

European Technical Approval ETA-10/0333

Handelsbezeichnung <i>Trade name</i>	Powers Injektionssystem V12 für Beton Powers Injection System V12 for concrete
Zulassungsinhaber Holder of approval	Powers Fasteners Australasia Pty Ltd. 205 Abbotts Road Dandenong SOUTH VICTORIA 3175 AUSTRALIEN
Zulassungsgegenstand und Verwendungszweck Generic type and use of construction product	Verbunddübel mit Ankerstange zur Verankerung im Beton Bonded Anchor with Anchor rod for use in concrete
or construction product	
Geltungsdauer: vom Validity: from	20 June 2013
bis <i>to</i>	15 May 2018
Herstellwerk Manufacturing plant	Powers Fasteners Australasia Pty Ltd., Plant1 Germany

English translation prepared by DIBt - Original version in German language

Diese Zulassung umfasst	
This Approval contains	

Diese Zulassung ersetzt This Approval replaces



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I LEGAL BASES AND GENERAL CONDITIONS

- 1 This European technical approval is issued by Deutsches Institut für Bautechnik in accordance with:
 - Council Directive 89/106/EEC of 21 December 1988 on the approximation of laws, regulations and administrative provisions of Member States relating to construction products¹, modified by Council Directive 93/68/EEC² and Regulation (EC) N° 1882/2003 of the European Parliament and of the Council³;
 - Gesetz über das In-Verkehr-Bringen von und den freien Warenverkehr mit Bauprodukten zur Umsetzung der Richtlinie 89/106/EWG des Rates vom 21. Dezember 1988 zur Angleichung der Rechts- und Verwaltungsvorschriften der Mitgliedstaaten über Bauprodukte und anderer Rechtsakte der Europäischen Gemeinschaften (Bauproduktengesetz - BauPG) vom 28. April 1998⁴, as amended by Article 2 of the law of 8 November 2011⁵;
 - Common Procedural Rules for Requesting, Preparing and the Granting of European technical approvals set out in the Annex to Commission Decision 94/23/EC⁶;
 - Guideline for European technical approval of "Metal anchors for use in concrete Part 5: Bonded anchors", ETAG 001-05.
- 2 Deutsches Institut für Bautechnik is authorized to check whether the provisions of this European technical approval are met. Checking may take place in the manufacturing plant. Nevertheless, the responsibility for the conformity of the products to the European technical approval and for their fitness for the intended use remains with the holder of the European technical approval.
- 3 This European technical approval is not to be transferred to manufacturers or agents of manufacturers other than those indicated on page 1, or manufacturing plants other than those indicated on page 1 of this European technical approval.
- 4 This European technical approval may be withdrawn by Deutsches Institut für Bautechnik, in particular pursuant to information by the Commission according to Article 5(1) of Council Directive 89/106/EEC.
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- 6 The European technical approval is issued by the approval body in its official language. This version corresponds fully to the version circulated within EOTA. Translations into other languages have to be designated as such.
- ¹ Official Journal of the European Communities L 40, 11 February 1989, p. 12
- Official Journal of the European Communities L 220, 30 August 1993, p. 1
- ³ Official Journal of the European Union L 284, 31 October 2003, p. 25
- Bundesgesetzblatt Teil I 1998, p. 812
- ⁵ Bundesgesetzblatt Teil I 2011, p. 2178

Official Journal of the European Communities L 17, 20 January 1994, p. 34



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II SPECIFIC CONDITIONS OF THE EUROPEAN TECHNICAL APPROVAL

1 Definition of product and intended use

1.1 Definition of the construction product

The "Powers Injection system V12 for concrete" is a bonded anchor consisting of a cartridge with Powers injection mortar V12 and a steel element. The steel elements are commercial threaded rods according to Annex 3 in the range of M8 to M30 or reinforcing bar according to Annex 4 in the range of diameter 8 to 32 mm.

The steel element is placed into a drilled hole filled with injection mortar and is anchored via the bond between metal part, injection mortar and concrete.

An illustration of the product and intended use is given in Annexes 1 and 2.

1.2 Intended use

The anchor is intended to be used for anchorages for which requirements for mechanical resistance and stability and safety in use in the sense of the Essential Requirements 1 and 4 of Council Directive 89/106 EEC shall be fulfilled and failure of anchorages made with these products would cause risk to human life and/or lead to considerable economic consequences. Safety in case of fire (Essential Requirement 2) is not covered in this European technical approval.

The anchor is to be used only for anchorages subject to static or quasi-static loading in reinforced or unreinforced normal weight concrete of strength classes C20/25 at minimum and C50/60 at most according to EN 206:2000-12.

The anchor may be used in cracked and non-cracked concrete.

The anchor may also be used under seismic action for performance category C1 according to Annex 23.

The anchor may be installed in dry or wet concrete.

The anchor sizes diameter 8 mm to 16 mm may also be installed in flooded holes.

The anchor may be used in the following temperature ranges:

Temperature range I:	-40 °C to +40 °C	(max long term temperature +24 °C and
		max short term temperature +40 °C)
Temperature range II:	-40 °C to +80 °C	(max long term temperature +50 °C and
		max short term temperature +80 °C)
Temperature range III:	-40 °C to +120 °C	(max long term temperature +72 °C and
		max short term temperature +120 °C)

Elements made of zinc coated steel:

The element made of zinc plated or hot dip galvanised steel may only be used in structures subject to dry internal conditions.

Elements made of stainless steel:

The element made of stainless steel 1.4401, 1.4404 or 1.4571 may be used in structures subject to dry internal conditions and also in structures subject to external atmospheric exposure (including industrial and marine environment), or exposure to permanently damp internal conditions, if no particular aggressive conditions exist. Such particular aggressive conditions are e. g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with extreme chemical pollution (e. g. in desulphurization plants or road tunnels where de-icing materials are used).



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Elements made of high corrosion resistant steel:

The element made of high corrosion resistant steel 1.4529 or 1.4565 may be used in structures subject to dry internal conditions and also in structures subject to external atmospheric exposure, in permanently damp internal conditions or in other particular aggressive conditions. Such particular aggressive conditions are e.g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with chemical pollution (e.g. in desulphurization plants or road tunnels where de-icing materials are used).

Elements made of reinforcing bars:

Post-installed reinforcing bars may be used as anchor designed in accordance with the EOTA Technical Report TR 029 or CEN/TS 1992-4:2009. Such applications are e.g. concrete overlay or shear dowel connections or the connections of a wall predominantly loaded by shear and compression forces with the foundation, where the reinforcing bars act as dowels to take up shear forces. Connections with post-installed reinforcing bars in concrete structures designed in accordance with EN 1992-1-1: 2004 are not covered by this European technical approval.

The provisions made in this European technical approval are based on an assumed working life of the anchor of 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

2 Characteristics of the product and methods of verification

2.1 Characteristics of the product

The anchor corresponds to the drawings and provisions given in the Annexes. The characteristic material values, dimensions and tolerances of the anchor not indicated in the Annexes shall correspond to the respective values laid down in the technical documentation⁷ of this European technical approval.

The characteristic values for the design of anchorages are given in the Annexes.

The two components of the injection mortar are delivered in unmixed condition in coaxial cartridges of sizes 150 ml, 280 ml, 300 ml, 310 ml, 330 ml, 380 ml, 410 ml or 420 ml, in side-by side-cartridges of sizes 235 ml, 345 ml or 825 ml or in foil tube cartridges of sizes 165 ml or 300 ml according to Annex 2. Each cartridge is marked with the imprint "V12", with processing notes, charge code, storage life, hazard code and curing- and processing time depending on temperature.

Elements made of reinforcing bars shall comply with the specifications given in Annex 4.

The marking of embedment depth may be done on jobsite.

2.2 Methods of verification

The assessment of fitness of the anchor for the intended use in relation to the requirements for mechanical resistance and stability and safety in use in the sense of the Essential Requirements 1 and 4 has been made in accordance with the "Guideline for European technical approval of Metal Anchors for Use in Concrete", Part 1 "Anchors in general" and Part 5 "Bonded anchors", on the basis of Option 1 and ETAG 001 Annex E "Assessment of Metal Anchors under Seismic Action".

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The technical documentation of this European technical approval is deposited at the Deutsches Institut für Bautechnik and, as far as relevant for the tasks of the approved bodies involved in the attestation of conformity procedure, is handed over to the approved bodies.



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In addition to the specific clauses relating to dangerous substances contained in this European technical approval, there may be other requirements applicable to the products falling within its scope (e.g. transposed European legislation and national laws, regulations and administrative provisions). In order to meet the provisions of the Construction Products Directive, these requirements need also to be complied with, when and where they apply.

3 Evaluation and attestation of conformity and CE marking

3.1 System of attestation of conformity

According to the Decision 96/582/EG of the European Commission⁸ system 2(i) (referred to as System 1) of the attestation of conformity applies.

This system of attestation of conformity is defined as follows:

System 1: Certification of the conformity of the product by an approved certification body on the basis of:

- (a) Tasks for the manufacturer:
 - (1) factory production control;
 - (2) further testing of samples taken at the factory by the manufacturer in accordance with a control plan;
- (b) Tasks for the approved body:
 - (3) initial type-testing of the product;
 - (4) initial inspection of factory and of factory production control;
 - (5) continuous surveillance, assessment and approval of factory production control.

Note: Approved bodies are also referred to as "notified bodies".

3.2 Responsibilities

3.2.1 Tasks for the manufacturer

3.2.1.1 Factory production control

The manufacturer shall exercise permanent internal control of production. All the elements, requirements and provisions adopted by the manufacturer shall be documented in a systematic manner in the form of written policies and procedures, including records of results performed. This production control system shall insure that the product is in conformity with this European technical approval.

The manufacturer may only use initial/raw/constituent materials stated in the technical documentation of this European technical approval.

The factory production control shall be in accordance with the control plan which is part of the technical documentation of this European technical approval. The control plan is laid down in the context of the factory production control system operated by the manufacturer and deposited at Deutsches Institut für Bautechnik.⁹

The results of factory production control shall be recorded and evaluated in accordance with the provisions of the control plan.

The control plan is a confidential part of the European technical approval and only handed over to the approved body involved in the procedure of attestation of conformity. See section 3.2.2.



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3.2.1.2 Other tasks for the manufacturer

The manufacturer shall, on the basis of a contract, involve a body which is approved for the tasks referred to in section 3.1 in the field of anchors in order to undertake the actions laid down in section 3.2.2 For this purpose, the control plan referred to in sections 3.2.1.1 and 3.2.2 shall be handed over by the manufacturer to the approved body involved.

The manufacturer shall make a declaration of conformity, stating that the construction product is in conformity with the provisions of this European technical approval.

3.2.2 Tasks for the approved bodies

The approved body shall perform the

- initial type-testing of the product,
- initial inspection of factory and of factory production control,
- continuous surveillance, assessment and approval of factory production control, in accordance with the provisions laid down in the control plan.

The approved body shall retain the essential points of its actions referred to above and state the results obtained and conclusions drawn in a written report.

The approved certification body involved by the manufacturer shall issue an EC certificate of conformity of the product stating the conformity with the provisions of this European technical approval.

In cases where the provisions of the European technical approval and its control plan are no longer fulfilled the certification body shall withdraw the certificate of conformity and inform Deutsches Institut für Bautechnik without delay.

3.3 CE marking

The CE marking shall be affixed on each packaging of the anchor. The letters "CE" shall be followed by the identification number of the approved certification body, where relevant, and be accompanied by the following additional information:

- the name and address of the holder of the approval (legal entity responsible for the manufacture),
- the last two digits of the year in which the CE marking was affixed,
- the number of the EC certificate of conformity for the product,
- the number of the European technical approval,
- the number of the guideline for European technical approval,
- use category (ETAG 001, Option 1, seismic anchor performance category C1),
- size.

4 Assumptions under which the fitness of the product for the intended use was favourably assessed

4.1 Manufacturing

The European technical approval is issued for the product on the basis of agreed data/information, deposited at Deutsches Institut für Bautechnik, which identifies the product that has been assessed and judged. Changes to the product or production process, which could result in this deposited data/information being incorrect, should be notified to Deutsches Institut für Bautechnik before the changes are introduced. Deutsches Institut für Bautechnik will decide whether or not such changes affect the approval and consequently the validity of the CE marking on the basis of the approval and if so whether further assessment or alterations to the approval shall be necessary.



