 280 ml, 300 ml, 310ml, 330 ml, 380 ml, 410 ml and 420 ml cartridge (Type: coaxial)



235 ml, 345 ml and 825 ml cartridge (Type: "side-by-side")

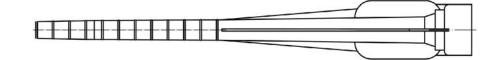


## 165 ml and 300 ml cartridge (Type: "foil tube")





Cartridge label: GEBOFIX PRO VE-SF, processing notes, charge-code, shelf life, hazard-code, curing- and processing time (depending on the temperature), with as well as without travel scale

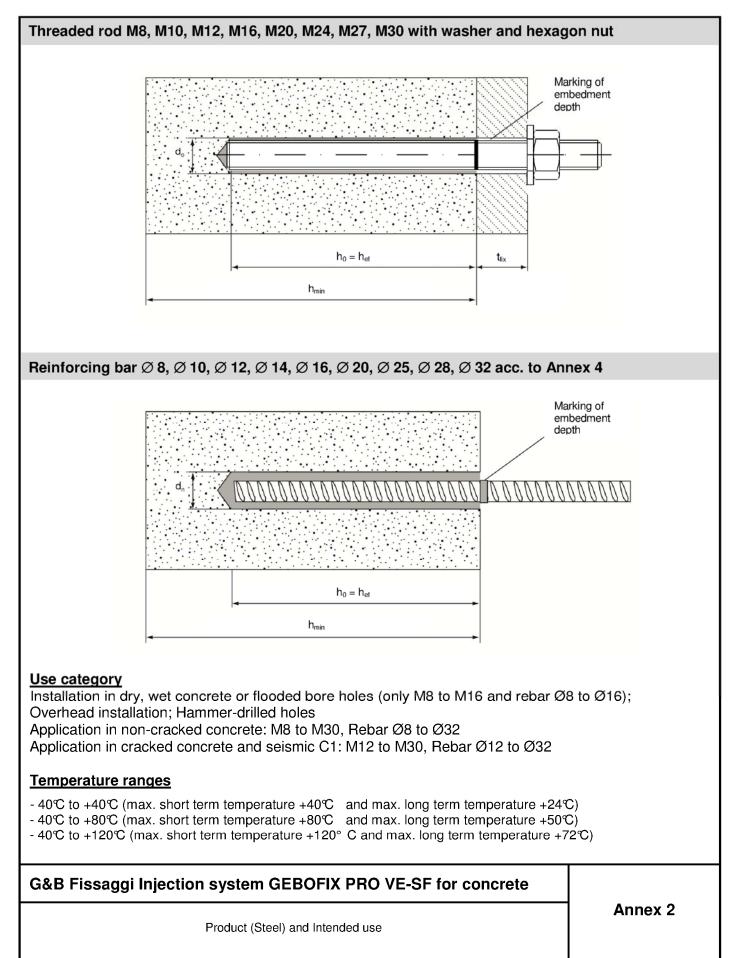


G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete

Product (Injection mortar) and static mixer

Annex 1







Tab	le 1a: Materials (Threaded rod	i)					
		L					
	hef						
	1		- 2				
			-				
	hef						
	-	L					
Part	Designation	Material					
	I, zinc plated $\geq$ 5 µm acc. to EN ISO 404						
hot-d	dip galvanised ≥ 40 μm acc. to EN ISO <sup>-</sup> ∣						
1	Anchor rod	Steel, EN 10087 or EN 10263 Property class 4,6, 5.8, 8.8, EN ISO 898-1.	1999				
──		Property class 4 (for class 4.6 rod) EN ISO					
2	Hexagon nut, EN ISO 4032	Property class 5 (for class 5.8 rod) EN ISO	898-2,				
		Property class 8 (for class 8.8 rod) EN ISO	898-2				
3	Washer, EN ISO 887, EN ISO 7089, EN ISO 7093, or EN ISO 7094	Steel, zinc plated or hot-dip galvanised					
Stair	nless steel						
Juli		Material 1.4401 / 1.4404 / 1.4571, EN 1008	8-1:2005				
1	Anchor rod	> M24: Property class 50 EN ISO 3506	0-1.2003,				
		≤ M24: Property class 70 EN ISO 3506					
2	Hexagon nut, EN ISO 4032	Material 1.4401 / 1.4404 / 1.4571 EN 10088 > M24: Property class 50 (for class 50 rod)					
<b>1</b>	Hexagon hut, EN 130 4032	$\leq$ M24: Property class 30 (for class 30 rod) $\leq$ M24: Property class 70 (for class 70 rod)					
3	Washer, EN ISO 887, EN ISO 7089,	Material 1.4401, 1.4404 or 1.4571, EN 100					
	EN ISO 7093, or EN ISO 7094		00				
High	corrosion resistance steel						
		Material 1.4529 / 1.4565, EN 10088-1:2005	,				
1	Anchor rod	<ul> <li>&gt; M24: Property class 50 EN ISO 3506</li> <li>≤ M24: Property class 70 EN ISO 3506</li> </ul>					
		Material 1.4529 / 1.4565 EN 10088,					
2	Hexagon nut, EN ISO 4032	> M24: Property class 50 (for class 50 rod)					
		≤ M24: Property class 70 (for class 70 rod)	EN ISO 3506				
3	Washer, EN ISO 887, EN ISO 7089, EN ISO 7093, or EN ISO 7094	Material 1.4529 / 1.4565, EN 10088					
Com	mercial standard rod with:	I					
	Materials, dimensions and mechanica	l properties acc. Table 1a					
-	Inspection certificate 3.1 acc. to EN 10						
-	Marking of embedment depth						
G&E	3 Fissaggi Injection system GEB	OFIX PRO VE-SF for concrete					
			Annex 3				
	Materials (Thr	eaded rod)					



Table 1b: Mate	rials (Rebar)		
<b> </b>	h <sub>ef</sub>	000000000000000000000000000000000000000	►
	92-1-1 Annex C, Table C.	1, Properties of reinforcement:	
Product form Class		Bars and de-coiled B	c c
	rength f <sub>yk</sub> or f <sub>0,2k</sub> (N/mm²)	400 to 600	
Minimum value of k =	(f <sub>t</sub> / f <sub>y</sub> ) <sub>k</sub>	≥ 1,08	≥ 1,15 < 1,35
Characteristic strain a $\epsilon_{uk}$ (%)	t maximum force	≥ 5,0	≥ 7,5
Bendability		Bend/Rebend to	est
Maximum deviation from nominal mass (individual bar) (%)	Nominal bar size (mm) ≤ 8 > 8	± 6,0 ± 4,5	
Abstract of EN 199 Product form	92-1-1 Annex C, Table C.2	2N, Properties of reinforcement: Bars and de-coiled	d rods
Class		В	С
Min. value of related rip area f <sub>R,min</sub>	nominal diameter of the rebar (mm) 8 to 12 > 12	0,040 0,056	
with: d = nominal diam	r rib h <sub>rib</sub> shall fulfil the followin neter of the rebar post-installed rebar as anchor	ng requirement: 0,05 * d ≤ $h_{rib}$ ≤ 0,07 * c see chapter 4.2 <b>X PRO VE-SF for concrete</b>	
	Materials (Reinforcin	ng bar)	Annex 4

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#### Deutsches Institut für Bautechnik

Table 2:   Installation	parameters fo	or threa	aded ro	d						
Anchor size		M 8	M 10	M 12	M 16	M 20	M 24	M 27	M 30	
Nominal drill hole diameter	d <sub>0</sub> [mm] =	10	12	14	18	24	28	32	35	
Effective encharge denth	h <sub>ef,min</sub> [mm] =	64	80	96	128	160	192	216	240	
Effective anchorage depth	h <sub>ef,max</sub> [mm] =	144	180	216	288	360	432	486	540	
Diameter of clearance hole in the fixture $d_f[mm] \le 9$ 1214182226		26	30	33						
Diameter of steel brush	d <sub>b</sub> [mm] ≥	≥ 12 14 16 20 26 30 34				37				
Torque moment	T <sub>inst</sub> [Nm] ≤	10 20 40 80 120 160 180 2				200				
Thiskness of fixture	t <sub>fix,min</sub> [mm] >	0								
Thickness of fixture	t <sub>fix,max</sub> [mm] <				15	00				
Minimum thickness of member	h <sub>min</sub> [mm]		<sub>≇f</sub> + 30 m ≥ 100 mn				h <sub>ef</sub> + 2d <sub>0</sub>	i		
Minimum spacing	s <sub>min</sub> [mm]	40	50	60	80	100	120	135	150	
Minimum edge distance	c <sub>min</sub> [mm]	40	50	60	80	100	120	135	150	