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4.2 Design of anchorages

The fitness of the anchor for the intended use is given under the following conditions:

The anchorages are designed either in accordance with the

The anchorages are designed in accordance with the

- EOTA Technical Report TR 029 "Design of bonded anchors"¹⁰
- or in accordance with the
- CEN/TS 1992-4:2009

and EOTA Technical Report TR 045 "Design of Metal Anchors under Seismic Action" under the responsibility of an engineer experienced in anchorages and concrete work.

Anchorages shall be positioned outside of critical regions (e.g. plastic hinges) of the concrete structure. Fastenings in stand-off installation or with a grout layer under seismic action are not covered by this European technical approval.

Post-installed reinforcing bars may be used as anchor designed in accordance with the EOTA Technical Report TR 029 or CEN/TS 1992-4:2009. The basic assumptions for the design according to anchor theory shall be observed. This includes the consideration of tension and shear loads and the corresponding failure modes as well as the assumption that the base material (concrete structural element) remains essentially in the serviceability limit state (either non-cracked or cracked) when the connection is loaded to failure. Such applications are e.g. concrete overlay or shear dowel connections or the connections of a wall predominantly loaded by shear and compression forces with the foundation, where the rebars act as dowels to take up shear forces. Connections with reinforcing bars in concrete structures designed in accordance with EN 1992-1-1:2004 (e.g. connection of a wall loaded with tension forces in one layer of the reinforcement with the foundation) are not covered by this European technical approval.

Verifiable calculation notes and drawings are prepared taking account of the loads to be anchored.

The position of the anchor is indicated on the design drawings (e.g. position of the anchor relative to reinforcement or to supports, etc.).

4.3 Installation of anchors

The fitness for use of the anchor can only be assumed if the anchor is installed as follows:

- anchor installation carried out by appropriately qualified personnel and under the supervision of the person responsible for technical matters of the site,
- anchor installation in accordance with the manufacturer's specifications and drawings using the tools indicated in the technical documentation of this European technical approval,
- use of the anchor only as supplied by the manufacturer without exchanging the components,
- commercial standard threaded rods, washers and hexagon nuts may be used if the following requirements are fulfilled:
 - material, dimensions and mechanical properties of the metal parts according to the specifications given in Annex 3,
 - confirmation of material and mechanical properties of the metal parts by inspection certificate 3.1 according to EN 10204:2004, the documents should be stored,

The Technical Report TR 029 "Design of Bonded Anchors" is published in English on EOTA website www.eota.eu.



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- marking of the threaded rod with the envisage embedment depth. This may be done by the manufacturer of the rod or the person on jobsite.
- embedded reinforcing bars shall comply with specifications given in Annex 4,
- checks before placing the anchor to ensure that the strength class of the concrete in which the anchor is to be placed is in the range given and is not lower than that of the concrete to which the characteristic loads apply,
- check of concrete being well compacted, e.g. without significant voids,
- marking and keeping the effective anchorage depth,
- edge distance and spacing not less than the specified values without minus tolerances,
- positioning of the drill holes without damaging the reinforcement,
- drilling by hammer-drilling only,
- in case of aborted drill hole: the drill hole shall be filled with mortar,
- cleaning the drill hole in accordance with Annexes 6 to 8,
- during installation and curing of the chemical mortar the anchor component installation temperature shall be at least -10 °C; the temperature; observing the curing time according to Annex 7, Table 4 until the anchor may be loaded,
- for injection of the mortar in bore holes of diameter $d_0 > 20$ mm piston plugs according to Annex 8 shall be used for overhead or horizontal injection,
- installation torque moments are not required for functioning of the anchor. However, the torque moments given in Annex 5 must not be exceeded.

5 Indications to the manufacturer

5.1 Responsibility of the manufacturer

The manufacturer is responsible to ensure that the information on the specific conditions according to 1 and 2 including Annexes referred to as well as sections 4.2, 4.3 and 5.2 is given to those who are concerned. This information may be made by reproduction of the respective parts of the European technical approval.

In addition all installation data shall be shown clearly on the package and/or on an enclosed instruction sheet, preferably using illustration(s).

The minimum data required are:

- drill bit diameter,
- hole depth,
- diameter of anchor rod,
- minimum effective anchorage depth,
- information on the installation procedure, including cleaning of the hole with the cleaning equipments, preferably by means of an illustration,
- anchor component installation temperature,
- ambient temperature of the concrete during installation of the anchor,
- admissible processing time (open time) of the mortar,
- curing time until the anchor may be loaded as a function of the ambient temperature in the concrete during installation,
- maximum torque moment,
- identification of the manufacturing batch,

All data shall be presented in a clear and explicit form.



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5.2 Packaging, transport and storage

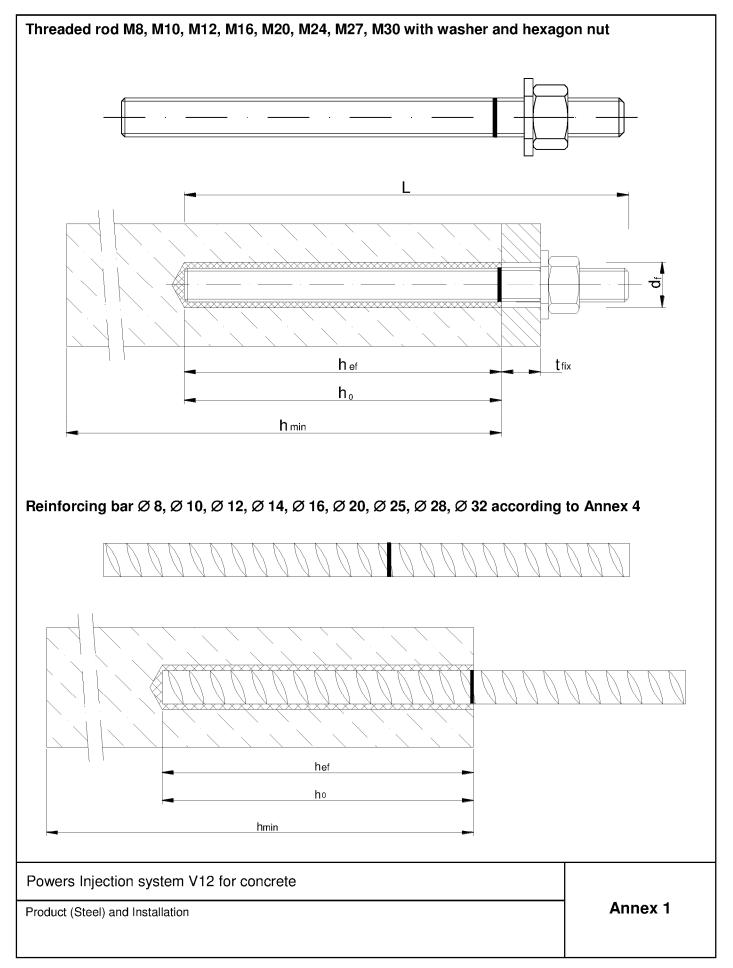
The cartridges shall be protected against sun radiation and shall be stored according to the manufacturer's installation instructions in dry condition at temperatures of at least +5 °C to not more than +25 °C.

Cartridges with expired shelf life must no longer be used.

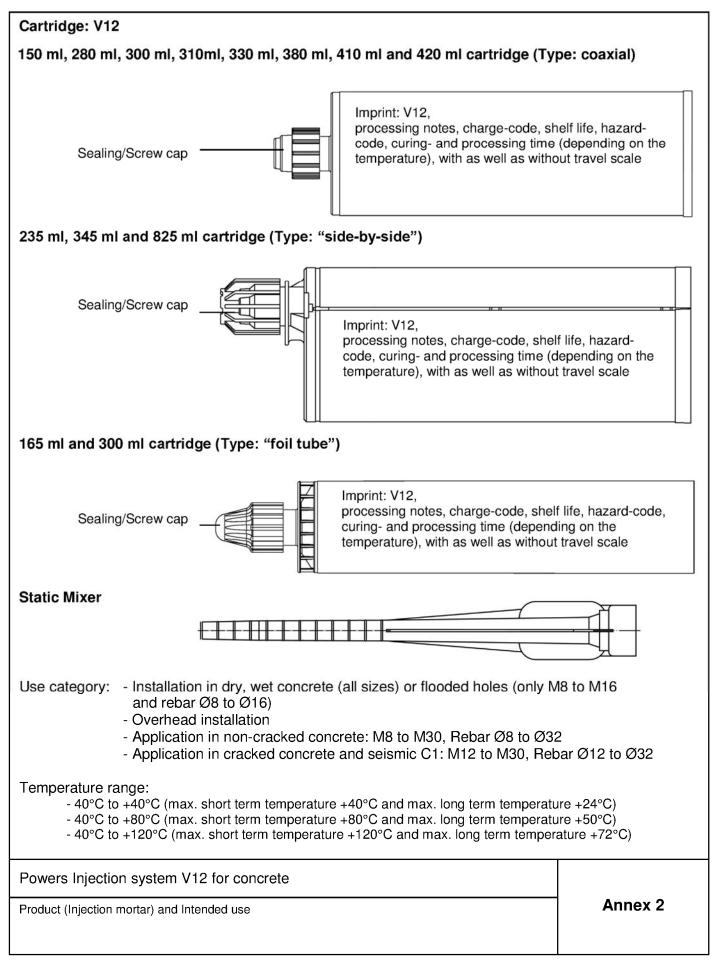
The anchor shall only be packaged and supplied as a complete unit. Cartridges may be packed separately from metal parts.

Andreas Kummerow p.p. Head of Department *beglaubigt:* Baderschneider











Tab	ole 1a: Materials (Threaded ro	d)	
		Lges	
Part	Designation I, zinc plated ≥ 5 µm acc. to EN ISO 404	Material	
	l, zinc plated ≥ 5 μm acc. to EN ISO 404 dip galvanised ≥ 40 μm acc. to EN ISO 1		
1	Anchor rod	Steel, EN 10087 or EN 10263 Property class 4.6, 5.8, 8.8, EN ISO 898-1:	
2	Hexagon nut, EN ISO 4032	Property class 4 (for class 4.6 rod) EN ISO Property class 5 (for class 5.8 rod) EN ISO Property class 8 (for class 8.8 rod) EN ISO	898-2,
3	Washer, EN ISO 887, EN ISO 7089, EN ISO 7093, or EN ISO 7094	Steel, zinc plated or hot-dip galvanised	
Stair	nless steel		
1	Anchor rod	Material 1.4401 / 1.4404 / 1.4571, EN 1008 > M24: Property class 50 EN ISO 3506 ≤ M24: Property class 70 EN ISO 3506	
2	Hexagon nut, EN ISO 4032	Material 1.4401 / 1.4404 / 1.4571 EN 10088 > M24: Property class 50 (for class 50 rod) ≤ M24: Property class 70 (for class 70 rod)	EN ISO 3506
3	Washer, EN ISO 887, EN ISO 7089, EN ISO 7093, or EN ISO 7094	Material 1.4401, 1.4404 or 1.4571, EN 100	88
High	corrosion resistance steel		
1	Anchor rod	Material 1.4529 / 1.4565, EN 10088-1:2005 > M24: Property class 50 EN ISO 3506 ≤ M24: Property class 70 EN ISO 3506	3
2	Hexagon nut, EN ISO 4032	Material 1.4529 / 1.4565 EN 10088, > M24: Property class 50 (for class 50 rod) ≤ M24: Property class 70 (for class 70 rod)	
3	Washer, EN ISO 887, EN ISO 7089, EN ISO 7093, or EN ISO 7094	Material 1.4529 / 1.4565, EN 10088	
Con - - -	nmercial standard rod with: Materials, dimensions and mechanica Inspection certificate 3.1 acc. to EN 1 Marking of embedment depth		
<u> </u>	vers Injection system V12 for concrete	2	Annex 3