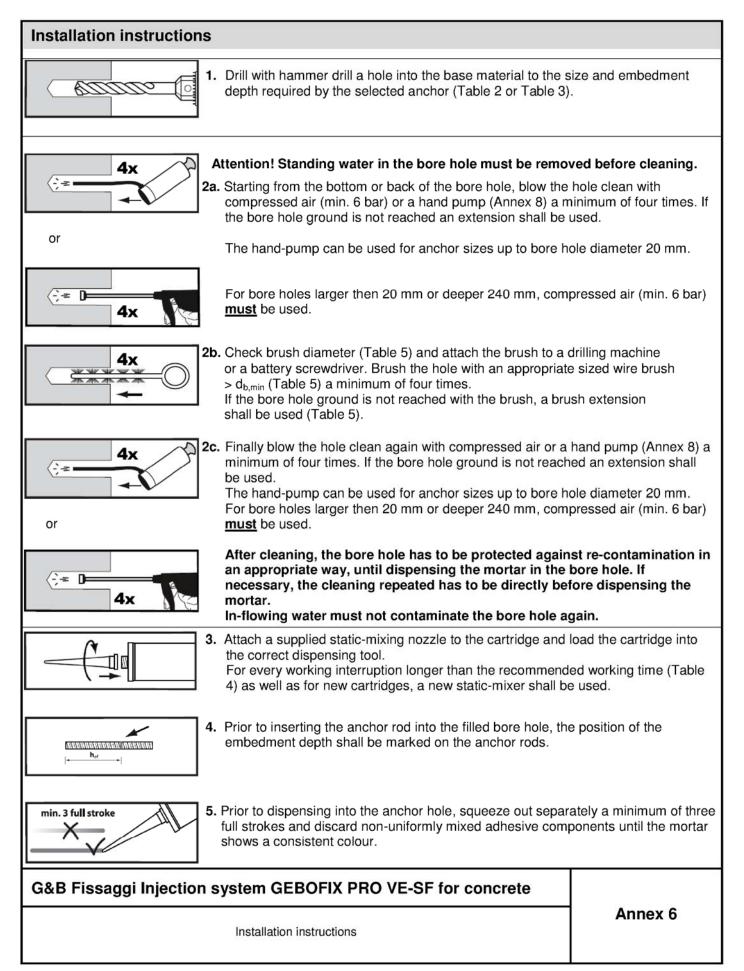
## Table 3:Installation parameters for rebar

			-	-	-					
Rebar size		Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Nominal drill hole diameter	d <sub>0</sub> [mm] =	12	14	16	18	20	24	32	35	40
Effective anaborage depth	h <sub>ef,min</sub> [mm] =	64	80	96	112	128	160	200	224	256
Effective anchorage depth	h <sub>ef,max</sub> [mm] =	144	180	216	252	288	360	450	504	576
Diameter of steel brush	d <sub>b</sub> [mm] ≥	14	16	18	20	22	26	34	37	41,5
Minimum thickness of member	h <sub>min</sub> [mm]	h <sub>ef</sub> + 30 mm ≥ 100 mm								
Minimum spacing	s <sub>min</sub> [mm]	40	50	60	70	80	100	125	140	160
Minimum edge distance	c <sub>min</sub> [mm]	40	50	60	70	80	100	125	140	160

# G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete

Annex 5







Installation instruction	ns (continuation)
	<b>6.</b> Starting from the bottom or back of the cleaned anchor hole fill the hole up to approximately two-thirds with adhesive. Slowly withdraw the static mixing nozzle as the hole fills to avoid creating air pockets. For embedment larger than 190 mm an extension nozzle shall be used. For overhead and horizontal installation in bore holes larger than $\emptyset$ 20 mm a piston plug and extension nozzle (Annex 8) shall be used. Observe the gel-/ working times given in Table 4.
	<b>7.</b> Push the threaded rod or reinforcing bar into the anchor hole while turning slightly to ensure positive distribution of the adhesive until the embedment depth is reached. The anchor should be free of dirt, grease, oil or other foreign material.
X	8. Be sure that the anchor is fully seated at the bottom of the hole and that excess mortar is visible at the top of the hole. If these requirements are not maintained, the application has to be renewed. For overhead application the anchor rod should be fixed (e.g. wedges).
+20°C 00:45″	<ol> <li>Allow the adhesive to cure to the specified time prior to applying any load or torque. Do not move or load the anchor until it is fully cured (attend Table 4).</li> </ol>
	10. After full curing, the add-on part can be installed with the max. torque (Table 2) by using a calibrated torque wrench.

#### Table 4: Minimum curing time

Base material temperature	Gel time (working time)	Minimum curing time in dry concrete	Minimum curing time in wet concrete
-10℃ to -4℃ 1)	90 min	24 h	48 h
-5°C to -1°C 2)	90 min	14 h	24 h
+0°C to +5°C $^{2)}$	45 min	7 h	14 h
+5°C to +9°C <sup>2)</sup>	25 min	2 h	4 h
+10℃ to +19℃ <sup>2)</sup>	15 min	80 min	160 min
+20°C to +29°C <sup>2)</sup>	6 min	45 min	90 min
+30°C to +34°C 2)	4 min	25 min	50 min
+35°C to +39°C <sup>2)</sup>	2 min	20 min	40 min
+40 °C <sup>2)</sup>	1,5 min	15 min	30 min
<sup>1)</sup> Cortridge temperature mu	at he at min 15%		

<sup>1)</sup> Cartridge temperature <u>must</u> be at min. +15°C  $^{2)}$  Minimum cartridge temperature +5°C

# G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete

Annex 7

Installation instructions (continuation) Curing time



Table 5: Paran	neter clear	ning and se	etting tools		
Anchor	Size (mm)	Nominal drill bit diameter d <sub>o</sub> (mm)	Steel Brush d₅ (mm)	Steel Brush (min brush diameter) d <sub>b,min</sub> (mm)	Piston plug
		8		in the second	
	M8	10,0	12,0	10,5	
	M10	12,0	14,0	12,5	
Threaded	M12	14,0	16,0	14,5	
Rod	M16	18,0	20,0	18,5	
	M20	24,0	26,0	24,5	#24
	M24	28,0	30,0	28,5	#28
	M27	32,0	34,0	32,5	#32
	M30	35,0	37,0	35,5	#35
	Ø8	12,0	14,0	12,5	
	Ø10	14,0	16,0	14,5	
	Ø12	16,0	18,0	16,5	
Rebar	Ø14	18,0	20,0	18,5	
	Ø16	20,0	22,0	20,5	
1999,999,999,999,999,999,997,997,997,997	Ø20	24,0	26,0	24,5	#24
	Ø25	32,0	34,0	32,5	#32
	Ø28	35,0	37,0	35,5	#35
	Ø32	40,0	41,5	38,5	#38

Hand pump (volume 750 ml) Drill bit diameter (d<sub>0</sub>): 10 mm to 20 mm

Compressed air tool (min 6 bar) Drill bit diameter ( $d_0$ ): 10 mm to 40 mm

# G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete

Cleaning and setting tools





Anchor size threaded rod				M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30	
Steel failure					1							
Characteristic tension res Steel, property class 4.6	sistance,	N <sub>Rk,s</sub>	[kN]	15	23	34	63	98	141	184	224	
Partial safety factor		γ <sub>Ms,N</sub> <sup>1)</sup>	L				2	,0				
Characteristic tension res	sistance,	N <sub>Rk,s</sub>	[kN]	18	29	42	78	122	176	230	280	
Steel, property class 5.8 Characteristic tension res Steel, property class 8.8	sistance,	N <sub>Rk,s</sub>	[kN]	29	46	67	125	196	282	368	449	
Partial safety factor		γ <sub>Ms,N</sub> <sup>1)</sup>					1.	50				
Characteristic tension res Stainless steel A4 and He property class 50 (>M24)	CR,	N <sub>Rk,s</sub>	[kN]	26	41	59	110	171	247	230	281	
Partial safety factor	, , , , , , , , , , , , , , , , , , ,	γ <sub>Ms,N</sub> <sup>1)</sup>				1,	87			2,	86	
Combined pull-out and	concrete cone failure											
Characteristic bond resis	tance in non-cracked co	ncrete C20/	25									
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,ucr}}$	[N/mm <sup>2</sup> ]	8,5	10,0	10,0	10,0	10,0	9,5	8,5	7,5	
40°C/24°C	flooded bore hole	$\tau_{Rk,ucr}$	[N/mm <sup>2</sup> ]	6,0	7,5	7,5	7,5		not adr	nissible		
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\rm Rk,ucr}$	[N/mm²]	6,5	7,5	7,5	7,5	7,5	7,0	6,5	5,5	
80°C/50°C	flooded bore hole	$\tau_{\text{Rk,ucr}}$	[N/mm <sup>2</sup> ]	4,5	5,5	5,5	5,5		not admissible			
1209C/729C	dry and wet concrete	$\tau_{\text{Rk,ucr}}$	[N/mm <sup>2</sup> ]	4,5	5,5	5,5	5,5	5,5	5,5	4,5	3,5	
	flooded bore hole	$\tau_{\text{Rk,ucr}}$	[N/mm <sup>2</sup> ]	3,5	4,0	4,0	4,0		not adr	nissible		
Increasing factors for con	ocrata	C30/37 1,04					04					
$\psi_c$	lorete	C40/50		1,08								
Splitting failure		C50/60					1,	10				
Spinning failure			2)			h/	h <sub>ef</sub> ]					
	_	h/	′ h <sub>ef</sub> <sup>3)</sup> ≥ 2,0	1	,0 h <sub>et</sub>	2	,0					
Edge distance c <sub>cr,sp</sub> [mm]	for	2,0 > h /	h <sub>ef</sub> <sup>3)</sup> > 1,3	4,6 h	l <sub>ef</sub> - 1,8 h	1	,3		$\searrow$			
	-					-  '	,0					
		h /	h <sub>ef</sub> <sup>3)</sup> ≤ 1,3	2,	26 h <sub>ef</sub>		+	i 1,0∙h	<sub>ef</sub> 2,2	26∙h <sub>ef</sub>	<b>c</b> <sub>cr,sp</sub>	
Axial distance		S <sub>cr,sp</sub>	[mm]				2 c	or,sp				
Partial safety factor (dry a	and wet concrete)	$\gamma_{Mp} = \gamma_{Mc} =$	= γ <sub>Msp</sub> <sup>1)</sup>	1,5 <sup>4)</sup>				1,8 <sup>5)</sup>				
Partial safety factor (flood	ded bore hole)	$\gamma_{Mp} = \gamma_{Mc} =$	= γ <sub>Msp</sub> <sup>1)</sup>		2,	1 <sup>6)</sup>			not admissible			
<ul> <li><sup>2)</sup> Explanations se</li> <li><sup>3)</sup> h = concrete me</li> <li><sup>4)</sup> The partial safet</li> <li><sup>5)</sup> The partial safet</li> </ul>	ther national regulation e section 1.2 mber thickness, $h_{ef} = \gamma$ y factor $\gamma_2 = 1.0$ is including y factor $\gamma_2 = 1.2$ is including y factor $\gamma_2 = 1.4$ is including	effective a luded. luded.	inchorage o	depth								
	njection system		FIX PRO	) VE-S	SF for	conc	rete					
aab i loodggi li												