Table 1b: Mate	erials (Rebar)		
Abstract of EN 19	h _{ef}	1, Properties of reinforceme	nt:
Product form		-	
			e-coiled rods
Class		В	C
Characteristic yield str	ength f_{yk} or $f_{0,2k}$ (N/mm ²)	400	to 600
Minimum value of k =	$(f_t / f_y)_k$	≥ 1,08	≥ 1,15 < 1,35
Characteristic strain at ε _{uk} (%)	t maximum force	≥ 5,0	≥ 7,5
Bendability		Bend/Re	ebend test
Maximum deviation from nominal mass (individual bar) (%)	Nominal bar size (mm) ≤ 8 > 8		6,0 4,5
	92-1-1 Annex C, Table C.2	2N, Properties of reinforcem	
Product form			e-coiled rods
Class Min. value of related rip area f _{R,min}	nominal diameter of the rebar (mm) 8 to 12 > 12		040 056
(d: Nominal diameter	shall be in the range 0,05d ≤ h of the bar; h: Rip height of the post-installed rebar as anchor	e bar)	
Powers Injection sy	stem V12 for concrete		
Materials (Reinforcing b	ar)		Annex 4

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Table 2:Installation	parameters fo	or threa	aded ro	d					
Anchor size		M 8	M 10	M 12	M 16	M 20	M 24	M 27	M 30
Nominal drill hole diameter	d ₀ [mm] =	10	12	14	18	24	28	32	35
Effective encharge depth	h _{ef,min} [mm] =	60	60	70	80	90	96	108	120
Effective anchorage depth	h _{ef,max} [mm] =	160	200	240	320	400	480	540	600
Diameter of clearance hole in the fixture	d _f [mm] ≤	9	12	14	18	22	26	30	33
Diameter of steel brush	d _b [mm] ≥	12	14	16	20	26	30	34	37
Torque moment	T _{inst} [Nm] ≤	10	20	40	80	120	160	180	200
Thickness of fixture	t _{fix,min} [mm] >	0							
Thickness of fixture	t _{fix,max} [mm] <	1500							
Minimum thickness of member	h _{min} [mm]] h _{ef} + 30 mm ≥ 100 mm h _{ef} + 2d₀							
Minimum spacing	s _{min} [mm]	40	50	60	80	100	120	135	150
Minimum edge distance	c _{min} [mm]	40	50	60	80	100	120	135	150

Table 3: Installation parameters for rebar

Rebar size			Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Nominal drill hole diameter	d ₀ [mm] =	12	14	16	18	20	24	32	35	40
h _{ef,min} [mm]		60	60	70	75	80	90	100	112	128
Effective anchorage depth	h _{əf,max} [mm] =	160	200	240	280	320	400	480	540	640
Diameter of steel brush	d _b [mm] ≥	14 16		18	20	22	26	34	37	41,5
Minimum thickness of member	h _{min} [mm]		30 mm 3 mm	$h_{ef} + 2d_0$						
Minimum spacing	s _{min} [mm]	40	50	60	70	80	100	125	140	160
Minimum edge distance	c _{min} [mm]	40	50	60	70	80	100	125	140	160

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Installation parameters

Annex 5



Installation inst	ructions							
	Drill with hammer drill a hole into the base material to the size and embedment depth required by the selected anchor (Table 2 or Table 3).							
	Attention! Standing water in the bore hole must be removed	d before cleaning.						
4x	2a. Starting from the bottom or back of the bore hole, blow the hole compressed air (min. 6 bar) or a hand pump (Annex 8) a minim the bore hole ground is not reached an extension shall be used	um of four times. If						
or	The hand-pump can be used for anchor sizes up to bore hole di	ameter 20 mm.						
4x	For bore holes larger then 20 mm or deeper 240 mm, compress must be used.	ed air (min. 6 bar)						
	2b. Check brush diameter (Table 5) and attach the brush to a drillin or a battery screwdriver. Brush the hole with an appropriate size > d _{b.min} (Table 5) a minimum of four times.							
4x	If the bore hole ground is not reached with the brush, a brush ex shall be used (Table 5).	xtension						
	2c. Finally blow the hole clean again with compressed air (min. 6 ba (Annex 8) a minimum of four times. If the bore hole ground is no							
4x or	extension shall be used. The hand-pump can be used for anchor sizes up to bore hole d For bore holes larger then 20 mm or deeper 240 mm, compress <u>must</u> be used.							
4x	After cleaning, the bore hole has to be protected against re an appropriate way, until dispensing the mortar in the bore the cleaning repeated has to be directly before dispensing In-flowing water must not contaminate the bore hole again.	hole. If necessary, the mortar.						
	3 Attach a supplied static-mixing nozzle to the cartridge and load correct dispensing tool. Cut off the foil tube clip before use. For every working interruption longer than the recommended we as well as for new cartridges, a new static-mixer shall be used.	-						
her	4. Prior to inserting the anchor rod into the filled bore hole, the posenbedment depth shall be marked on the anchor rods.	ition of the						
min. 3 full stroke	5. Prior to dispensing into the anchor hole, squeeze out separately full strokes and discard non-uniformly mixed adhesive component shows a consistent grey colour. For foil tube cartridges is must be minimum of six full strokes.	nts until the mortar						
Powers Injection sy	vstem V12 for concrete							
Installation instructions		Annex 6						



Installation inst	ructions (continuation)
	6 Starting from the bottom or back of the cleaned anchor hole fill the hole up to approximately two-thirds with adhesive. Slowly withdraw the static mixing nozzle as the hole fills to avoid creating air pockets. For embedment larger than 190 mm an extension nozzle shall be used. For overhead and horizontal installation a piston plug (Annex 8) and extension nozzle shall be used. Observe the gel-/ working times given in Table 4.
	Push the threaded rod or reinforcing bar into the anchor hole while turning slightly to ensure positive distribution of the adhesive until the embedment depth is reached. The anchor should be free of dirt, grease, oil or other foreign material.
	8. Be sure that the anchor is fully seated at the bottom of the hole and that excess mortar is visible at the top of the hole. If these requirements are not maintained, the application has to be renewed. For overhead application the anchor rod should be fixed (e.g. wedges).
+20°C	9. Allow the adhesive to cure to the specified time prior to applying any load or torque. Do not move or load the anchor until it is fully cured (attend Table 4).
	 After full curing, the add-on part can be installed with the max. torque (Table 2) by using a calibrated torque wrench.

Table 4: Minimum curing time

Concrete temperature	Gelling- / working time	Minimum curing time in dry concrete ²⁾
≥ -10 °C ¹⁾	90 min	24 h
≥ -5 °C	90 min	14 h
≥ 0 °C	45 min	7 h
≥ +5 °C	25 min	2 h
≥ + 10 °C	15 min	80 min
≥ + 20 °C	6 min	45 min
≥ + 30 °C	4 min	25 min
≥ + 35 °C	2 min	20 min
≥ + 40 °C	1,5 min	15 min

2) In wet concrete the curing time must be doubled

Powers Injection system V12 for concrete

Installation instructions (continuation) Curing time

Annex 7



Steel brush ⊐⊨≈⊭∠∠*₩₩₩₩₩₩₩₩₩*₽Ĺ \mathbf{d}_{b} Ι Table 5: Parameter cleaning and setting tools d_{b.min} Threaded d₀ \mathbf{d}_{b} Piston min. Rebar Rod Drill bit - Ø Brush - Ø plug Brush - Ø (No.) (mm) (mm) (mm) (mm) (mm) M8 10 12 10,5 M10 8 12 14 12,5 No M12 10 14 16 14,5 piston plug 12 16 18 16,5 required M16 14 18 20 18.5 16 20 22 20,5 M20 20 24 26 24,5 # 24 M24 28 30 28,5 # 28 M27 25 32 34 32,5 # 32 M30 28 35 37 # 35 35,5 32 40 41,5 40,5 # 38



Hand pump (volume 750 ml) Drill bit diameter (d₀): 10 mm to 20 mm





Rec. compressed air tool (min 6 bar) Drill bit diameter (d₀): 10 mm to 40 mm

Piston plug for overhead or horizontal installation Drill bit diameter (d₀): 24 mm to 40 mm

Powers Injection system V12 for concrete

Cleaning and setting tools

Annex 8



Combined pull-out and concrete cone failure Combined pull-out and concrete concrete C20/25 Temperature range I ⁵ : dry and wet concrete $\tau_{R6,ucr}$ [N/mm?] 10 12 12 12 12 12 11 10 d0°C/24°C flooded bore hole $\tau_{R6,ucr}$ [N/mm?] 7,5 8,5 8,5 8,5 not admissible Temperature range II ⁵ : dry and wet concrete $\tau_{R6,ucr}$ [N/mm?] 7,5 9 9 9 9 9 9 8,5 7,5 flooded bore hole $\tau_{R6,ucr}$ [N/mm?] 5,5 6,5 6,5 6,5 6,5 6,5 6,5 6,5 6,5 6,5	nchor size threaded roo	d			M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30	
Steel, property class 4.6 Nm.e [NM] 15 23 34 b3 98 [14] 194 Partial safety factor Ymm,h ⁻¹	eel failure				1	1	1	1	1	1	1		
Partial safety factor $(\gamma_{MA,1}^{(1)})$ 2.0 Characteristic tension resistance, Steel, property class 5.8 N _{RA} [kN] 18 29 42 78 122 176 230 Characteristic tension resistance, Steel, property class 5.8 N _{RA} [kN] 29 46 67 125 196 282 368 Partial safety factor Ymax1 ¹¹ 1.50 1.50 1.50 1.50 1.10 171 247 230 Characteristic tension resistance, Starless steel A1 and HCR, property class 50 (MA2) and 70 (≤ M24) N _{RA} [kN] 26 41 59 110 171 247 230 Cambined pull-out and concrete cone failure Ymax1 ¹¹ 1.87 2.17 2.17 2.11 10 Characteristic bond resistance in non-cracked concrete $\Sigma_{0/25}$ Temperature range I ¹⁶ : dry and wet concrete τ_{maxr} [N/mm ²] 1.0 12 12 12 11 10 Choded bore hole τ_{maxr} [N/mm ²] 7.5 8.5 8.5 not admissible Temperature range II ⁶ : 10°/C24°C dry and wet concrete τ_{maxr} [N/mm ²]		stance,	N _{Rk,s}	[kN]	15	23	34	63	98	141	184	224	
Steel, property class 5.8 Nika. [kN] 10 29 42 78 122 170 230 Steel, property class 8.8 Nika.a [kN] 29 46 67 125 196 282 368 Partial safety factor γ_{Max}^{-1} 1.50 1.50 196 282 368 Partial safety factor γ_{Max}^{-1} 1.50 1.50 1.50 2.30 Characterific tension resistance, stanles, steel A4 and HCA, property class 50 (-M24) and 70 (< M24)			γ _{Ms,N} ¹⁾			1	1	2	,0	1	1		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		stance,	N _{Rk,s}	[kN]	18	29	42	78	122	176	230	280	
Partial safety factor $\gamma_{(h_{0},N}^{-1)}$ 1.50 Characteristic tension resistance, Stainless steel A4 and HCR, property class 5 (s/M24) and 70 (\leq M24) N _{N,8} [kN] 26 41 59 110 171 247 230 Partial safety factor $\gamma_{(h_{0},N)}^{-11}$ 1,87 2,1 Combined pull-out and concrete cone failure $\gamma_{(h_{0},N)}^{-11}$ 1,87 2,1 Characteristic bond resistance in non-cracked concrete $\tau_{(h_{0},m)}^{-11}$ 10 12 12 12 11 10 Of C/24°C dry and wet concrete $\tau_{(h_{0},m)}^{-11}$ 10 12 12 12 11 10 Of C/24°C dry and wet concrete $\tau_{(h_{0},m)}^{-11}$ [N/mm?] 7,5 8,5 8,5 not admissible Temperature range [1 ⁶): dry and wet concrete $\tau_{(h_{0},m)}^{-11}$ [N/mm?] 5,5 6,5 6,5 6,5 5,5 5,5 Temperature range [1 ⁶): dry and wet concrete $\tau_{(h_{0},m)}^{-11}$ [N/mm?] 5,5 6,5 6,5 6,5 6,5 5,5 5,5 Temperature range [1 ⁶): dry and wet concret	naracteristic tension resi	stance,	N _{Rk,s}	[kN]	29	46	67	125	196	282	368	449	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			γ _{Ms,N} ¹⁾				I	۱. 1,	50	I			
Partial safety factor $\gamma_{Me,N}^{(1)}$ 1,87 2,4 Combined pull-out and concrete cone failure Characteristic bond resistance in non-cracked concrete C20/25 Temperature range [s]: dry and wet concrete T _{FR,MET} [N/mm ²] 10 12 12 11 10 Temperature range [s]: dry and wet concrete T _{TR,MET} [N/mm ²] 7,5 8,5 8,5 not admissible Temperature range [I] ⁶ : dry and wet concrete T _{TR,MET} [N/mm ²] 7,5 8,5 6,5 <th c<="" td=""><td>naracteristic tension resis ainless steel A4 and HC</td><td>R,</td><td></td><td>[kN]</td><td>26</td><td>41</td><td>59</td><td>-</td><td></td><td>247</td><td>230</td><td>281</td></th>	<td>naracteristic tension resis ainless steel A4 and HC</td> <td>R,</td> <td></td> <td>[kN]</td> <td>26</td> <td>41</td> <td>59</td> <td>-</td> <td></td> <td>247</td> <td>230</td> <td>281</td>	naracteristic tension resis ainless steel A4 and HC	R,		[kN]	26	41	59	-		247	230	281
$\begin{array}{c c c c c c c } \hline Characteristic bond resistance in non-cracked concrete C20/25 \\ \hline Temperature range I^{5)} & dry and wet concrete $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$			γ _{Ms,N} 1)				1,	87	1		2,	86	
$ \begin{array}{c c c c c c c } \hline \mbox{Temperature range } I^{5}: & \mbox{dry and wet concrete} & $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$	ombined pull-out and c	oncrete cone failure											
$\begin{array}{c c c c c c } \hline \begin{tabular}{ c c c } \hline \begin{tabular}{ c c c c } \hline \begin{tabular}{ c c c c } \hline \begin{tabular}{ c c c c c } \hline \begin{tabular}{ c c c c c c } \hline \begin{tabular}{ c c c c c c c } \hline \begin{tabular}{ c c c c c c c } \hline \hline \end{tabular} \hline \end{tabular}$	naracteristic bond resista	ance in non-cracked con	crete C20	/25									
$ \frac{40^{\circ}\text{C}/24^{\circ}\text{C}}{10000000000000000000000000000000000$	$\frac{1}{1}$	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm ²]	10	12	12	12	12	11	10	9	
$\begin{array}{c c c c c c c c c } \hline Prime range III^{\circ}: & Prime range III^{\circ}$		flooded bore hole	τ _{Rk,ucr}	[N/mm ²]	7,5	8,5	8,5	8,5		not adı	nissible		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	emperature range II ⁵⁾ :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm ²]	7,5	9	9	9	9	8,5	7,5	6,5	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		flooded bore hole	$\tau_{Rk,ucr}$	T _{Rk,ucr} [N/mm ²] 5,5 6,5 6,5 6,5 r				not adr	not admissible				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	emperature range III ⁵⁾ :	dry and wet concrete	$ au_{Rk,ucr}$	[N/mm ²]	5,5	6,5	6,5	6,5	6,5	6,5	5,5	5,0	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		flooded bore hole	$\tau_{Rk,ucr}$	[N/mm ²]	4,0	5,0	5,0	5,0	not admissible				
			C30/37 1,04										
Splitting failure Edge distance $c_{or,sp}$ [mm] $1,0 \cdot h_{ef} \leq 2 \cdot h_{ef} \left(2,5 - \frac{h}{h_{ef}}\right) \leq 2,4 \cdot h_{ef}$ Axial distance $s_{or,sp}$ [mm] $2 c_{cr,sp}$ Partial safety factor (dry and wet concrete) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ $1,5^{2}$ $1,8^{3}$ Partial safety factor (flooded bore hole) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ $2,1^{4}$ not admissible 1 In absence of other national regulations 2 The partial safety factor $\gamma_{2} = 1.0$ is included. 3 The partial safety factor $\gamma_{2} = 1.2$ is included. 3 The partial safety factor $\gamma_{2} = 1.4$ is included.	5	rete	C40/50		1,08								
Edge distance $c_{cr,sp}$ [mm] $1,0 \cdot h_{ef} \leq 2 \cdot h_{ef} \left(2,5 - \frac{h}{h_{ef}}\right) \leq 2,4 \cdot h_{ef}$ Axial distance $s_{cr,sp}$ [mm] $2 c_{cr,sp}$ Partial safety factor (dry and wet concrete) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ $1,5^{2}$ $1,8^{3}$ Partial safety factor (flooded bore hole) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ $2,1^{4}$ not admissible $^{1)}$ In absence of other national regulations $^{2)}$ The partial safety factor $\gamma_{2} = 1.0$ is included. $^{3)}$ The partial safety factor $\gamma_{2} = 1.2$ is included. $^{4)}$ The partial safety factor $\gamma_{2} = 1.4$ is included.			C50/60					1,	10				
Axial distance $s_{cr,sp}$ [mm] $2 c_{cr,sp}$ Partial safety factor (dry and wet concrete) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ $1,5^{2}$ $1,8^{3}$ Partial safety factor (flooded bore hole) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ $2,1^{4}$ not admissible $^{1)}$ In absence of other national regulations $^{2)}$ The partial safety factor $\gamma_2 = 1.0$ is included. $^{3)}$ The partial safety factor $\gamma_2 = 1.2$ is included. $^{4)}$ The partial safety factor $\gamma_2 = 1.4$ is included. $\gamma_{Mp} = 1.4$ is included.	litting failure							(<u> </u>			
Partial safety factor (dry and wet concrete) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ 1,5 ² 1,8 ³ Partial safety factor (flooded bore hole) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ 2,1 ⁴ not admissible ¹⁾ In absence of other national regulations $^{2)}$ The partial safety factor $\gamma_2 = 1.0$ is included. $^{3)}$ The partial safety factor $\gamma_2 = 1.2$ is included. ⁴⁾ The partial safety factor $\gamma_2 = 1.4$ is included.	lge distance		C _{cr,sp}	[mm]		1,() · h _{ef} ≤:	2 · h _{ef} (2	,5 – <u>n</u> h _{ef}) ≤ 2,4 ·	h _{ef}		
Partial safety factor (flooded bore hole) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1}$ 2,14)not admissible1) In absence of other national regulations2) The partial safety factor $\gamma_2 = 1.0$ is included.3) The partial safety factor $\gamma_2 = 1.2$ is included.4) The partial safety factor $\gamma_2 = 1.4$ is included.	vial distance		S _{cr,sp}	[mm]				2 c	cr,sp				
¹⁾ In absence of other national regulations ²⁾ The partial safety factor $\gamma_2 = 1.0$ is included. ³⁾ The partial safety factor $\gamma_2 = 1.2$ is included. ⁴⁾ The partial safety factor $\gamma_2 = 1.4$ is included.	artial safety factor (dry ar	nd wet concrete)	$\gamma_{Mp} = \gamma_{Mc}$	$= \gamma_{Msp}{}^{1)}$	1,5 ²⁾				1,8 ³⁾				
²⁾ The partial safety factor $\gamma_2 = 1.0$ is included. ³⁾ The partial safety factor $\gamma_2 = 1.2$ is included. ⁴⁾ The partial safety factor $\gamma_2 = 1.4$ is included.				$= \gamma_{Msp}{}^{1)}$	2,14)			not admissible					
Explanations see section 1.2	²⁾ The partial safet ³⁾ The partial safet	y factor $\gamma_2 = 1.0$ is inc y factor $\gamma_2 = 1.2$ is inc y factor $\gamma_2 = 1.4$ is inc	luded. luded.										
Powers Injection system V12 for concrete	owers Injection s	ystem V12 for cor	ncrete										



Anchor size threaded roo	d			M 12	M 16	M 20	M24	M 27	M 30	
Steel failure						•		•		
Characteristic tension resis Steel, property class 4.6	stance,	N _{Rk,s}	[kN]	34	63	98	141	184	224	
Partial safety factor		γ _{Ms,N} ¹⁾				2	,0			
Characteristic tension resis	stance,	N _{Rk,s}	[kN]	42	78	122	176	230	280	
Steel, property class 5.8 Characteristic tension resis	stance,	N _{Rk.s}	[kN]	67	125	196	282	368	449	
Steel, property class 8.8 Partial safety factor		γ _{Ms,N} ¹⁾	[]				50			
Characteristic tension resis Stainless steel A4 and HC	R,	N _{Rk,s}	[kN]	59	110	171	247	230	281	
property class 50 (>M24) a Partial safety factor	and 70 (≤ M24)	γ _{Ms,N} ¹⁾			1,	87		2.	l 86	
Combined pull-out and c	oncrete cone failure	,, .			,			,		
•	ance in cracked concrete C2	0/25								
- 14)	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm ²]	5,5	5,5	5,5	5,5	6,5	6,5	
Temperature range I ⁴⁾ : 40°C/24°C	flooded bore hole	τ _{Rk,cr}	[N/mm ²]	5,5	5,5		not adı	l missible		
	dry and wet concrete	τ _{Rk,cr}	[N/mm ²]	4,0	4,0	4,0	4,0	4,5	4,5	
B0°C/50°C	mperature range II ":		[N/mm²]	4,0 4,0 not adi			Imissible			
Temperature range III ⁴⁾ : 120°C/72°C	dry and wet concrete	τ _{Rk,cr}	[N/mm ²]	3,0	3,0	3,0	3,0	3,5	3,5	
	flooded bore hole	$\tau_{Rk,cr}$	[N/mm²]	3,0	3,0 not admissible					
		C30/37	7			1,	04			
ncreasing factors for conc ⊭₀	rete	C40/50)	1,08						
		C50/60)			1,	10			
Splitting failure			1			(
Edge distance		C _{cr,sp}	[mm]	$1,0 \cdot h_{ef} \leq 2 \cdot h_{ef} \left(2,5 - \frac{h}{h_{ef}}\right) \leq \frac{1}{2} \left(2,5 - \frac{h}{2}\right)$				≤ 2,4 · h _{ef}		
Axial distance		S _{cr,sp}	[mm]	2 c _{cr}			cr,sp			
Partial safety factor (dry ar	nd wet concrete)	$\gamma_{Mp} = \gamma_{N}$	$\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{1}$		1,8			,8 ²⁾		
Partial safety factor (flooded bore hole)		$\gamma_{Mp} = \gamma_{N}$	$\gamma_{Mp}=\gamma_{Mc}=\gamma_{Msp}{}^{1)}$		2,1 ³⁾		not admissible			
²⁾ The partial safet	ther national regulations y factor $\gamma_2 = 1.2$ is include y factor $\gamma_2 = 1.4$ is include e section 1.2									