Anchor size threaded rod				M 12	M 16	M 20	M24	M 27	M 30	
Steel failure					I			<b></b>		
Characteristic tension resista Steel, property class 4.6	nce,	N <sub>Rk,s</sub>	[kN]	34	63	98	141	184	224	
Partial safety factor		γ <sub>Ms,N</sub> 1)	1			2	2,0			
Characteristic tension resista	nce,	N <sub>Rk,s</sub>	[kN]	42	78	122	176	230	280	
Steel, property class 5.8 Characteristic tension resista	nce.									
Steel, property class 8.8		N <sub>Rk,s</sub>	[kN]	67	125	196	282	368	449	
Partial safety factor		γ <sub>Ms,N</sub> <sup>1)</sup>				1	,50			
Characteristic tension resista Stainless steel A4 and HCR, property class 50 (>M24) and		N <sub>Rk,s</sub>	[kN]	59	110	171	247	230	281	
Partial safety factor		$\gamma_{MS,N}$ 1)				,87		2,	86	
Combined pull-out and con	crete cone failure									
Characteristic bond resistanc	e in cracked concrete C20/2	25			_			_	_	
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	4,5	4,5	4,5	4,5	5,0	5,0	
40°C/24°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	4,5	4,5		not adr	nissible		
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	3,0	3,0	3,0	3,0	4,0	4,0	
80°C/50°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	3,0	3,0		not adr	nissible		
	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	2,5	2,5	2,5	2,5	3,0	3,0	
120℃/72℃	flooded bore hole	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	2,5	2,5		not adr	nissible		
		C30/37 1,04					,04			
Increasing factors for concret $\Psi_{c}$	e	C40/50		1,08						
10		C50/60				1	,10			
Splitting failure			-							
		h /	h <sub>el</sub> <sup>3)</sup> ≥ 2,0	1,0 h	et	h/h <sub>ef</sub>				
Edge distance c <sub>cr,sp</sub> [mm] for		2,0 > h / h <sub>et</sub> <sup>3)</sup> > 1,3		4,6 h <sub>et</sub> - 1,8 h		1,3				
		h/)	h <sub>et</sub> <sup>3)</sup> ≤ 1,3	2,26 ł	1 <sub>el</sub>	1	1,0∙h <sub>ef</sub>	2,26 <sup>.</sup> h <sub>e</sub>	C <sub>cr,s</sub>	
Axial distance		S <sub>cr,sp</sub>	[mm]			2	C <sub>cr,sp</sub>			
Partial safety factor (dry and	wet concrete)	$\gamma_{Mp} = \gamma_M$	$c = \gamma_{Msp}^{1}$	1,84)			,8 <sup>4)</sup>			
Partial safety factor (flooded l	oore hole)	$\gamma_{Mp} = \gamma_M$	$_{c} = \gamma_{Msp}^{1}$	2,1	5)		not adn	not admissible		
	national regulations	ve ancho	rage depth	I						
<ul> <li><sup>2)</sup> Explanations see se</li> <li><sup>3)</sup> h = concrete member</li> <li><sup>4)</sup> The partial safety fa</li> </ul>	thickness, $h_{ef} = effectivector \gamma_2 = 1.2 is included.ctor \gamma_2 = 1.4 is included.$									
<ul> <li><sup>2)</sup> Explanations see se</li> <li><sup>3)</sup> h = concrete member</li> <li><sup>4)</sup> The partial safety fa</li> </ul>	er thickness, $h_{ef}$ = effective ctor $\gamma_2$ = 1.2 is included. ctor $\gamma_2$ = 1.4 is included.		PRO VE	E-SF for	r conc	rete				



Table 7: Design according t cracked and non-c										
Anchor size threaded rod			M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
Steel failure without lever arm				L		<b></b>		<b></b>		
Characteristic shear resistance, Steel, property class 4.6	V <sub>Rk,s</sub>	[kN]	7	12	17	31	49	71	92	112
Partial safety factor	γ <sub>Ms,V</sub> 1)					1,	67			
Characteristic shear resistance, Steel, property class 5.8	V <sub>Rk,s</sub>	[kN]	9	15	21	39	61	88	115	140
Characteristic shear resistance, Steel, property class 8.8	V <sub>Rk,s</sub>	[kN]	15	23	34	63	98	141	184	224
Partial safety factor	γ <sub>Ms,V</sub> 1)					1,	25			
Characteristic shear resistance, Stainless steel A4 and HCR, property class 50 (>M24) and 70 ( $\leq$ M24)	V <sub>Rk,s</sub>	[kN]	13	20	30	55	86	124	115	140
Partial safety factor	$\gamma_{\rm Ms,V}$ 1)				1,	56			2,	38
Steel failure with lever arm										
Characteristic bending moment, Steel, property class 4.6	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	15	30	52	133	260	449	666	900
Partial safety factor	$\gamma_{\rm Ms,V}$ 1)					1,	67			
Characteristic bending moment, Steel, property class 5.8	$M^0{}_{Rk,s}$	[Nm]	19	37	65	166	324	560	833	1123
Characteristic bending moment, Steel, property class 8.8	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	30	60	105	266	519	896	1333	1797
Partial safety factor	$\gamma_{\rm Ms,V}$ 1)					1,	25			
Characteristic bending moment, Stainless steel A4 and HCR, property class 50 (>M24) and 70 (≤ M24)	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	26	52	92	232	454	784	832	1125
Partial safety factor	$\gamma_{\text{Ms,V}}$ 1)				1,	56			2,	38
Concrete pry-out failure										
Factor k in equation (5.7) of Technical Report TR 029 for the design of Bonded Anchors						2	,0			
Partial safety factor	$\gamma_{Mop}$ 1)					1,5	0 2)			
Concrete edge failure										
See section 5.2.3.4 of Technical Report TR 029 for	or the desi	gn of Bon	ded Anch	ors						
Partial safety factor	γ <sub>Mo</sub> <sup>1)</sup>					1,5	0 2)			
<sup>1)</sup> In absence of other national regulations <sup>2)</sup> The partial safety factor $\gamma_2 = 1.0$ is include	ed.									
G&B Fissaggi Injection system				SF fo	or con	crete		٨٣	nex 1	1
Application with threaded rod Design acc. to TR 029, Characteristic values for shear loads in cracked and non-cracked concrete under static and quasi-static action								AI		•



	gn according cracked conc									loads	in	
Anchor size reinforcing b	ar			Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure						<b></b>						
Characteristic tension resis reinforcing bar according to		N <sub>Rk,s</sub>	[kN]					$A_s \times f_{uk}^7$	)			
Partial safety factor		γ <sub>Ms,N</sub> 1)				TR 0	29 Secti	on 3.2.2	.2, Eq. 3	3.3a <sup>7)</sup>		
Combined pull-out and co	oncrete cone failure											
Characteristic bond resistar	nce in uncracked cond	crete C20/28	5									
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm <sup>2</sup> ]	8,5	10	10	10	10	10	9,0	8,0	7,0
40℃/24℃	flooded bore hole	τ <sub>Rk,ucr</sub>	[N/mm <sup>2</sup> ]	6,0	7,5	7,5	7,5	7,5		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\rm Rk,ucr}$	[N/mm <sup>2</sup> ]	6,5	7,5	7,5	7,5	7,5	7,5	7,0	6,0	5,0
80℃/50℃	flooded bore hole	$\tau_{\rm Rk,ucr}$	[N/mm <sup>2</sup> ]	4,5	5,5	5,5	5,5	5,5		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\rm Rk,ucr}$	[N/mm <sup>2</sup> ]	4,5	5,5	5,5	5,5	5,5	5,5	5,0	4,5	4,0
120°C/72°C	flooded bore hole	$\tau_{\rm Rk,ucr}$	[N/mm <sup>2</sup> ]	3,5	4,0	4,0	4,0	4,0		not adr	nissible	
		C30/37						1,04				
Increasing factors for concr	ete	C40/50						1,08				
Ψc		C50/60						1,10				
Splitting failure												
		h/	h <sub>ef</sub> <sup>3)</sup> ≥ 2,0		1,0 h <sub>ef</sub>		h/h <sub>ef</sub> 7					
	-					_	2,0 -			_		
Edge distance c <sub>cr,sp</sub> [mm] fo	r -	2,0 > h /	h <sub>ef</sub> <sup>3)</sup> > 1,3	4,6	h <sub>ef</sub> - 1,8	h	1,3 -					
		h /	h <sub>ef</sub> <sup>3)</sup> ≤ 1,3		2,26 h <sub>et</sub>		+		1,0∙h <sub>ef</sub>	2,26		cr,sp
Axial distance		S <sub>cr,sp</sub>	[mm]					2 c <sub>cr,sp</sub>	1,0 Het	2,20	riet	
Partial safety factor (dry and	d wet concrete)	$\gamma_{Mp} = \gamma_{Mc} =$	γ <sub>Msp</sub> <sup>1)</sup>	1,5 <sup>4)</sup>				1,	8 <sup>5)</sup>			
Partial safety factor (flooded	d bore hole)	$\gamma_{Mp} = \gamma_{Mc} =$	γ <sub>Msp</sub> <sup>1)</sup>			2,1 <sup>6)</sup>				not adr	nissible	
<sup>1)</sup> In absence of othe <sup>2)</sup> Explanations see = <sup>3)</sup> h = concrete mem <sup>4)</sup> The partial safety <sup>5)</sup> The partial safety <sup>6)</sup> The partial safety <sup>7)</sup> $f_{uk}$ , $f_{yk}$ according to Attend chapter 4.2 for do	section 1.2 ber thickness, $h_{ef} =$ factor $\gamma_2 = 1.0$ is inc factor $\gamma_2 = 1.2$ is inc factor $\gamma_2 = 1.4$ is inc prelevant Technica	effective a cluded. cluded. cluded. luded. I Specifica	tion for the		rcing ba	ar						
Attend chapter 4.2 for de	esign of post-installe	ed rebar as	s anchor									
G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete Application with reinforcing bar Annex 12												
Characteristic values for		FR 029, I concrete i	under s	tatic an	d quas	i-static	action					