Table 7:	Design according cracked and non-										
Anchor size thread	ded rod			M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
Steel failure witho	ut lever arm			•	•	•	•	•			
Characteristic shear Steel, property class	,	$V_{Rk,s}$	[kN]	7	12	17	31	49	71	92	112
Partial safety factor		γ _{Ms,V} 1)	1		•		1,	67			
Characteristic shear Steel, property class		$V_{Rk,s}$	[kN]	9	15	21	39	61	88	115	140
Characteristic shear Steel, property class		$V_{Rk,s}$	[kN]	15	23	34	63	98	141	184	224
Partial safety factor		γ _{Ms,V} 1)					1,	25			
Characteristic shear Stainless steel A4 a property class 50 (>		V _{Rk,s}	[kN]	13	20	30	55	86	124	115	140
Partial safety factor		γ _{Ms,V} 1)				1,	56			2,	38
Steel failure with lo	ever arm										
Characteristic bend Steel, property class		M ⁰ _{Rk,s}	[Nm]	15	30	52	133	260	449	666	900
Partial safety factor		γ _{Ms,V} 1)			•		1,	67			
Characteristic bend Steel, property class	ing moment, s 5.8	M ⁰ _{Rk,s}	[Nm]	19	37	65	166	324	560	833	1123
Characteristic bend Steel, property class	ing moment,	M ⁰ _{Rk,s}	[Nm]	30	60	105	266	519	896	1333	1797
Partial safety factor		γ _{Ms,V} 1)					1,	25			
Characteristic bend Stainless steel A4 a property class 50 (>		M ⁰ _{Rk,s}	[Nm]	26	52	92	232	454	784	832	1125
Partial safety factor		γ _{Ms,V} 1)				1,	56			2,	38
Concrete pry-out f	ailure			•							
	n (5.7) of Technical Report gn of Bonded Anchors						2	,0			
Partial safety factor		$\gamma_{Mcp}{}^{1)}$					1,5	i0 ²⁾			
Concrete edge fail	ure										
See section 5.2.3.4	of Technical Report TR 029	for the desig	gn of Bond	led Ancho	rs						
Partial safety factor		γ _{Mc} ¹⁾					1,5	i0 ²⁾			
¹⁾ In absence c ²⁾ The partial sa	of other national regulation afety factor $\gamma_2 = 1.0$ is inclu	s ided.									
Powers Inject	ion system V12 for co	oncrete									
	threaded rod R 029, Characteristic valu quasi-static action	es for shea	ar loads i	n cracke	d and no	n-cracke	d concre	te	An	nex 1 [.]	1



	esign according on-cracked con								ion l	oads	in	
Anchor size reinforci	ng bar			Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure				1	1	1			1			
Characteristic tension r reinforcing bar accordir		N _{Rk,s}	[kN]				,	$A_s \times f_{uk}^{6}$)			
Partial safety factor		γ _{Ms,N} ¹⁾				TR 02	29 Section	on 3.2.2	.2, Eq. 3	.3a ⁶⁾		
Combined pull-out an	d concrete cone failure	1										
Characteristic bond res	istance in uncracked cond	rete C20/25										
Temperature range I ⁵⁾ :	dry and wet concrete	τ _{Rk,ucr}	[N/mm ²]	10	12	12	12	12	12	11	10	8,5
40°C/24°C	flooded bore hole	$ au_{Rk,ucr}$	[N/mm ²]	7,5	8,5	8,5	8,5	8,5		not adr	nissible	
Temperature range II ⁵⁾	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm ²]	7,5	9	9	9	9	9	8,0	7,0	6,0
80°C/50°C	flooded bore hole	$ au_{\mathrm{Rk,ucr}}$	[N/mm²]	5,5	6,5	6,5	6,5	6,5		not adr	nissible	
Temperature range III ⁵	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm ²]	5,5	6,5	6,5	6,5	6,5	6,5	6,0	5,0	4,5
120°C/72°C	flooded bore hole	$\tau_{Rk,ucr}$	[N/mm ²]	4,0	5,0	5,0	5,0	5,0		not adr	nissible	1
	I	C30/37						1,04				
Increasing factors for c	oncrete	C40/50						1,08				
Ψc		C50/60						1,10				
Splitting failure												
Edge distance		C _{cr,sp}	[mm]		1	,0 ⋅ h _{ef}	≤2 ⋅h _e	2,5 -	$\left(\frac{h}{h_{ef}}\right) \le$	2,4 · h _e	f	
Axial distance		S _{cr,sp}	[mm]					2 c _{cr,sp}				
Partial safety factor (dr	y and wet concrete)	$\gamma_{Mp} = \gamma_{Mc} =$	= γ _{Msp} ¹⁾	1,5 ²⁾				1,	8 ³⁾			
Partial safety factor (flo	oded bore hole)	$\gamma_{Mp} = \gamma_{Mc} =$	= γ _{Msp} ¹⁾		•	2,1 ⁴⁾				not adr	nissible	
 ²⁾ The partial sa ³⁾ The partial sa ⁴⁾ The partial sa ⁵⁾ Explanations ⁶⁾ f_{uk}, f_{yk} see rel 	f other national regulati afety factor $\gamma_2 = 1.0$ is in afety factor $\gamma_2 = 1.2$ is in afety factor $\gamma_2 = 1.4$ is in see section 1.2 evant Technical Specif f post-installed rebar as	cluded. cluded. cluded. cation for		-								
Application with reir Design acc. to TR 0			concrete u	nder sta	tic and	guasi-	static a	ction		Ann	ex 12	



	gn according to TR (ked concrete under s	-					ension	load	s in	
Anchor size reinforcing ba	ır			Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure						•	•			
Characteristic tension resista reinforcing bar according to		N _{Rk,s}	[kN]				$A_s \times f_{uk}$ ⁵⁾			
Partial safety factor		γ _{Ms,N} 1)	•		TR	029 Sect	tion 3.2.2.	2, Eq. 3.3	3a ⁵⁾	
Combined pull-out and co	ncrete cone failure			•						
Characteristic bond resistan	ce in cracked concrete C20/25									
Temperature range I ⁴⁾ :	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm²]	5,5	5,5	5,5	5,5	5,5	6,5	6,5
40°C/24°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm²]	5,5	5,5	5,5		not adr	nissible	
Temperature range II ⁴⁾ :	dry and wet concrete	$\tau_{\text{Rk,cr}}$	[N/mm²]	4,0	4,0	4,0	4,0	4,0	4,5	4,5
80°C/50°C	flooded bore hole	$\tau_{\text{Rk,cr}}$	[N/mm²]	4,0	4,0	4,0		not adr	nissible	
Temperature range III ⁴⁾ :	dry and wet concrete	$\tau_{\text{Rk,cr}}$	[N/mm²]	3,0	3,0	3,0	3,0	3,0	3,5	3,5
120°C/72°C	flooded bore hole	$\tau_{\text{Rk,cr}}$	[N/mm ²]	3,0	3,0	3,0		not adr	nissible	
		C30/37					1,04			
Increasing factors for concre Ψ_{c}	ote	C40/50	1				1,08			
		C50/60					1,10			
Splitting failure		1								
Edge distance		C _{cr,sp}	[mm]		1 ,0 ⋅ h _e	_{af} ≤2.h,	ef (2,5 -	$\frac{h}{h_{ef}} \le 2$	2,4 · h _{ef}	
Axial distance		S _{cr,sp}	[mm]				2 c _{cr,sp}			
Partial safety factor (dry and	wet concrete)		$_{\rm lc} = \gamma_{\rm Msp}^{1)}$				1,8 ²⁾			
Partial safety factor (flooded	bore hole)	$\gamma_{Mp}=\gamma_N$	$_{\rm lc} = \gamma_{\rm Msp}^{1)}$		2,1 ³⁾			not adr	nissible	
²⁾ The partial safety ³⁾ The partial safety ⁴⁾ Explanations see ⁵⁾ f _{uk} , f _{yk} see relevar	er national regulations factor $\gamma_2 = 1.2$ is included. factor $\gamma_2 = 1.4$ is included. section 1.2 It Technical Specification for st-installed rebar as anchor st									
	stem V12 for concrete							٨٣	nov 1')
Application with reinforc Design acc. to TR 029, Characteristic values for	ing bar tension loads in cracked cor	ncrete u	nder static a	and quas	ii-static a	action		AU	nex 13)



Table 9:	Design accord and non-crack										n crac	ked
Anchor size reinfo	rcing bar			Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure withou	ut lever arm											
Characteristic shear bar according to Ani	r resistance, reinforcing nex 4	$V_{Rk,s}$	[kN]				0,5	0 x A _s x f	3) uk			
Partial safety factor		γ _{Ms,V} ¹⁾	•			TR 02	29 Sectio	n 3.2.2.2	, Eq. 3.3	b+c ³⁾		
Steel failure with le	ever arm	I		1								
Characteristic bendi reinforcing bar acco		M ⁰ _{Rk,s}	[Nm]				1.2	2 ·W _{el} · f _u	3) k			
Partial safety factor		γ _{Ms,V} ¹⁾				TR 02	29 Sectio	n 3.2.2.2	, Eq. 3.3	b+c ³⁾		
Concrete pry-out fa	ailure											
	(5.7) of Technical Repor on of bonded anchors	t						2,0				
Partial safety factor		γ _{Мер} 1)						1,50 ²⁾				
Concrete edge fail	ure											
See section 5.2.3.4	of Technical Report TR 0	29 for the de	sign of B	onded Ar	nchors							
²⁾ The partial sa ³⁾ f _{uk} , f _{yk} see re	f other national regulat afety factor γ ₂ = 1.0 is in levant Technical Spec ign of post-installed rel	ncluded. ification for		-								
Powers Inject	ion system V12 for	r concrete)									
	reinforcing bar R 029, Characteristic v quasi-static action	alues for st	near load	ds in cra	icked an	d non-cr	acked c	oncrete		Anr	nex 14	ļ



Anchor size threaded rod				M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
Steel failure											
Characteristic tension resist Steel, property class 4.6	tance,	N _{Rk,s}	[kN]	15	23	34	63	98	141	184	224
Partial safety factor		γ _{Ms,N} ¹⁾					2	,0			
Characteristic tension resist	tance,	N _{Rk,s}	[kN]	18	29	42	78	122	176	230	280
Steel, property class 5.8 Characteristic tension resist	tance.	,									
Steel, property class 8.8		N _{Rk,s}	[kN]	29	46	67	125	196	282	368	449
Partial safety factor		γ _{Ms,N} ¹⁾					1,	50			
Characteristic tension resist Stainless steel A4 and HCF property class 50 (>M24) ar	۲, ۱	$N_{Rk,s}$	[kN]	26	41	59	110	171	247	230	281
Partial safety factor	· ·	γ _{Ms,N} ¹⁾				. 1,	87			2,	86
Combined pull-out and co	oncrete failure	I									
Characteristic bond resistar	nce in non-cracked concrete	e C20/25									
Temperature range I ⁵ :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm ²]	10	12	12	12	12	11	10	9
40°C/24°C	flooded bore hole	$\tau_{Rk,ucr}$	[N/mm ²]	7,5	8,5	8,5	8,5		not adr	nissible	
Temperature range II ⁵⁾ :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm ²]	7,5	9	9	9	9	8,5	7,5	6,5
80°C/50°C	flooded bore hole	τ _{Rk,ucr}	[N/mm ²]	5,5	6,5	6,5	6,5		not adr	nissible	
Temperature range III ⁵ :	dry and wet concrete	τ _{Rk,ucr}	[N/mm ²]	5,5	6,5	6,5	6,5	6,5	6,5	5,5	5,0
120°C/72°C	flooded bore hole	τ _{Rk,ucr}	[N/mm ²]	4,0	5,0	5,0	5,0		not adr	nissible	
		C30/37					1,0	L 04			
Increasing factors for concr	ete	C40/50					1,4	08			
Ψα		C50/60					1,	10			
Factor according to CEN/TS 1992-4-5 Section 6	<u> </u>	k ₈	[-]				10),1			
Concrete cone failure	5.2.2.3										
Factor according to CEN/TS 1992-4-5 Section 6	\$ 2 3 1	k _{ucr}	[-]				10),1			
Edge distance	5.2.0.1	C _{cr,N}	[mm]				1,5	h _{et}			
Axial distance		S _{cr,N}	[mm]					h _{ef}			
Splitting failure											
Edge distance		C _{cr,sp}	[mm]		1	,0 ⋅ h _{ef} ≤	$2 \cdot h_{ef} (2,$	$\overline{5 - \frac{h}{h_{ef}}}$	≤ 2,4 · h _e	əf	
Axial distance		S _{cr,sp}	[mm]				2 c	cr,sp			
Partial safety factor (dry and	d wet concrete)	$\gamma_{Mp} = \gamma_{Mc}$	$\gamma_{\rm Msp}^{(1)}$	1,5 ²⁾				1,8 ³⁾			
Partial safety factor (flooded	d bore hole)	$\gamma_{Mp} = \gamma_{Mc}$	$\gamma_{\rm Msp} = \gamma_{\rm Msp}$		2,	1 ⁴⁾			not adr	nissible	
²⁾ The partial safety ³⁾ The partial safety	ther national regulations factor $\gamma_2 = 1.0$ is include factor $\gamma_2 = 1.2$ is include factor $\gamma_2 = 1.4$ is include section 1.2	ed.									
Powers Injection sy	stem V12 for concr	ete									