Anchor size reinforcing bar Steel failure Characteristic tension resistance, reinforcing bar according to Annex Partial safety factor		N <sub>Rk,s</sub> γ <sub>Ms,N</sub> <sup>1)</sup>	[kN]	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Characteristic tension resistance, reinforcing bar according to Annex Partial safety factor		~~~*-	[kN]							
reinforcing bar according to Annex Partial safety factor		~~~*-	[kN]							
	e cone failure	γ <sub>Ms,N</sub> 1)					$A_s x f_{uk}^{6)}$			
	e cone failure		•		TR	029 Sect	ion 3.2.2.	2, Eq. 3.3	a <sup>6)</sup>	
Combined pull-out and concrete										
Characteristic bond resistance in c	cracked concrete C20/2	25								
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	4,5	4,5	4,5	4,5	4,5	5,0	5,0
40°C/24°C	flooded bore hole	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	4,5	4,5	4,5		not adn	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	3,0	3,0	3,0	3,0	3,0	4,0	4,0
80°C/50°C	flooded bore hole	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	3,0	3,0	3,0		not adn	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	2,5	2,5	2,5	2,5	2,5	3,0	3,0
120°C/72°C	flooded bore hole	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	2,5	2,5	2,5		not adn	nissible	
Increasing factors for concrete		C30/37					1,04			
Increasing factors for concrete		C40/50					1,08			
Ψc		C50/60	i				1,10			
Splitting failure										
		h	/ h <sub>ef</sub> <sup>3)</sup> ≥ 2,0	1,0	h <sub>et</sub>	h/h <sub>ef</sub>				
Edge distance $c_{\text{cr,sp}}$ [mm] for		2,0 > h	/ h <sub>ef</sub> <sup>3)</sup> > 1,3	4,6 h <sub>et</sub> -	• 1,8 h	1,3			\	
		h	/ h <sub>ef</sub> <sup>3)</sup> ≤ 1,3	2,26	h <sub>et</sub>	-	1,0	)∙h <sub>ef</sub> 2	2,26 <sup>.</sup> h <sub>ef</sub>	• c <sub>cr,sp</sub>
Axial distance		S <sub>cr,sp</sub>	[mm]				2 c <sub>cr,sp</sub>			
Partial safety factor (dry and wet c	oncrete)		$_{\rm lc} = \gamma_{\rm Msp}^{1}$				1,8 <sup>4)</sup>			
Partial safety factor (flooded bore I		$\gamma_{Mp}=\gamma_M$	$_{\rm Mc} = \gamma_{\rm Msp}^{1)}$		2,1 <sup>5)</sup>			not adr	nissible	
<ol> <li>In absence of other national equations are section</li> <li>Explanations see section</li> <li>h = concrete member thi</li> <li>The partial safety factor</li> <li>The partial safety factor</li> <li>f<sub>uk</sub>, f<sub>yk</sub> according to relev</li> <li>Attend chapter 4.2 for design c</li> </ol>	n 1.2 ickness, $h_{ef}$ = effecti $\gamma_2$ = 1.2 is included. $\gamma_2$ = 1.4 is included. ant Technical Speci	fication f	for the reinf		ar					
G&B Fissaggi Injectio	Application with Design acc.	reinforci to TR 02	ing bar 29,					Ar	nnex 1	3



Table 9: Design accordi and non-cracke										in cra	cked
Anchor size reinforcing bar			Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure without lever arm											
Characteristic shear resistance, reinforcing bar according to Annex 4	V <sub>Rk,s</sub>	[kN]				0,5	0 x A <sub>s</sub> x f	; 3) uk			
Partial safety factor	γ <sub>Ms,V</sub> 1)				TR 02	9 Sectio	n 3.2.2.2	, Eq. 3.3	b+c 3)		
Steel failure with lever arm											
Characteristic bending moment, reinforcing bar according to Annex 4	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]				1.2	2 ·W <sub>el</sub> · f <sub>u</sub>	3) Ik			
Partial safety factor	γ <sub>Ms</sub> ,v <sup>1)</sup>		TR 029 Section 3.2.2.2, Eq. 3.3 b+c <sup>3)</sup>								
Concrete pry-out failure											
Factor k in equation (5.7) of Technical Repo TR 029 for the design of bonded anchors	rt		2,0								
Partial safety factor	γ <sub>Mcp</sub> <sup>1)</sup>						1,50 <sup>2)</sup>				
Concrete edge failure											
See section 5.2.3.4 of Technical Report TR	029 for the d	esign of I	Bonded A	Anchors							
Partial safety factor	γ <sub>Mc</sub> <sup>1)</sup>						1,50 <sup>2)</sup>				
<sup>1)</sup> In absence of other national regulations <sup>2)</sup> The partial safety factor $\gamma_2 = 1.0$ is included. <sup>3)</sup> f <sub>uk</sub> , f <sub>yk</sub> according to relevant Technical Specification for the reinforcing bar Attend chapter 4.2 for design of post-installed rebar as anchor											

Application with reinforcing bar Design acc. to TR 029, Characteristic values for shear loads in cracked and non-cracked concrete under static and quasi-static action Annex 14



Anchor size threaded rod				M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
Steel failure											
Characteristic tension resist Steel, property class 4.6	tance,	N <sub>Rk,s</sub>	[kN]	15	23	34	63	98	141	184	224
Partial safety factor		γ <sub>Ms,N</sub> <sup>1)</sup>					2	,0			
Characteristic tension resist	tance,	N <sub>Rk,s</sub>	[kN]	18	29	42	78	122	176	230	280
Steel, property class 5.8 Characteristic tension resist	tance,			29	46	67	125	196	282	368	449
Steel, property class 8.8	··· ·· · · ·	N <sub>Rk,s</sub>	[kN]	29	40	67			282	368	449
Partial safety factor Characteristic tension resist	tanco	γ <sub>Ms,N</sub> <sup>1)</sup>	1				1,	50			
Stainless steel A4 and HCF property class 50 (>M24) at	<b>λ</b> ,	N <sub>Rk,s</sub>	[kN]	26	41	59	110	171	247	230	281
Partial safety factor		γ <sub>Ms,N</sub> <sup>1)</sup>				1,	87			2,3	86
Combined pull-out and co	oncrete failure										
Characteristic bond resistar	nce in non-cracked concrete	e C20/25									
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm <sup>2</sup> ]	8,5	10,0	10,0	10,0	10,0	9,5	8,5	7,5
40℃/24℃	flooded bore hole	$\tau_{Rk,ucr}$	[N/mm <sup>2</sup> ]	6,0	7,5	7,5	7,5		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm <sup>2</sup> ]	6,5	7,5	7,5	7,5	7,5	7,0	6,5	5,5
80°C/50°C	flooded bore hole	$\tau_{Rk,ucr}$	[N/mm²]	4,5	5,5	5,5	5,5		not admis		
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm <sup>2</sup> ]	4,5	5,5	5,5	5,5	5,5	5,5	4,5	3,5
120°C/72°C	flooded bore hole	$\tau_{Rk,ucr}$	[N/mm <sup>2</sup> ]	3,5	4,0	4,0	4,0		not adr	nissible	
Increasing factors for concr	ete	C30/37					,	04			
$\psi_c$		C40/50 C50/60					,	08 10			
Factor according to CEN/TS	5 1992-4-5 Section 6.2.2.3	k <sub>8</sub>	[-]				10				
Concrete cone failure											
Factor according to CEN/TS	5 1992-4-5 Section 6.2.3.1	k <sub>ucr</sub>	[-]				1(	),1			
Edge distance		C <sub>or,N</sub>	[mm]				1,5	h <sub>et</sub>			
Axial distance		S <sub>cr,N</sub>	[mm]				3,0	h <sub>et</sub>			
Splitting failure											
		h/	h <sub>ef</sub> <sup>3)</sup> ≥ 2,0	1,0	0 h <sub>et</sub>		1/h <sub>ef</sub> ]		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
Edge distance c <sub>cr,sp</sub> [mm] for	r	2,0 > h /	h <sub>ef</sub> <sup>3)</sup> > 1,3	4,6 h <sub>e</sub>	ւ - 1,8 h		2,0		$\searrow$		
		h /	h <sub>ef</sub> <sup>3)</sup> ≤ 1,3	2,2	?6 h <sub>ef</sub>	1				c <sub>c</sub>	r.sp
Axial distance		S <sub>ar,sp</sub>	[mm]				2 0	1,0 h	<sub>ef</sub> 2,26	i∙h <sub>ef</sub>	
Partial safety factor (dry and	d wet concrete)	$\gamma_{Mp} = \gamma_{Mc}$	× · •	1,5 <sup>4)</sup>				1,8 <sup>5)</sup>			
Partial safety factor (flooded		$\gamma_{Mp} = \gamma_{Mc}$			2,	1 <sup>6)</sup>			not adr	nissible	
<ol> <li>In absence of other na</li> <li>Explanations see section</li> <li>h = concrete member t</li> </ol>	on 1.2			<sup>5)</sup> The	e partial e partial e partial	safety f	factor y <sub>2</sub>	= 1.2 is	s includ	ed.	
G&B Fissaggi Inj	ection system GE Application wi Design according	th threade	ed rod	E-SF	for co	oncre	te		Anr	nex 1	5

Z55531.13

Characteristic values for tension loads in non-cracked concrete under static and quasi-static action



Anchor size threaded rod				M 12	M 16	M 20	M24	M27	M30
Steel failure									
Characteristic tension resista Steel, property class 4.6	nce,	N <sub>Rk,s</sub>	[kN]	34	63	98	141	184	224
Partial safety factor		YMs,N <sup>1</sup>				2	.0		
Characteristic tension resista	nce,	N <sub>Rk,s</sub>	[kN]	42	78	122	176	230	280
Steel, property class 5.8 Characteristic tension resista	ince.								
Steel, property class 8.8		N <sub>Rk,s</sub>	[kN]	67	125	196	282	368	449
Partial safety factor	0.11	γ <sub>Ms,N</sub> 1)				1,	50		
Characteristic tension resista HCR, property class 50 (>M2		N <sub>Rk,s</sub>	[kN]	59	110	171	247	230	281
Partial safety factor		γ <sub>Ms,N</sub> 1)			1,	87		2,8	86
Combined pull-out and cor	crete failure	•	•						
Characteristic bond resistance	e in cracked concrete C20/25	5							
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	4,5	4,5	4,5	4,5	5,0	5,0
40°C/24°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	4,5	4,5		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\rm Rk,cr}$	[N/mm <sup>2</sup> ]	3,5	3,5	3,5	3,5	4,0	4,0
80°C/50°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	3,5	3,5		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	2,5	2,5	2,5	2,5	3,0	3,0
120℃/72℃	flooded bore hole	$\tau_{\text{Rk,cr}}$	[N/mm <sup>2</sup> ]	2,5	2,5		not adr	nissible	
Increasing factors for concret		C30/37				1,	04		
Increasing factors for concret $\Psi_c$	le	C40/50				1,	08		
		C50/60				1,	10		
Factor according to CEN/TS	1992-4-5 Section 6.2.2.3	k <sub>8</sub>	[-]			7	,2		
Concrete cone failure									
Factor according to CEN/TS	1992-4-5 Section 6.2.3.1	k <sub>cr</sub>	[-]			7	,2		
Edge distance		C <sub>cr,N</sub>	[mm]			1,5	h <sub>et</sub>		
Axial distance		S <sub>cr,N</sub>	[mm]			3,0	h <sub>et</sub>		
Splitting failure			•						
		h	/ h <sub>et</sub> <sup>3)</sup> ≥ 2,0	1,0 h	ef	h/h <sub>ef</sub>			
Edge distance $c_{cr,sp}$ [mm] for		2,0 > h	/ h <sub>ef</sub> <sup>3)</sup> > 1,3	4,6 h <sub>et</sub> -	1,8 h	1,3			
		h	/ h <sub>ef</sub> <sup>3)</sup> ≤ 1,3	2,26	1 <sub>el</sub>	<u> </u>	1,0 h <sub>ef</sub>	2,26 <sup>.</sup> h <sub>ef</sub>	⁺ c <sub>cr,sp</sub>
Axial distance		S <sub>cr,sp</sub>	[mm]				or,sp		
Partial safety factor (dry and	wet concrete)	$\gamma_{Mp} = \gamma_{Mc} =$				1,	8 <sup>4)</sup>		
Partial safety factor (flooded	bore hole)	$\gamma_{Mp} = \gamma_{Mc} =$	=γ <sub>Msp</sub> <sup>1)</sup>	2,	1 <sup>5)</sup>		not adr	nissible	
<ol> <li>In absence of other r</li> <li>Explanations see sec</li> <li>h = concrete member</li> </ol>	ational regulations tion 1.2 r thickness, h <sub>ef</sub> = effective	anchorage	depth	<sup>4)</sup> The pa <sup>5)</sup> The pa	rtial safe rtial safe	ty factor $\gamma$ ty factor $\gamma$	½ = 1.2 is ½ = 1.4 is	included. included.	
G&B Fissaggi Inje	ction system GEB	OFIX PI	RO VE-S	F for c	oncre	te			16



#### Design according to CEN/TS 1992-4: Characteristic values for shear loads in Table 11: cracked and non-cracked concrete under static and quasi-static action

Anchor size threaded rod			M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
Steel failure without lever arm										
Characteristic shear resistance, Steel, property class 4.6	V <sub>Rk,s</sub>	[kN]	7	12	17	31	49	71	92	112
Partial safety factor	γ <sub>Ms,V</sub> <sup>1)</sup>					1,6	67			
Characteristic shear resistance, Steel, property class 5.8	$V_{Rk,s}$	[kN]	9	15	21	39	61	88	115	140
Characteristic shear resistance, Steel, property class 8.8	V <sub>Rk,s</sub>	[kN]	15	23	34	63	98	141	184	224
Partial safety factor	γ <sub>Ms,V</sub> 1)					1,2	25			
Characteristic shear resistance, Stainless steel A4 and HCR, property class 50 (>M24) and 70 (≤ M24)	V <sub>Rk.s</sub>	[kN]	13	20	30	55	86	124	115	140
Partial safety factor	γ <sub>Ms,V</sub> <sup>1)</sup>				1,:	56			2,3	38
Ductility factor according to CEN/TS 1992-4-5 Section 6.3.2.1	k2					0,	8			
Steel failure with lever arm										
Characteristic bending moment, Steel, property class 4.6	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	15	30	52	133	260	449	666	900
Partial safety factor	γ <sub>Ms,V</sub> 1)					1,6	67			
Characteristic bending moment, Steel, property class 5.8	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	19	37	65	166	324	560	833	1123
Characteristic bending moment, Steel, property class 8.8	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	30	60	105	266	519	896	1333	1797
Partial safety factor	γ <sub>Ms,V</sub> <sup>1)</sup>					1,2	25			
Characteristic bending moment, Stainless steel A4 and HCR, property class 50 (>M24) and 70 ( $\leq$ M24)	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	26	52	92	232	454	784	832	1125
Partial safety factor	γ <sub>Ms</sub> ,v <sup>1)</sup>				1,	56			2,	38
Concrete pry-out failure										
Factor in equation (27) of CEN/TS 1992-4-5 Section 6.3.3	k <sub>3</sub>					2,	0			
Partial safety factor	γ <sub>Mop</sub> <sup>1)</sup>					1,5	0 2)			
Concrete edge failure <sup>3)</sup>	·									
Effective length of anchor	h	[mm]				l <sub>t</sub> = min(h	<sub>ef</sub> ; 8 d <sub>nom</sub> )			
Outside diameter of anchor	d <sub>nom</sub>	[mm]	8	10	12	16	20	24	27	30
Partial safety factor	$\gamma_{Mc}^{(1)}$					1,5	0 2)			

<sup>1)</sup> In absence of other national regulations

<sup>2)</sup> The partial safety factor  $\gamma_2 = 1.0$  is included. <sup>3)</sup> See CEN/TS 1992-4-5 Section 6.3.4

## G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete

Annex 17

Application with threaded rod Design according to CEN/TS 1992-4, Characteristic values for shear loads in cracked and non-cracked concrete under static and quasi-static action