Table 10b: Design according to CEN/TS 1992-4: Characteristic values for tension loads in cracked concrete under static and quasi-static action Anchor size threaded rod M 12 M 20 M30 M 16 M24 M27 Steel failure Characteristic tension resistance, $N_{\mathsf{R}k,s}$ [kN] 34 63 98 141 184 224 Steel, property class 4.6 $\gamma_{Ms,N}$ 1) Partial safety factor 2.0 Characteristic tension resistance. N_{Rk,s} [kN] 42 78 122 176 230 280 Steel, property class 5.8 Characteristic tension resistance, 125 282 368 449 N_{Rk,s} [kN] 67 196 Steel, property class 8.8 γ_{Ms,N}¹⁾ Partial safety factor 1,50 Characteristic tension resistance. Stainless steel A4 and HCR, [kN] 59 110 171 247 230 281 $N_{Rk,s}$ property class 50 (>M24) and 70 (≤ M24) γ_{Ms,N} ¹⁾ Partial safety factor 1,87 2,86 Combined pull-out and concrete failure Characteristic bond resistance in cracked concrete C20/25 dry and wet concrete [N/mm²] 5,5 5,5 5,5 5,5 6,5 6,5 Temperature range I⁴⁾: $\tau_{Rk,cr}$ 40°C/24°C flooded bore hole $\tau_{Rk,cr}$ [N/mm²] 5.5 5.5 not admissible dry and wet concrete $\tau_{Rk,cr}$ [N/mm²] 4.0 4.0 4.0 4.0 4.5 4.5 Temperature range II⁴⁾: 80°C/50°C flooded bore hole $\tau_{Rk.cr}$ [N/mm²] 4,0 4,0 not admissible dry and wet concrete $\tau_{\rm Bk \ cr}$ [N/mm²] 3,0 3,0 3,0 3.5 3,5 3.0 Temperature range III⁴: 120°C/72°C flooded bore hole $\tau_{\text{Rk,cr}}$ [N/mm²] 3,0 3,0 not admissible C30/37 1,04 Increasing factors for concrete C40/50 1,08 Ψc C50/60 1,10 Factor according to k_8 7,2 [-] CEN/TS 1992-4-5 Section 6.2.2.3 Concrete cone failure Factor according to k_{cr} [-] 7,2 CEN/TS 1992-4-5 Section 6.2.3.1 Edge distance C_{cr,N} [mm] 1,5 h_{ef} Axial distance [mm] 3,0 h_{ef} S_{cr,N} Splitting failure h $1,0 \cdot h_{ef} \le 2 \cdot h_{ef}$ 2,5 \leq 2,4 \cdot h_{ef} Edge distance [mm] C_{cr,sp} h_{ef} Axial distance [mm] 2 c_{cr,sp} S_{cr,sp} 1,8²⁾ $\gamma_{Mp}=\gamma_{Mc}=\gamma_{Msp}\ ^{1)}$ Partial safety factor (dry and wet concrete) Partial safety factor (flooded bore hole) $\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}$ ¹⁾ 2,1³⁾ not admissible ¹⁾ In absence of other national regulations ²⁾ The partial safety factor $\gamma_2 = 1.2$ is included. ³⁾ The partial safety factor $\gamma_2 = 1.4$ is included. ⁴⁾ Explanations see section 1.2 Powers Injection system V12 for concrete Annex 16 Application with threaded rod Design according to CEN/TS 1992-4 Characteristic values for tension loads in cracked concrete under static and quasi-static action



Table 11: Design according to CEN/TS 1992-4: Characteristic values for shear loads in cracked and non-cracked concrete under static and quasi-static action

Anchor size threaded rod			M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
Steel failure without lever arm			1	1	1	1	1	1	1	1
Characteristic shear resistance, Steel, property class 4.6	V _{Rk,s}	[kN]	7	12	17	31	49	71	92	112
Partial safety factor	γ _{Ms,V} 1)	•				1,	67			
Characteristic shear resistance, Steel, property class 5.8	V _{Rk,s}	[kN]	9	15	21	39	61	88	115	140
Characteristic shear resistance, Steel, property class 8.8	V _{Rk,s}	[kN]	15	23	34	63	98	141	184	224
Partial safety factor	γ _{Ms,V} ¹⁾					1,:	25			
Characteristic shear resistance, Stainless steel A4 and HCR, property class 50 (>M24) and 70 (\leq M24)	$V_{Rk,s}$	[kN]	13	20	30	55	86	124	115	140
Partial safety factor	$\gamma_{Ms,V}$ 1)				1,	56			2,	38
Ductility factor according to CEN/TS 1992-4-5 Section 6.3.2.1	k ₂					0	.8			
Steel failure with lever arm	-									
Characteristic bending moment, Steel, property class 4.6	$M^0_{\rm Rk,s}$	[Nm]	15	30	52	133	260	449	666	900
Partial safety factor	γ _{Ms,V} 1)					1,	67			
Characteristic bending moment, Steel, property class 5.8	M ⁰ _{Rk,s}	[Nm]	19	37	65	166	324	560	833	112
Characteristic bending moment, Steel, property class 8.8	M ⁰ _{Rk,s}	[Nm]	30	60	105	266	519	896	1333	179
Partial safety factor	$\gamma_{Ms,V}$ 1)					1,:	25			
Characteristic bending moment, Stainless steel A4 and HCR, property class 50 (>M24) and 70 (≤ M24)	M ⁰ _{Rk,s}	[Nm]	26	52	92	232	454	784	832	112
Partial safety factor	γ _{Ms,V} 1)				1,	56			2,	38
Concrete pry-out failure	•								1	
Factor in equation (27) of CEN/TS 1992-4-5 Section 6.3.3	k ₃					2	0			
Partial safety factor	γ _{Mcp} ¹⁾					1,5	0 2)			
Concrete edge failure ³⁾										
Effective length of anchor	l _t	[mm]				$I_{f} = min(h$	_{ef} ; 8 d _{nom})			
Outside diameter of anchor	d _{nom}	[mm]	8	10	12	16	20	24	27	30
Partial safety factor	γ _{Mc} ¹⁾					1,5	0 2)			
¹⁾ In absence of other nationa ²⁾ The partial safety factor γ_2 = ³⁾ See CEN/TS 1992-4-5 Sect	1.0 is includ	led.								

Powers Injection system V12 for concrete

Application with threaded rod Design according to CEN/TS 1992-4, Characteristic values for shear loads in cracked and noncracked concrete under static and quasi-static action Annex 17



	sign according to ds in non-cracke										n	
Anchor size reinforcing t	par			Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure				I		I	1	I	I	1		
Characteristic tension resist reinforcing bar according to	,	N _{Rk,s}	[kN]					A _s x f _{uk} ⁶)			
Partial safety factor		γ _{Ms,N} 1)			С	EN/TS	1992-4-1	Section	14.4.3.1	.1, Eq. 4	6)	
Combined pull-out and c	oncrete failure			1								
Characteristic bond resista	nce in non-cracked concre	ete C20/2	5									
Temperature range I ⁵⁾ :	dry and wet concrete	$\tau_{Rk,ucr}$	[N/mm ²]	10	12	12	12	12	12	11	10	8,5
40°C/24°C	flooded bore hole	$\tau_{Rk,ucr}$	[N/mm ²]	7,5	8,5	8,5	8,5	8,5		not adr	ı nissible	
T 115).	dry and wet concrete	τ _{Rk,ucr}	[N/mm²]	7,5	9	9	9	9	9	8,0	7,0	6,0
Temperature range II ⁵⁾ : 80°C/50°C	flooded bore hole	τ _{Rk,ucr}	[N/mm ²]	5,5	6,5	6,5	6,5	6,5		not adr	l nissible	
	dry and wet concrete	τ _{Rk,ucr}	[N/mm ²]	5,5	6,5	6,5	6,5	6,5	6.5	6.0	5.0	4,5
Temperature range III ⁵⁾ : 120°C/72°C	flooded bore hole		[N/mm ²]	4,0	5,0	5,0	5,0	5,0	0,0	,	nissible	4,0
		τ _{Rk,ucr} C30/37		4,0	5,0	5,0	5,0	1,04		not au	lissible	
Increasing factors for conc	rete	C30/37						1,04				
Ψc		C50/60						1,00				
Factor according to CEN/TS 1992-4-5 Section	6000	k ₈	[-]					10,1				
Concrete cone failure	0.2.2.3											
Factor according to CEN/TS 1992-4-5 Section	6091	k _{ucr}	[-]					10,1				
Edge distance	0.2.3.1	C _{cr,N}	[mm]					1,5 h _{et}				
Axial distance		S _{cr.N}	[mm]					3,0 h _{ef}				
Splitting failure				1								
Edge distance		C _{cr,sp}	[mm]			1,0 · h,	_{ef} ≤2 ⋅h _e	ef (2,5	$\frac{h}{h_{ef}} \le 2$,4 ⋅ h _{ef}		
Axial distance		S _{cr,sp}	[mm]					2 c _{cr,sp}				
Partial safety factor (dry ar	nd wet concrete)	$\gamma_{Mp} = \gamma_N$	$\gamma_{\rm Mc} = \gamma_{\rm Msp}^{1)}$	1,5 ²⁾				1,	8 ³⁾			
Partial safety factor (floode	ed bore hole)		$_{\rm Hc} = \gamma_{\rm Msp}^{1)}$		1	2,1 ⁴⁾				not adr	nissible	
²⁾ The partial safet ³⁾ The partial safet ⁴⁾ The partial safet ⁵⁾ Explanations se	her national regulations y factor $\gamma_2 = 1.0$ is includy y factor $\gamma_2 = 1.2$ is includy y factor $\gamma_2 = 1.4$ is include e section 1.2 ant Technical Specification	led. led. led.	he reinforc	ing bar								
Regarding design of po	ost-installed rebar as an	chor se	e chapter 4	.2					1			
Powers Injection s	ystem V12 for conc	rete										
Application with reinfor Design according to Characteristic values for	cing bar EN/TS 1992-4 <u>,</u> or tension loads in non-c	cracked	concrete u	nder sta	atic and	l quasi-	static a	ction		Anne	ex 18	



Table 12b: Desig in cra	gn according to acked concrete						es for	tensic	on load	ds
Anchor size reinforcing b	bar			Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure				1				1		
Characteristic tension resis according to Annex 4	stance, reinforcing bar	N _{Rk,s}	[kN]				$A_s \times f_{uk}$ ⁵⁾			
Partial safety factor		γ _{Ms,N} ¹⁾	•		CEN/TS	5 1992-4-	1 Section	4.4.3.1.1	, Eq. 4 ⁵⁾	
Combined pull-out and c	oncrete failure	•		•						
Characteristic bond resista	nce in cracked concrete	C20/25								
Temperature range I ⁴⁾ :	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm ²]	5,5	5,5	5,5	5,5	5,5	6,5	6,5
40°C/24°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm ²]	5,5	5,5	5,5		not adr	nissible	
Temperature range II ⁴⁾ :	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm ²]	4,0	4,0	4,0	4,0	4,0	4,5	4,5
80°C/50°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm²]	4,0	4,0	4,0		not adr	nissible	I
Temperature range III ⁴⁾ :	dry and wet concrete	$\tau_{Rk,cr}$	[N/mm²]	3,0	3,0	3,0	3,0	3,0	3,5	3,5
120°C/72°C	flooded bore hole	$\tau_{Rk,cr}$	[N/mm ²]	3,0	3,0	3,0		not adr	nissible	
	I	C30/37					1,04			
Increasing factors for conclusion Ψ_{c}	rete	C40/50					1,08			
		C50/60		-			1,10			
Factor according to CEN/TS 1992-4-5 Section	6.2.2.3	k ₈	[-]				7,2			
Concrete cone failure										
Factor according to CEN/TS 1992-4-5 Section	6.2.3.1	k _{cr}	[-]				7,2			
Edge distance		C _{cr,N}	[mm]				1,5 h _{ef}			
Axial distance		S _{cr,N}	[mm]				3,0 h _{ef}			
Splitting failure										
Edge distance		C _{cr,sp}	[mm]		1,0 ·	h _{ef} ≤2 ⋅h	$I_{ef}\left(2,5-\frac{1}{h}\right)$	$\left(\frac{h}{n_{ef}}\right) \le 2,4$	∙h _{ef}	
Axial distance		S _{cr,sp}	[mm]				2 c _{cr,sp}			
Partial safety factor (dry an	nd wet concrete)	$\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}^{-1)}$	•				1,8 ²⁾			
Partial safety factor (floode	d bore hole)	$\gamma_{Mp} = \gamma_{Mc} = \gamma_{Msp}{}^{1)}$			2,1 ³⁾			not adr	nissible	
²⁾ The partial safety ³⁾ The partial safety ⁴⁾ Explanations see	Int Technical Specific	uded. uded. ation for the rein	-							
Powers Injection sy Application with reinfor Design according to	cing bar EN/TS 1992-4,							An	nex 19)
Characteristic values for	or tension loads in cra	icked concrete u	Inder static	and quas	si-static a	action				