	gn according to s in non-cracke										on	
Anchor size reinforcing ba	ar			Ø8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure												
Characteristic tension resist reinforcing bar according to		N <sub>Rk,s</sub>	[kN]					A <sub>s</sub> x f <sub>uk</sub> <sup>7</sup>	)			
Partial safety factor		γ <sub>Ms,N</sub> 1)			С	EN/TS 1	1992-4-1	Section	4.4.3.1	.1, Eq. 4	7)	
Combined pull-out and co	ncrete failure											
Characteristic bond resistan	ce in non-cracked concr	ete C20/	25									
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,ucr}}$	[N/mm²]	8,5	10	10	10	10	10	9,0	8,0	7,0
40°C/24°C	flooded bore hole	$\tau_{\text{Rk,ucr}}$	[N/mm²]	6,0	7,5	7,5	7,5	7,5		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,ucr}}$	[N/mm²]	6,5	7,5	7,5	7,5	7,5	7,5	7,0	6,0	5,0
80°C/50°C	flooded bore hole	$\tau_{\text{Rk,ucr}}$	[N/mm²]	4,5	5,5	5,5	5,5	5,5		not adr	nissible	_
Temperature range II <sup>2)</sup> :	dry and wet concrete	$\tau_{\text{Rk,ucr}}$	[N/mm <sup>2</sup> ]	4,5	5,5	5,5	5,5	5,5	5,5	5,0	4,5	4,0
120°C/72°C	flooded bore hole	$\tau_{\text{Rk,ucr}}$	[N/mm <sup>2</sup> ]	3,5	4,0	4,0	4,0	4,0		not adr	nissible	
Increasing factors for concre	rto.	C30/37	r					1,04				
$\psi_c$	ele	C40/50						1,08				
Factor according to		C50/60						1,10				
CEN/TS 1992-4-5 Section 6	92-4-5 Section 6.2.2.3 K <sub>8</sub> [-]											
Concrete cone failure												
Factor according to CEN/TS 1992-4-5 Section 6	.2.3.1	k <sub>ucr</sub>	[-]					10,1				
Edge distance		C <sub>cr,N</sub>	[mm]	1,5 h <sub>ef</sub>								
Axial distance		S <sub>cr,N</sub>	[mm]					3,0 h <sub>ef</sub>				
Splitting failure			h <sub>el</sub> <sup>3)</sup> ≥ 2,0		1,0 h <sub>et</sub>		h/h <sub>ef</sub>					
Edge distance $c_{cr,sp}$ [mm] for		2,0 > h /	h <sub>ef</sub> <sup>3)</sup> > 1,3	4,6	h <sub>el</sub> - 1,8	h	1,3 -					
		h /	h <sub>ef</sub> <sup>3)</sup> ≤ 1,3	2	2,26 h <sub>ef</sub>		1		1,0 ⋅h <sub>ef</sub>	2,26	·h.,	C <sub>cr,sp</sub>
Axial distance		S <sub>cr,sp</sub>	[mm]					2 c <sub>cr,sp</sub>	., v l'et	2,20	· 'et	
Partial safety factor (dry and	wet concrete)		$r_{\rm lc} = \gamma_{\rm Msp}^{1}$	1,5 <sup>4)</sup>				1,	8 <sup>5)</sup>			
Partial safety factor (flooded	l bore hole)		$_{\rm lc} = \gamma_{\rm Msp}^{1}$			2,1 <sup>6)</sup>				not adr	nissible	
<ul> <li><sup>2)</sup> Explanations see s</li> <li><sup>3)</sup> h = concrete memb</li> <li><sup>4)</sup> The partial safety f</li> <li><sup>5)</sup> The partial safety f</li> <li><sup>6)</sup> The partial safety f</li> </ul>	r national regulations section 1.2 per thickness, $h_{ef} = efficient actor \gamma_2 = 1.0$ is include actor $\gamma_2 = 1.2$ is include actor $\gamma_2 = 1.4$ is include the relevant Technic	fective a led. led. led.			einforcir	ıg bar						
G&B Fissaggi Inje	-				SF fo	or cor	ncrete	)				
<b>G&amp;B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete</b> Application with reinforcing bar Design according to <b>CEN/TS 1992-4</b> . Characteristic values for tension loads in non-cracked concrete under static and quasi-static action									Ann	ex 18	5	



Table 12b: Desig in cra	gn according to acked concrete						es for	tensi	on loa	ds
Anchor size reinforcing	bar			Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure										
Characteristic tension resi according to Annex 4	istance, reinforcing bar	N <sub>Rk,s</sub>	[kN]				$A_s \times f_{uk}$ <sup>6)</sup>			
Partial safety factor		$\gamma_{\rm Ms,N}$ 1)			CEN/TS	5 1992-4- <sup>-</sup>	1 Section	4.4.3.1.1	, Eq. 4 <sup>6)</sup>	
Combined pull-out and	concrete failure	•								
Characteristic bond resist	ance in cracked concret	te C20/25								
Temperature range I <sup>2)</sup> :	dry and wet concrete	$\tau_{\rm Rk,cr}$	[N/mm <sup>2</sup> ]	4,5	4,5	4,5	4,5	4,5	5,0	5,0
40°C/24°C	flooded bore hole	τ <sub>Rk,cr</sub>	[N/mm²]	4,5	4,5	4,5		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	τ <sub>Rk,cr</sub>	[N/mm <sup>2</sup> ]	3,0	3,0	3,0	3,0	3,0	4,0	4,0
80°C/50°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm <sup>2</sup> ]	3,0	3,0	3,0		not adr	nissible	
Temperature range II <sup>2)</sup> :	dry and wet concrete	τ <sub>Rk,cr</sub>	[N/mm <sup>2</sup> ]	2,5	2,5	2,5	2,5	2,5	3,0	3,0
120℃/72℃	flooded bore hole	τ <sub>Rk.cr</sub>	[N/mm <sup>2</sup> ]	2,5	2,5	2,5		not adr	ı nissible	·
		C30/37					1,04			
Increasing factors for cone $\Psi_{c}$	crete	C40/50					1,08			
		C50/60	-				1,10			
Factor according to CEN/TS 1992-4-5 Section	6.2.2.3	k <sub>8</sub>	[-]				7,2			
Concrete cone failure										
Factor according to CEN/TS 1992-4-5 Section	n 6.2.3.1	k <sub>or</sub>	Ð				7,2			
Edge distance		C <sub>cr,N</sub>	[mm]				1,5 h <sub>ef</sub>			
Axial distance		S <sub>cr,N</sub>	[mm]				3,0 h <sub>ef</sub>			
Splitting failure										
		h	/ h <sub>el</sub> <sup>3)</sup> ≥ 2,0	1,4	0 h <sub>ef</sub>	h/h <sub>ef</sub>				
Edge distance $c_{cr,sp}$ [mm] f	- or	2,0 > h	/ h <sub>ef</sub> <sup>3)</sup> > 1,3	4,6 h <sub>e</sub>	<sub>i</sub> - 1,8 h	1,3 -				
	-	h	/ h <sub>ef</sub> <sup>3)</sup> ≤ 1,3	2,2	?6 h <sub>et</sub>	1		0.1		→ c <sub>cr,sp</sub>
Axial distance		S <sub>or,sp</sub>	[mm]				2 C <sub>or,sp</sub>	,0∙h <sub>ef</sub>	2,26 h <sub>ef</sub>	
Partial safety factor (dry a	nd wet concrete)	$\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{1}$					1,8 <sup>4)</sup>			
Partial safety factor (flood		$\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{1}$			2,1 <sup>5)</sup>			not adr	nissible	
<ol> <li>In absence of ott</li> <li>Explanations see</li> <li>h = concrete men</li> <li>The partial safety</li> <li>The partial safety</li> </ol>	her national regulatio	ns effective ancho luded. luded.	rage depth	rcing ba			I			
G&B Fissaggi In	jection system	GEBOFIX	PRO VE	-SF fo	r cond	crete				
Characteristic values	Applicatic Design acco s for tension loads in	on with reinforcir rding to CEN/TS cracked concre	§ 1992-4,	tic and c	quasi-sta	tic actio	n	Ar	nex 1	9



Table 13: Design according t in cracked and nor	o CEN/TS -cracked	1992 conc	-4: C reteι	harao undei	cteris r stati	stic va ic and	alues d qua	for s si-st	shear atic a	load	s I
Anchor size reinforcing bar			Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure without lever arm											
Characteristic shear resistance, reinforcing bar according to Annex 4	V <sub>RK,s</sub>	[kN]				0,50	$0 \times A_s \times f$	f <sub>uk</sub> <sup>4)</sup>			
Partial safety factor	γ <sub>Ms,V</sub> 1)			CEN	V/TS 199	92-4-1 S	Section 4	.4.3.1.1	, Eq. 5 -	+ 6 4)	
Ductility factor according to CEN/TS 1992-4-5 Section 6.3.2.1	k <sub>2</sub>						0,8				
Steel failure with lever arm											
Characteristic bending moment, reinforcing bar according to Annex 4	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]				1.2	2 ⋅W <sub>el</sub> ⋅ f	4) Jk			
Partial safety factor	γ <sub>Ms,V</sub> <sup>1)</sup>			CEN	V/TS 199	92-4-1 S	Section 4	.4.3.1.1	, Eq. 5 -	+ 6 4)	
Concrete pry-out failure											
Factor in equation (27) of CEN/TS 1992-4-5 Section 6.3.3	k <sub>3</sub>						2,0				
Partial safety factor	γ <sub>Mcp</sub> <sup>1)</sup>						1,50 <sup>2)</sup>				
Concrete edge failure <sup>3)</sup>											
Effective length of anchor	Jr.	[mm]				l <sub>1</sub> = m	nin(h <sub>ef</sub> ; 8	d <sub>nom</sub> )			
Outside diameter of anchor	d <sub>nom</sub>	[mm]	8	10	12	14	16	20	24	27	30
Partial safety factor	γ <sub>Ma</sub> <sup>1)</sup>						1,50 <sup>2)</sup>				
<sup>1)</sup> In absence of other national reg <sup>2)</sup> The partial safety factor $\gamma_2 = 1.0$ <sup>3)</sup> See CEN/TS 1992-4-5 Section 6 <sup>4)</sup> f <sub>uk</sub> , f <sub>yk</sub> according to relevant Tech Attend chapter 4.2 for design of post-installed	γ <sub>Mc</sub> <sup>1)</sup> 1,50 <sup>2)</sup> al regulations         = 1.0 is included.         etion 6.3.4         t Technical Specification for the reinforcing bar										
G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete											

Application with reinforcing bar Design according to CEN/TS 1992-4, Characteristic values for shear loads in cracked and non-cracked concrete under static and quasi-static action