Table 13: Design according t in cracked and nor											
Anchor size reinforcing bar			Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Steel failure without lever arm											
Characteristic shear resistance, reinforcing bar according to Annex 4	V _{Rk,s}	[kN]				0,50	0 x A _s x f	f _{uk} ⁴⁾			
Partial safety factor	γ _{Ms,V} 1)			CE	V/TS 199	92-4-1 S	Section 4	4.3.1.1	, Eq. 5 +	· 6 ⁴⁾	
Ductility factor according to CEN/TS 1992-4-5 Section 6.3.2.1	k ₂						0,8				
Steel failure with lever arm											
Characteristic bending moment, reinforcing bar according to Annex 4	M ⁰ _{Rk,s}	[Nm]				1.2	2 ·W _{el} · f _ι	4) JK			
Partial safety factor	γ _{Ms,V} ¹⁾			CE	N/TS 199	92-4-1 S	Section 4	4.3.1.1	, Eq. 5 +	· 6 ⁴⁾	
Concrete pry-out failure											
Factor in equation (27) of CEN/TS 1992-4-5 Section 6.3.3	k ₃						2,0				
Partial safety factor	γ _{Mep} ¹⁾						1,50 ²⁾				
Concrete edge failure ³⁾											
Effective length of anchor	l _t	[mm]				l _t = m	iin(h _{et} ; 8	d _{nom})			
Outside diameter of anchor	d _{nom}	[mm]	8	10	12	14	16	20	24	27	30
Partial safety factor	γ _{Mc} ¹⁾						1,50 ²⁾				
¹⁾ In absence of other national reg ²⁾ The partial safety factor $\gamma_2 = 1.0$ ³⁾ See CEN/TS 1992-4-5 Section 6 ⁴⁾ f _{uk} , f _{yk} see relevant Technical Sp Regarding design of post-installed	is included. 5.3.4 secification for										
Powers Injection system V12 for con	crete								_	_	
Application with reinforcing bar Design according to CEN/TS 1992-4, Charac cracked concrete under static and quasi-stat		s for she	ear loac	ls in cra	acked a	nd non	-		Anne	ex 20	



Anchor size threa	aded rod		M 8	M 10	M 12	M 16	M 20	M24	M 27	м зо
Non-cracked con	crete C20	/25								
40°C/24°C ²⁾	δ _{N0}	[mm/(N/mm ²)]	0,021	0,023	0,026	0,031	0,036	0,041	0,045	0,049
40°C/24°C	$\delta_{N_{\infty}}$	[mm/(N/mm ²)]	0,030	0,033	0,037	0,045	0,052	0,060	0,065	0,07
80°C/50°C ²⁾	δ _{N0}	[mm/(N/mm ²)]	0,050	0,056	0,063	0,075	0,088	0,100	0,110	0,11
80°C/50°C	$\delta_{N\infty}$	[mm/(N/mm ²)]	0,072	0,081	0,090	0,108	0,127	0,145	0,159	0,17
120°C/72°C ²⁾	δ _{N0}	[mm/(N/mm ²)]	0,050	0,056	0,063	0,075	0,088	0,100	0,110	0,11
120°C/72°C	$\delta_{N\infty}$	[mm/(N/mm ²)]	0,072	0,081	0,090	0,108	0,127	0,145	0,159	0,17
Cracked concrete	e C20/25									
	δ _{N0}	[mm/(N/mm ²)]					0,0)70		
40°C/24°C ²⁾	$\delta_{N\infty}$	[mm/(N/mm ²)]		-			0,1	105		
80°C/50°C ²⁾	δ _{N0}	[mm/(N/mm ²)]					0,1	170		
80°C/50°C	$\delta_{N\infty}$	[mm/(N/mm ²)]		-			0,2	245		
120°C/72°C ²⁾	δ _{N0}	[mm/(N/mm ²)]					0,1	170		
120-0/72-0 /	$\delta_{N_{\infty}}$	[mm/(N/mm ²)]		-			0,2	245		

Displacement for short term load = $\delta_{N0} \cdot \tau_{Sd} / 1,4;$ Displacement for long term load = $\delta_{N_{o}} \cdot \tau_{Sd} / 1,4$; (τ_{Sd} : design bond strength) ²⁾ Explanations see section 1.2

Displacement for shear load threaded rod ³⁾ Table 15:

	aded rod		M 8	M 10	M 12	M 16	M 20	M24	M 27	M 30
For non-cracked	concrete	C20/25					1			
	δ _{V0}	[mm/(kN)]	0,06	0,06	0,05	0,04	0,04	0,03	0,03	0,03
All temperatures	δ_{V_∞}	[mm/(kN)]	0,09	0,08	0,08	0,06	0,06	0,05	0,05	0,05
For cracked cond	crete C20/	25	•							
	δνο	[mm/(kN)]			0,11	0,10	0,09	0,08	0,08	0,07
All temperatures	δ _{V∞}	[mm/(kN)]		-	0,17	0,15	0,14	0,13	0,12	0,10
Powers Injectio	-	V12 for concrete						Ar	inex 2	1



Anchor size r	einforci	ng bar	Ø8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Non-cracked	concret	e C20/25		1		1	1	I	I	1	
(0.0.2)	δ _{N0}	[mm/(N/mm ²)]	0,021	0,023	0,026	0,028	0,031	0,036	0,043	0,047	0,05
40°C/24°C ²⁾	$\delta_{N_{\infty}}$	[mm/(N/mm ²)]	0,030	0,033	0,037	0,041	0,045	0,052	0,061	0,071	0,07
80°C/50°C ²⁾	δ _{N0}	[mm/(N/mm ²)]	0,050	0,056	0,063	0,069	0,075	0,088	0,104	0,113	0,12
80°C/50°C	$\delta_{N\infty}$	[mm/(N/mm ²)]	0,072	0,081	0,090	0,099	0,108	0,127	0,149	0,163	0,18
120°C/72°C ²⁾	δ _{N0}	[mm/(N/mm ²)]	0,050	0,056	0,063	0,069	0,075	0,088	0,104	0,113	0,12
120 0/12 0	$\delta_{N\infty}$	[mm/(N/mm ²)]	0,072	0,081	0,090	0,099	0,108	0,127	0,149	0,163	0,18
Cracked cond	crete C2	0/25									
40°C/24°C ²⁾	δ _{N0}	[mm/(N/mm ²)]						0,070			
40°C/24°C -/	$\delta_{N\infty}$	[mm/(N/mm ²)]		-				0,105			
80°C/50°C ²⁾	δ _{N0}	[mm/(N/mm ²)]						0,170			
80°C/50°C	$\delta_{N\infty}$	[mm/(N/mm ²)]		-				0,245			
(0000/7000 2)	δ _{N0}	[mm/(N/mm ²)]						0,170			
		,		_							
Displacem	ent for sh ent for lor n bond st ns see se	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength)	_{Sd} / 1,4; _{Sd} / 1,4;	ads rei	nforcin	ng bar ^s	3)	0,245			
 ¹⁾ Calculation Displacem Displacem ^{(τ_{Sd}: desig Explanation} Table 17: 	n of the dia nent for sh nent for lor n bond sti ns see se Disp	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) ection 1.2	_{Sd} / 1,4; _{Sd} / 1,4;	ads reil Ø 10	nforcin Ø 12	n g bar [≎] Ø 14	3) Ø 16	0,245 Ø 20	Ø 25	Ø 28	Ø3
¹⁾ Calculation Displacem ^{(τ_{Sd}: desig ²⁾ Explanatio Table 17:}	n of the dia nent for sh nent for lor n bond sti ns see se Disp reinforci	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) action 1.2 lacement for sl ing bar	_{sd} / 1,4; _{sd} / 1,4; near lo a			-			Ø 25	Ø 28	Ø3
 ¹⁾ Calculation Displacem (TSd: desig ²⁾ Explanation Table 17: Anchor size r Non-cracked 	n of the dia nent for sh nent for lor n bond sti ns see se Disp reinforci	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) action 1.2 lacement for sl ing bar	_{sd} / 1,4; _{sd} / 1,4; near lo a			-			Ø 25 0,03	Ø 28	
¹⁾ Calculation Displacem Displacem (T _{Sd} : desig ²⁾ Explanation Table 17: Anchor size r Non-cracked All	n of the dia nent for sh nent for lor n bond stu ins see se Disp reinforcia	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) ection 1.2 lacement for sl ing bar e C20/25	s _d / 1,4; _{sd} / 1,4; near loa	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20			0,03
 ¹⁾ Calculation Displacem Displacem ^{(T}Sd: desig ²⁾ Explanation Table 17: Anchor size r Non-cracked All temperatures 	n of the dialent for shaten the for lor on bond strains see se $Disp$ reinforcia $\frac{\delta_{V0}}{\delta_{V\infty}}$	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) action 1.2 lacement for sl ing bar e C20/25 [mm/(kN)] [mm/(kN)]	sd / 1,4; sd / 1,4; near loa Ø 8 0,06	Ø 10 0,05	Ø 12 0,05	Ø 14 0,04	Ø 16 0,04	Ø 20 0,04	0,03	0,03	0,03
 ¹⁾ Calculation Displacem Displacem (Tsd: desig 2) Explanation Table 17: Anchor size r Non-cracked All temperatures Cracked condition 	n of the dialent for shaten the for lor on bond strains see se $Disp$ reinforcia $\frac{\delta_{V0}}{\delta_{V\infty}}$	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) action 1.2 lacement for sl ing bar e C20/25 [mm/(kN)] [mm/(kN)]	sd / 1,4; sd / 1,4; near loa Ø 8 0,06	Ø 10 0,05	Ø 12 0,05	Ø 14 0,04	Ø 16 0,04	Ø 20 0,04	0,03	0,03	Ø 32 0,03 0,04
 ¹⁾ Calculation Displacem (TSd: desig ²⁾ Explanation Table 17: Anchor size m Non-cracked 	n of the dia nent for sh nent for lor n bond stu ins see se Disp reinforcia	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) ection 1.2 lacement for sl ing bar e C20/25	s _d / 1,4; _{sd} / 1,4; near loa	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20			
 ¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size m Non-cracked All temperatures Cracked cond 	n of the dialent for shaent for lor n bond string see se Disp reinforcia δ_{V0} $\delta_{V\infty}$	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) ection 1.2 lacement for sl ing bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25	sd / 1,4; sd / 1,4; near loa Ø 8 0,06	Ø 10 0,05	Ø 12 0,05 0,08	Ø 14 0,04 0,06	Ø 16 0,04 0,06	Ø 20 0,04 0,05	0,03 0,05	0,03	0,(0,(
¹⁾ Calculation Displacem Displacem ²⁾ Explanatio Table 17: Anchor size r Non-cracked All emperatures Cracked cone	n of the dialent for sheent for lor n bond strans see se Disp reinforcia δv_0 δv_{∞} crete C24 δv_0	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) ection 1.2 lacement for sl ing bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25	sd / 1,4; sd / 1,4; near loa Ø 8 0,06	Ø 10 0,05	Ø 12 0,05 0,08	Ø 14 0,04 0,06	Ø 16 0,04 0,06	Ø 20 0,04 0,05	0,03 0,05	0,03	0,0 0,0 0,0
 ¹⁾ Calculation Displacem Displacem ²⁾ Explanatio Table 17: Anchor size r Non-cracked All emperatures Cracked cond All emperatures 	$\begin{array}{c} \text{n of the dial}\\ \text{n of the diall \\ \text{n of the dial}\\ n $	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ing term load = $\delta_{N\infty} \cdot \tau_s$ rength) action 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] [mm/(kN)]	sd / 1,4; hear loa Ø 8 0,06 0,09	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,0 0,0 0,0
 ¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size r Non-cracked All emperatures Cracked cond All emperatures ³⁾ Calculation Displacem 	n of the dialent for sheent for sheent for lor n bond strans see se $Disp$ reinforcia δv_0 δv_{∞} crete C24 δv_0 δv_{∞} n of the dialent for sh	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength) oction 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25 [mm/(kN)] splacement for design ort term load = $\delta_{V0} \cdot V$	sd / 1,4; hear loa Ø 8 0,06 0,09 - hoad /_ / 1,4;	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,0 0,0 0,0
 ¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size r Non-cracked All temperatures Cracked cone All temperatures ³⁾ Calculation Displacem 	n of the dialent for sheent for lor n bond strans see se Disp reinforcia δv_0 δv_{∞} crete C24 δv_{∞} n of the dialent for sheent for lor	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength) oction 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25 [mm/(kN)] splacement for design ort term load = $\delta_{V0} \cdot V$	sd / 1,4; hear loa Ø 8 0,06 0,09 - hoad /_ / 1,4;	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,0 0,0 0,0
¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size r Non-cracked All temperatures Cracked cone All temperatures ³⁾ Calculation Displacem Displacem	n of the dialent for sheent for lor n bond strans see se Disp reinforcia δv_0 δv_{∞} crete C24 δv_{∞} n of the dialent for sheent for lor	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength) oction 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25 [mm/(kN)] splacement for design ort term load = $\delta_{V0} \cdot V$	sd / 1,4; hear loa Ø 8 0,06 0,09 - hoad /_ / 1,4;	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,0; 0,04
 ¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size r Non-cracked All temperatures Cracked cone All temperatures ³⁾ Calculation Displacem Displacem 	n of the dialent for sheent for lor n bond strans see se Disp reinforcia δv_0 δv_{∞} crete C24 δv_{∞} n of the dialent for sheent for lor	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength) oction 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25 [mm/(kN)] splacement for design ort term load = $\delta_{V0} \cdot V$	sd / 1,4; hear loa Ø 8 0,06 0,09 - hoad /_ / 1,4;	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,0; 0,04
 ¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size r Non-cracked All temperatures Cracked cone All temperatures ³⁾ Calculation Displacem Displacem 	n of the dialent for sheent for lor n bond strans see se Disp reinforcia δv_0 δv_{∞} crete C24 δv_{∞} n of the dialent for sheent for lor	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength) oction 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25 [mm/(kN)] splacement for design ort term load = $\delta_{V0} \cdot V$	sd / 1,4; hear loa Ø 8 0,06 0,09 - hoad /_ / 1,4;	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,00
 ¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size r Non-cracked All temperatures Cracked cone All temperatures ³⁾ Calculation Displacem Displacem 	n of the dialent for sheent for lor n bond strans see se Disp reinforcia δv_0 δv_{∞} crete C24 δv_{∞} n of the dialent for sheent for lor	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength) oction 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25 [mm/(kN)] splacement for design ort term load = $\delta_{V0} \cdot V$	sd / 1,4; hear loa Ø 8 0,06 0,09 - hoad /_ / 1,4;	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,00
¹⁾ Calculation Displacem Displacem ²⁾ Explanation Table 17: Anchor size r Non-cracked All temperatures Cracked cone All temperatures ³⁾ Calculation Displacem Displacem	n of the dialent for sheent for lor n bond strans see se Disp reinforcia δv_0 δv_{∞} crete C24 δv_{∞} n of the dialent for sheent for lor	$[mm/(N/mm^2)]$ splacement for design ort term load = $\delta_{N0} \cdot \tau$ ort term load = $\delta_{N\infty} \cdot \tau_s$ rength) oction 1.2 lacement for sl ng bar e C20/25 [mm/(kN)] [mm/(kN)] 0/25 [mm/(kN)] splacement for design ort term load = $\delta_{V0} \cdot V$	sd / 1,4; hear loa Ø 8 0,06 0,09 - hoad /_ / 1,4;	Ø 10 0,05	Ø 12 0,05 0,08 0,11	Ø 14 0,04 0,06 0,11	Ø 16 0,04 0,06 0,10	Ø 20 0,04 0,05 0,09	0,03 0,05 0,08	0,03 0,04 0,07	0,00