Annex 20



Table 14: D	isplacen	nents for tension	loads th	readeo	d rod <sup>1</sup>	)				
Anchor size three	aded rod		М 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
Non-cracked con	crete C20	)/25	•							
40℃/24℃ <sup>2)</sup>	δ <sub>N0</sub>	[mm/(N/mm²)]	0,021	0,023	0,026	0,031	0,036	0,041	0,045	0,049
400/240	$\delta_{N\infty}$	[mm/(N/mm²)]	0,030	0,033	0,037	0,045	0,052	0,060	0,065	0,071
80°C/50°C <sup>2)</sup>	$\delta_{N0}$	[mm/(N/mm <sup>2</sup> )]	0,050	0,056	0,063	0,075	0,088	0,100	0,110	0,119
800/500	$\delta_{N\infty}$	[mm/(N/mm²)]	0,072	0,081	0,090	0,108	0,127	0,145	0,159	0,172
120℃/72℃ <sup>2)</sup>	δ <sub>N0</sub>	[mm/(N/mm²)]	0,050	0,056	0,063	0,075	0,088	0,100	0,110	0,119
1200/720	$\delta_{N\infty}$	[mm/(N/mm <sup>2</sup> )]	0,072	0,081	0,090	0,108	0,127	0,145	0,159	0,172
Cracked concret	e C20/25									
	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]					0,0	)70		
40°C/24°C <sup>2)</sup>	$\delta_{N^{\infty}}$	[mm/(N/mm <sup>2</sup> )]		-			0,1	05		
2)	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]					0,1	70		
80°C/50°C <sup>2)</sup>	$\delta_{N\infty}$	[mm/(N/mm <sup>2</sup> )]		-			0,2	245		
10000/7000 2)	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]					0,1	70		
120℃/72℃ <sup>2)</sup>	$\delta_{N_\infty}$	[mm/(N/mm <sup>2</sup> )]					0,2	245		

 $^{1)}$  Calculation of the displacement for design load Displacement for short term load =  $\delta_{N0} \cdot \tau_{Sd} / 1,4;$  Displacement for long term load =  $\delta_{N\infty} \cdot \tau_{Sd} / 1,4;$  ( $\tau_{Sd}$ : design bond strength)

<sup>2)</sup> Explanations see section 1.2

## Table 15: Displacement for shear load threaded rod <sup>3)</sup>

Anchor size thre	aded rod		M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
For non-cracked co	ncrete C20/	25	-	-	-	-	-	-		-
	δνο	[mm/(kN)]	0,06	0,06	0,05	0,04	0,04	0,03	0,03	0,03
All temperatures	$\delta_{V_\infty}$	[mm/(kN)]	0,09	0,08	0,08	0,06	0,06	0,05	0,05	0,05
For cracked concret	e C20/25									
All temperatures	δνο	[mm/(kN)]		_	0,11	0,10	0,09	0,08	0,08	0,07
Airtemperatures	$\delta_{V\infty}$	[mm/(kN)]		-	0,17	0,15	0,14	0,13	0,12	0,10
Displacement for	or short tern	nent for design load n load = $\delta_{V0} \cdot V_d / 1,4;$ load = $\delta_{V_{\infty}} \cdot V_d / 1,4;$			1	1	1	1	1	L

(V<sub>d</sub>: design shear load)

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Anchor size reinforcing bar			Ø8		Ø 12	Ø 14	Ø 16	Ø 20			
Non-cracked	concrete	e C20/25									
40°C/24°C <sup>2)</sup>	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]	0,021	0,023	0,026	0,028	0,031	0,036	0,043	0,047	0,052
	$\delta_{N_{\infty}}$	[mm/(N/mm <sup>2</sup> )]	0,030	0,033	0,037	0,041	0,045	0,052	0,061	0,071	0,075
80°C/50°C <sup>2)</sup>	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]	0,050	0,056	0,063	0,069	0,075	0,088	0,104	0,113	0,12
	$\delta_{N_\infty}$	[mm/(N/mm <sup>2</sup> )]	0,072	0,081	0,090	0,099	0,108	0,127	0,149	0,163	0,18
120°C/72°C <sup>2)</sup>	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]	0,050	0,056	0,063	0,069	0,075	0,088	0,104	0,113	0,12
	$\delta_{N\infty}$	[mm/(N/mm <sup>2</sup> )]	0,072	0,081	0,090	0,099	0,108	0,127	0,149	0,163	0,18
Cracked con	crete C2	0/25									
2)	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]						0,070			
40°C/24°C <sup>2)</sup>	δ <sub>N∞</sub>	[mm/(N/mm <sup>2</sup> )]	1	-				0,105			
9090/5090 <sup>2)</sup>	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]						0,170			
80°C/50°C <sup>2)</sup>	$\delta_{N_{\infty}}$	[mm/(N/mm <sup>2</sup> )]	1	-				0,245			
10000 /7000 <sup>2)</sup>	δ <sub>N0</sub>	[mm/(N/mm <sup>2</sup> )]						0,170			
120°C/72°C <sup>2)</sup>											
Displacem	ent for sho ent for long 1 bond stre	$[mm/(N/mm^2)]$ placement for design rt term load = $\delta_{N0} \cdot \tau_S$ g term load = $\delta_{N\infty} \cdot \tau_S$ ength) tion 1.2	<sub>3d</sub> / 1,4;	-				0,245			
Displacem Displacem (t <sub>Sd</sub> : design <sup>2)</sup> Explanation	of the disp ent for sho ent for long n bond stre ns see sec	placement for design rt term load = $\delta_{N0} \cdot \tau_S$ g term load = $\delta_{N\infty} \cdot \tau_S$ ength) tion 1.2	<sub>3d</sub> / 1,4;	Ø 10	Ø 12	Ø 14	Ø 16	0,245 Ø <b>20</b>	Ø 25	Ø 28	Ø 3
Displacem Displacem ( $ au_{Sd}$ : design <sup>2)</sup> Explanation	of the dis ent for sho ent for long n bond stre ns see sec reinforci	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2	<sub>Sd</sub> / 1,4; d / 1,4;	Ø 10	Ø 12	Ø 14	Ø 16		Ø 25	Ø 28	Ø 3
Displacem Displacem ( $ au_{Sd}$ : design <sup>2)</sup> Explanation Anchor size	of the dis ent for sho ent for long n bond stre ns see sec reinforci	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2	<sub>Sd</sub> / 1,4; d / 1,4;	Ø <b>10</b> 0,05	Ø <b>12</b> 0,05	Ø 14 0,04	Ø <b>16</b> 0,04		Ø <b>25</b> 0,03	Ø <b>28</b> 0,03	
Displacem Displacem ( $ au_{Sd}$ : design <sup>2)</sup> Explanation Anchor size For non-cracke	of the disp ent for sho ent for long h bond stre ns see sec reinforcia d concrete	placement for design rt term load = $\delta_{N0} \cdot \tau_S$ g term load = $\delta_{N\infty} \cdot \tau_S$ ength) tion 1.2 ng bar c C20/25	Ø8					Ø 20			0,03
Displacem Displacem (τ <sub>Sd</sub> : design	of the dispect for sho ent for long to bond stree the see sec reinforcial d concrete $\delta_{V0}$ $\delta_{V\infty}$	placement for design rt term load = $\delta_{N0} \cdot \tau_S$ g term load = $\delta_{N\infty} \cdot \tau_S$ ength) tion 1.2 ng bar e C20/25 [mm/(kN)] [mm/(kN)]	Ø <b>8</b> 0,06	0,05	0,05	0,04	0,04	Ø <b>20</b> 0,04	0,03	0,03	Ø <b>3</b> 0,03 0,04
Displacem Displacem (T <sub>Sd</sub> : design <sup>2)</sup> Explanation Anchor size For non-cracke All emperatures For cracked co	of the dispect for sho ent for long to bond stree the see sec reinforcial d concrete $\delta_{V0}$ $\delta_{V\infty}$	placement for design rt term load = $\delta_{N0} \cdot \tau_S$ g term load = $\delta_{N\infty} \cdot \tau_S$ ength) tion 1.2 ng bar e C20/25 [mm/(kN)] [mm/(kN)]	Ø <b>8</b> 0,06	0,05	0,05	0,04	0,04	Ø <b>20</b> 0,04	0,03	0,03	0,03
Displacem Displacem ( $\tau_{Sd}$ : design <sup>2)</sup> Explanation Anchor size For non-cracke All emperatures For cracked co All emperatures	of the dispersive of the disp	placement for design rt term load = $\delta_{N0} \cdot \tau_S$ g term load = $\delta_{N\infty} \cdot \tau_S$ ength) tion 1.2 ng bar c 220/25 [mm/(kN)] [mm/(kN)] 0/25	Ø 8 0,06 0,09	0,05	0,05 0,08	0,04 0,06	0,04 0,06	Ø <b>20</b> 0,04 0,05	0,03 0,05	0,03 0,04	0,03
Displacem Displacem ( $\tau_{Sd}$ : design <sup>2)</sup> Explanation Anchor size For non-cracke All emperatures For cracked co All emperatures <sup>3)</sup> Calculation Displacem	of the dispect for sho ent for long a bond stree as see sec reinforcia d concrete $\delta_{V0}$ $\delta_{V\infty}$ ncrete C20 $\delta_{V\infty}$ of the dispect for sho ent for long	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2 <b>ng bar</b> <b>c</b> C20/25 [mm/(kN)] [mm/(kN)] D/25 [mm/(kN)] placement for design rt term load = $\delta_{V0} \cdot V_s$ g term load = $\delta_{V\infty} \cdot V_s$	Ø 8 0,06 0,09 load d / 1,4;	0,05	0,05 0,08 0,11	0,04 0,06 0,11	0,04 0,06 0,10	Ø <b>20</b> 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,03
Displacem Displacem ( $\tau_{Sd}$ : design <sup>2)</sup> Explanation Anchor size For non-cracke All emperatures For cracked co All emperatures <sup>3)</sup> Calculation Displacem Displacem	of the dispect for sho ent for long a bond stree as see sec reinforcia d concrete $\delta_{V0}$ $\delta_{V\infty}$ ncrete C20 $\delta_{V\infty}$ of the dispect for sho ent for long	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2 <b>ng bar</b> <b>c</b> C20/25 [mm/(kN)] [mm/(kN)] D/25 [mm/(kN)] placement for design rt term load = $\delta_{V0} \cdot V_s$ g term load = $\delta_{V\infty} \cdot V_s$	Ø 8 0,06 0,09 load d / 1,4;	0,05	0,05 0,08 0,11	0,04 0,06 0,11	0,04 0,06 0,10	Ø <b>20</b> 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,03 0,04 0,06
Displacem Displacem ( $\tau_{Sd}$ : design <sup>2)</sup> Explanation Anchor size For non-cracke All emperatures For cracked co All emperatures <sup>3)</sup> Calculation Displacem Displacem	of the dispect for sho ent for long a bond stree as see sec reinforcia d concrete $\delta_{V0}$ $\delta_{V\infty}$ ncrete C20 $\delta_{V\infty}$ of the dispect for sho ent for long	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2 <b>ng bar</b> <b>c</b> C20/25 [mm/(kN)] [mm/(kN)] D/25 [mm/(kN)] placement for design rt term load = $\delta_{V0} \cdot V_s$ g term load = $\delta_{V\infty} \cdot V_s$	Ø 8 0,06 0,09 load d / 1,4;	0,05	0,05 0,08 0,11	0,04 0,06 0,11	0,04 0,06 0,10	Ø <b>20</b> 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,03
Displacem Displacem ( $ au_{Sd}$ : design 2) Explanation Anchor size For non-cracke All emperatures For cracked co All memperatures 3) Calculation Displacem Displacem	of the dispect for sho ent for long a bond stree as see sec reinforcia d concrete $\delta_{V0}$ $\delta_{V\infty}$ ncrete C20 $\delta_{V\infty}$ of the dispect for sho ent for long	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2 <b>ng bar</b> <b>c</b> C20/25 [mm/(kN)] [mm/(kN)] D/25 [mm/(kN)] placement for design rt term load = $\delta_{V0} \cdot V_s$ g term load = $\delta_{V\infty} \cdot V_s$	Ø 8 0,06 0,09 load d / 1,4;	0,05	0,05 0,08 0,11	0,04 0,06 0,11	0,04 0,06 0,10	Ø <b>20</b> 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,03 0,04 0,06
Displacem Displacem ( $ au_{sd}$ : design <sup>2)</sup> Explanation Anchor size For non-cracke All emperatures For cracked co All emperatures <sup>3)</sup> Calculation Displacem Displacem	of the dispect for sho ent for long a bond stree as see sec reinforcia d concrete $\delta_{V0}$ $\delta_{V\infty}$ ncrete C20 $\delta_{V\infty}$ of the dispect for sho ent for long	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2 <b>ng bar</b> <b>c</b> C20/25 [mm/(kN)] [mm/(kN)] D/25 [mm/(kN)] placement for design rt term load = $\delta_{V0} \cdot V_s$ g term load = $\delta_{V\infty} \cdot V_s$	Ø 8 0,06 0,09 load d / 1,4;	0,05	0,05 0,08 0,11	0,04 0,06 0,11	0,04 0,06 0,10	Ø <b>20</b> 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,03
Displacem Displacem ( $\tau_{Sd}$ : design <sup>2)</sup> Explanation Anchor size For non-cracke All emperatures For cracked co All emperatures <sup>3)</sup> Calculation Displacem Displacem	of the dispect for sho ent for long a bond stree as see sec reinforcia d concrete $\delta_{V0}$ $\delta_{V\infty}$ ncrete C20 $\delta_{V\infty}$ of the dispect for sho ent for long	placement for design rt term load = $\delta_{N0} \cdot \tau_s$ g term load = $\delta_{N\infty} \cdot \tau_s$ ength) tion 1.2 <b>ng bar</b> <b>c</b> C20/25 [mm/(kN)] [mm/(kN)] D/25 [mm/(kN)] placement for design rt term load = $\delta_{V0} \cdot V_s$ g term load = $\delta_{V\infty} \cdot V_s$	Ø 8 0,06 0,09 load d / 1,4;	0,05	0,05 0,08 0,11	0,04 0,06 0,11	0,04 0,06 0,10	Ø <b>20</b> 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,03 0,04 0,06

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## Design according to TR 045; Design under seismic action

The decision of the selection of the seismic performance category is in the responsibility of each individual Member State.

Furthermore, the values of a<sub>g</sub> · S assigned to the seismicity levels may be different in the National Annexes to EN 1998-1:2004 (EC8) compared to the values given in Table 18.

The recommended category C1 and C2 given in Table 18 are given in the case that no National requirements are defined.

## Table 18: Recommended seismic performance categories for anchors

Se	ismicity level <sup>a)</sup>	Importance Class acc. to EN 1998-1:2004, 4.2.5						
a <sub>g</sub> - S <sup>c)</sup>		I	Ш	III	IV			
Very low <sup>b)</sup>	a <sub>g</sub> ⋅S ≤ 0,05 g	No additional requirement						
Low <sup>b)</sup>	0,05 g < a <sub>g</sub> ·S ≤ 0,1 g	C1	C1 <sup>d)</sup> c	C2				
	a <sub>g</sub> ⋅S > 0,1 g	C1						

a) The values defining the seismicity levels may be found in the National Annex of EN 1998-1.

b) Definition according to EN 1998-1:2004, 3.2.1.

c) a<sub>g</sub> = Design ground acceleration on Type A ground (EN 1998-1: 2004, 3.2.1),

S = Soil factor (see e.g. EN 1998-1: 2004, 3.2.2).

d) C1 attachments of non-structural elements

e) C2 for connections between structural elements of primary and/or secondary seismic members

## Calculation of characteristic seismic resistance Rk.seis

Tension load:	$R_{k,seis} = \alpha_{gap} \cdot \alpha_{seis} \cdot \alpha_{N,seis} \cdot R^{o}_{k}$
	with $R_{k}^{0} = N_{Rk,s}$ , $N_{Rk,p}$ , $N_{Rk,c}$ , $N_{Rk,sp}$ (calculation according to CEN/TS 1992-4 or TR029) $\alpha_{N,seis} =$ see Table 19 or Table 20 for $N_{Rk,s}$ and $N_{Rk,p}$ $\alpha_{N,seis} =$ 1,0 for $N_{Rk,c}$ and $N_{Rk,sp}$ $\alpha_{gap} =$ see Table 21 $\alpha_{seis} =$ see Table 21
Shear load:	$\mathbf{R}_{k,seis} = \alpha_{gap} \cdot \alpha_{seis} \cdot \alpha_{V,seis} \cdot \mathbf{R}^{0}_{k}$
	with $R_{k}^{0} = V_{Rk,s}$ , $V_{Rk,c}$ , $V_{Rk,cp}$ (calculation according to CEN/TS 1992-4 or TR029) $\alpha_{V,seis} =$ see Table 19 or Table 20 for $V_{Rk,s}$ $\alpha_{V,seis} =$ 1,0 for $V_{Rk,c}$ and $V_{Rk,cp}$ $\alpha_{gap} =$ see Table 21 $\alpha_{seis} =$ see Table 21

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## G&B Fissaggi Injection system GEBOFIX PRO VE-SF for concrete

Annex 23

Design according to TR 045; Design under seismic action



Table 19: Reduction factors $\alpha_{N,seis}$ and $\alpha_{V,seis}$ for seismic design category C1 for threaded rods										
Anchor si	ze threaded rods			M 12	M 1	6 N	/ 20	M24	M 27	M 30
Tension lo	oad						<b>I</b>			
Steel failure	e (N <sub>Bks</sub> )	$\alpha_{N,seis}$	[-]				1,0	)		
	oull-out and concrete failure (N <sub>Rk,p</sub> )	α <sub>N,seis</sub>	[-]	0,68	0,6	8 (	0,68	0,69	0,69	0,69
Shear load		a n <sub>a</sub> pera		,	,		,			
Steel failure			0,70	0						
Steel failure without lever arm (V <sub>Rk,s</sub> )       α <sub>V,seis</sub> [-]       0,70         Table 20: Reduction factors α <sub>N,seis</sub> and α <sub>V,seis</sub> For seismic design category C1 for reinforcing bar										
Anchor si	ze reinforcing bar			Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Tension lo										
Steel failure		$\alpha_{N,seis}$	[-]				1,0			
	oull-out and concrete failure (N <sub>Rk,p</sub> )		[-]	0,68	0,68	0,68	0,68	0,69	0,69	0,69
Shear loa	1	$\alpha_{N,seis}$	111	0,00	0,00	0,00	0,00	0,00	0,00	0,00
	e without lever arm (V <sub>Rk.s</sub> )	$\alpha_{V,seis}$	[-]				0,70			
Loading	Failure modes				α <sub>ga</sub>	p	α <sub>seis</sub> - S faste		α <sub>seis</sub> - Fa gro	
	Steel failure				1,0		1,0	)	1,0	
	Pull-out failure					1,0 1,0		)	0,85	
Tension	Combined pull-out and concrete failure				1,0 1,0		,		35	
	Concrete cone failure					1,0 0,85				
	Splitting failure					1,0 1,0				
	Steel failure without lever arm				0,5 <sup>1)</sup> 1,0 NPD <sup>2)</sup> NPD					
Shear	Steel failure with lever arm Concrete edge failure				0,5 <sup>1)</sup> 1,0					
	Concrete pry-out failure					0,5 <sup>1)</sup> 0,85			0,2	
$\alpha_{gap} = 1$	itation for size of the clearance hole 1,0 in case of no clearance between formance Determined				,			1		
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