Design according to TR 045; Design under seismic action

The decision of the selection of the seismic performance category is in the responsibility of each individual Member State.

Furthermore, the values of $a_g \cdot S$ assigned to the seismicity levels may be different in the National Annexes to EN 1998-1:2004 (EC8) compared to the values given in Table 18.

The recommended category C1 and C2 given in Table 18 are given in the case that no National requirements are defined.

Table 18: Recommended seismic performance categories for anchors

Seismicity level ^{a)}		Importance Class acc. to EN 1998-1:2004, 4.2.5						
	$a_g \cdot S^{c)}$	I	II	Ш	IV			
Very low ^{b)}	a _g ·S ≤ 0,05 g	No additional requirement						
Low ^{b)}	0,05 g < a _g ·S ≤ 0,1 g	C1	C1 ^{d)} or C2 ^{e)}		C2			
< Low ^{b)}	a _g ⋅S > 0,1 g	C1	C2					

^{a)} The values defining the seismicity levels may be found in the National Annex of EN 1998-1.

^{b)} Definition according to EN 1998-1:2004, 3.2.1.

^{c)} a_g = Design ground acceleration on Type A ground (EN 1998-1: 2004, 3.2.1),

S = Soil factor (see e.g. EN 1998-1: 2004, 3.2.2).

d) C1 attachments of non-structural elements

e) C2 for connections between structural elements of primary and/or secondary seismic members

Calculation of characteristic seismic resistance R_{k,seis}

Tension load:	$R_{k,seis} = \alpha_{gap} \cdot \alpha_{seis} \cdot \alpha_{N,seis} \cdot R^{0}_{k}$
	with $R_{k}^{0} = N_{Rk,s}$, $N_{Rk,p}$, $N_{Rk,c}$, $N_{Rk,sp}$ (calculation according to CEN/TS 1992-4 or TR029) $\alpha_{N,seis} =$ see Table 19 or Table 20 for $N_{Rk,s}$ and $N_{Rk,p}$ $\alpha_{N,seis} =$ 1,0 for $N_{Rk,c}$ and $N_{Rk,sp}$ $\alpha_{gap} =$ see Table 21 $\alpha_{seis} =$ see Table 21
Shear load:	$\mathbf{R}_{k,seis} = \alpha_{gap} \cdot \alpha_{seis} \cdot \alpha_{V,seis} \cdot \mathbf{R}^{0}_{k}$
	with $R_{k}^{0} = V_{Rk,s}$, $V_{Rk,c}$, $V_{Rk,cp}$ (calculation according to CEN/TS 1992-4 or TR029) $\alpha_{V,seis} =$ see Table 19 or Table 20 for $V_{Rk,s}$ $\alpha_{V,seis} = 1,0$ for $V_{Rk,c}$ and $V_{Rk,cp}$ $\alpha_{gap} =$ see Table 21 $\alpha_{seis} =$ see Table 21

Powers Injection system V12 for concrete

Design according to TR 045; Design under seismic action

Annex 23



Table 1	9: Reduction factors α _{N,se} for seismic design cate			nreaded	l rods					
Anchor si	ze threaded rods			M 12	2 M 1	6 N	/ 20	M24	M 27	M 30
Tension lo	oad									
Steel failure	e (N _{Rk,s})	$\alpha_{N,seis}$	[-]				1,0	0		
Combined pull-out and concrete failure ($N_{Rk,p}$)		α _{N,seis}	[-]	0,68	0,6	8	0,68	0,69	0,69	0,69
Shear load							·	,	,	
Shear roadSteel failure without lever arm ($V_{Rk,s}$) $\alpha_{V,seis}$ [-]						0,7	'0			
Table 2	0: Reduction factors α _{N,se} for seismic design cate			einforci	ng ba	r				
Anchor si	ze reinforcing bar			Ø 12	Ø 14	Ø 16	Ø 20) Ø 25	j Ø 28	Ø 32
Tension lo				I			1		•	
Steel failure	e (N _{Bk.s})	$\alpha_{N,seis}$	[-]				1,0			
	bull-out and concrete failure ($N_{Bk,p}$)	α _{N,seis}	[-]	0,68	0,68	0,68	0,68	0,69	0,69	0,69
Shear loa		11,3013	1.1	,	· 1	,	,	,	/	
	e without lever arm (V _{Rk,s})	α _{V.seis}	[-]				0,70)		
	is neuron actors ugap	and α_{sei}	_{is} for re	esistan	ce uno	aer se	eismic	actior	IS	
Loading	1: Reduction factors α _{gap} Failure modes	and α_{sei}	_{is} for re	esistan	ce uno α _{ga}		α _{seis} - S	Single	α _{seis} - Fa	
		and α_{sei}	is for re	esistan		p		Single ener		up
	Failure modes	and α_{sei}	is for re	esistan	α _{ga}	p	α _{seis} - S faste	Single ener	α _{seis} - Fa gro	up 0
	Failure modes Steel failure		is for re		α _{ga} 1,0	p	α _{seis} - S faste 1,	Single ener 0 0	α _{seis} - Fa gro 1,	up 0 35
Loading	Failure modes Steel failure Pull-out failure		is for re		α _{ga} 1,0 1,0	p	α _{seis} - faste 1, 1,	Single ener 0 0 0	α _{seis} - Fa gro 1, 0,8	up 0 35 35
Loading	Failure modes Steel failure Pull-out failure Combined pull-out and concrete fa Concrete cone failure Splitting failure		is for re		α _{ga} 1,0 1,0 1,0 1,0 1,0	p	α _{seis} - faste 1, 1, 1, 0,8 1,	Single ener 0 0 0 0 35 0	α _{seis} - Fa gro 1, 0,ξ 0,ζ 0,ζ	up 0 35 35 75 35
Loading	Failure modes Steel failure Pull-out failure Combined pull-out and concrete fa Concrete cone failure Splitting failure Steel failure without lever arm		is for re		α _{ga} 1,0 1,0 1,0 1,0 1,0 0,5	p)))))))))))))))))))	α _{seis} - S faste 1, 1, 1, 1, 0,8 1, 1,	Single ener 0 0 0 35 0 0 0	α _{seis} - Fa gro 1, 0,ξ 0,7 0,ξ 0,ξ	up 0 35 35 75 35 35
Loading	Failure modes Steel failure Pull-out failure Combined pull-out and concrete fa Concrete cone failure Splitting failure Steel failure without lever arm Steel failure with lever arm		is for re		α _{ga} 1,0 1,0 1,0 1,0 1,0 0,5 NPD	p	α _{seis} - \$ faste 1, 1, 1, 0,ξ 1, 1, 1, NPI	Single ener 0	α _{seis} - Fa gro 1, 0,8 0,7 0,8 0,7 0,8 0,8 0,8	up 0 35 35 35 35 35 35 2 ²⁾
Loading Tension	Failure modes Steel failure Pull-out failure Combined pull-out and concrete fa Concrete cone failure Splitting failure Steel failure without lever arm		is for re		α _{ga} 1,0 1,0 1,0 1,0 1,0 0,5	p	α _{seis} - S faste 1, 1, 1, 1, 0,8 1, 1,	Single ener 0 0 0 0 35 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	α _{seis} - Fa gro 1, 0,ξ 0,7 0,ξ 0,ξ	up 0 35 35 35 35 35 35 2 ²⁾ 35
Loading Tension Shear ¹⁾ The lir ²⁾ ^{$\alpha_{gap} =$ No Pe}	Failure modes Steel failure Pull-out failure Combined pull-out and concrete fa Concrete cone failure Splitting failure Steel failure without lever arm Steel failure with lever arm Concrete edge failure	ailure e is given ir n fastener a	יד TR 029	Table 4.1	α _{ga} 1,0 1,0 1,0 1,0 1,0 0,5 0,5 0,5	p	α _{seis} - \$ faste 1, 1, 1, 0,ε 1, 1, 1, NPE 1,	Single ener 0 0 0 0 35 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	α _{seis} - Fa gro 1, 0,8 0,7 0,8 0,8 0,8 0,8 0,8	up 0 35 35 35 35 35 35 2 ²⁾ 35