



Approval body for construction products and types of construction

#### **Bautechnisches Prüfamt**

An institution established by the Federal and Laender Governments



## European Technical Assessment

English translation prepared by DIBt - Original version in German language

#### **General Part**

Technical Assessment Body issuing the European Technical Assessment:

Trade name of the construction product

Product family to which the construction product belongs

Manufacturer

Manufacturing plant

This European Technical Assessment contains

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of

Deutsches Institut für Bautechnik

ETA-13/0775

of 17 May 2018

Sormat Injection System ITH-Ve for rebar connection

Systems for post-installed rebar connections with mortar

Sormat Oy Harjutie 5 21290 RUSKO FINNLAND

SORMAT OY, Plant 8

21 pages including 3 annexes which form an integral part of this assessment

EAD 330087-00-0601

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#### Specific Part

#### 1 Technical description of the product

The subject of this European Technical Assessment is the post-installed connection, by anchoring or overlap connection joint, of reinforcing bars (rebars) in existing structures made of normal weight concrete, using the "Sormat Injection system ITH-Ve for rebar connection" in accordance with the regulations for reinforced concrete construction.

Reinforcing bars made of steel with a diameter  $\phi$  from 8 to 32 mm or the tension anchor ZA from sizes M12 to M24 according to Annex A and injection mortar ITH-Ve are used for rebar connections. The rebar is placed into a drilled hole filled with injection mortar and is anchored via the bond between rebar, injection mortar and concrete.

The product description is given in Annex A.

## 2 Specification of the intended use in accordance with the applicable European assessment Document

The performances given in Section 3 are only valid if the anchor is used in compliance with the specifications and conditions given in Annex B.

The verifications and assessment methods on which this European Technical Assessment is based lead to the assumption of a working life of the rebar connection of at least 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

#### 3 Performance of the product and references to the methods used for its assessment

#### 3.1 Mechanical resistance and stability (BWR 1)

Essential characteristic	Performance	
Characteristic resistance under static and quasi-static loading	See Annex C 1	

#### 3.2 Safety in case of fire (BWR 2)

Essential characteristic Performance	
Reaction to fire Class A1	
sistance to fire See Annex C 2 and C 3	

## 4 Assessment and verification of constancy of performance (AVCP) system applied, with reference to its legal base

In accordance with European Assessment Document EAD No. 330087-00-0601, the applicable European legal act is: [96/582/EC].

The system(s) to be applied is (are): 1



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5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable European Assessment Document

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited with Deutsches Institut für Bautechnik.

Issued in Berlin on 17 May 2018 by Deutsches Institut für Bautechnik

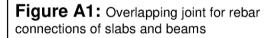
BD Dipl.-Ing. Andreas Kummerow Head of Department *beglaubigt:* Baderschneider

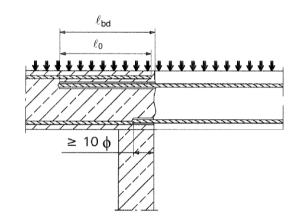
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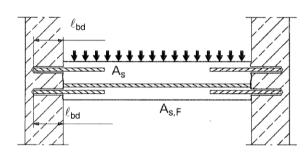


### Installation post installed rebar

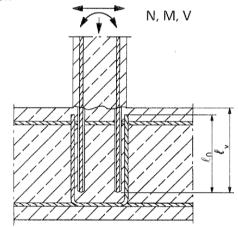




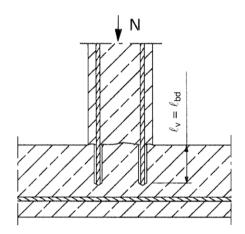
**Figure A3:** End anchoring of slabs or beams (e.g. designed as simply supported)

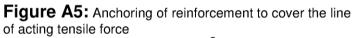


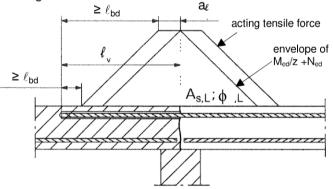
**Figure A2:** Overlapping joint at a foundation of a wall or column where the rebars are stressed in tension



**Figure A4:** Rebar connection for components stressed primarily in compression. The rebars sre stressed in compression







#### Note to Figure A1 to A5:

In the Figures no transverse reinforcement is plotted, the transverse reinforcement shall comply with EN 1992-1-1:2004+AC:2010.

Preparing of joints according to Annex B 2

 Sormat Injection System ITH-Ve for rebar connection

 Product description

 Installed condition and examples of use for rebars

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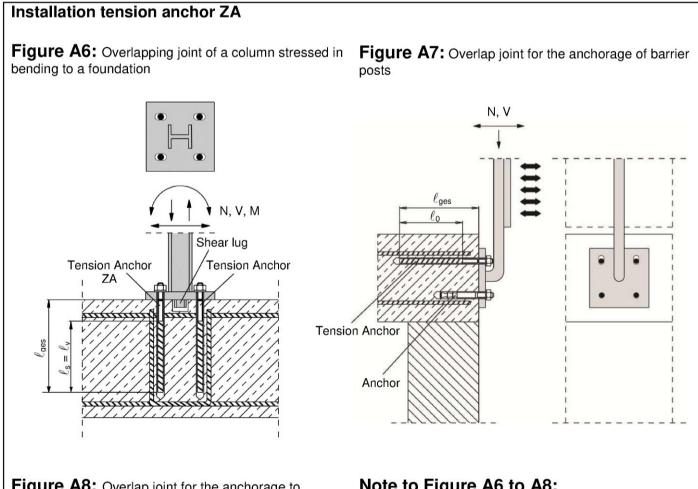
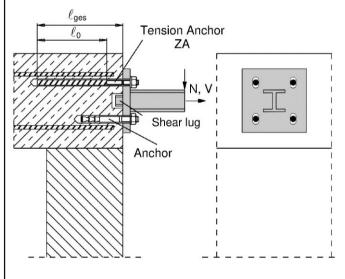


Figure A8: Overlap joint for the anchorage to centilever members



## Note to Figure A6 to A8:

In the Figures no transverse reinforcement is plotted, the transverse reinforcement shall comply with EN 1992-1-1:2002+AC:2010

#### Sormat Injection System ITH-Ve for rebar connection

#### **Product description** Installed condition and examples of use for tension anchors ZA

Annex A 2

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Sormat Injection System ITH-Ve	:	
Injection mortar: ITH-Ve Typ "coaxial": 150 ml, 280 ml, 300 ml up to 333 ml and 380 ml up to 420 ml cartridge	code, shelf lif code, curing-	Ve, processing notes, charge- fe, storage temperature, hazard- and processing time (depending erature), optional with travel scale
<b>Type "side-by-side":</b> 235 ml, 345 ml and 825 ml cartridge	code, shelf lif	Ve, processing notes, charge- fe, storage temperature, hazard- and processing time (depending erature), optional with travel scale
Static Mixer		
CRW 14W		
TAH 18W		
Piston plug VS and mixer extension		
Reinforcing bar (rebar): ø8 t	to ø32	
Tension Anchor ZA: M12 to	M24	
000 \$ \$ 0000	000000	
Sormat Injection System ITH-Ve fo	r rebar connection	
<b>Product description</b> Injection mortar / Static mixer / Rebar	/ Tension Anchor ZA	Annex A 3

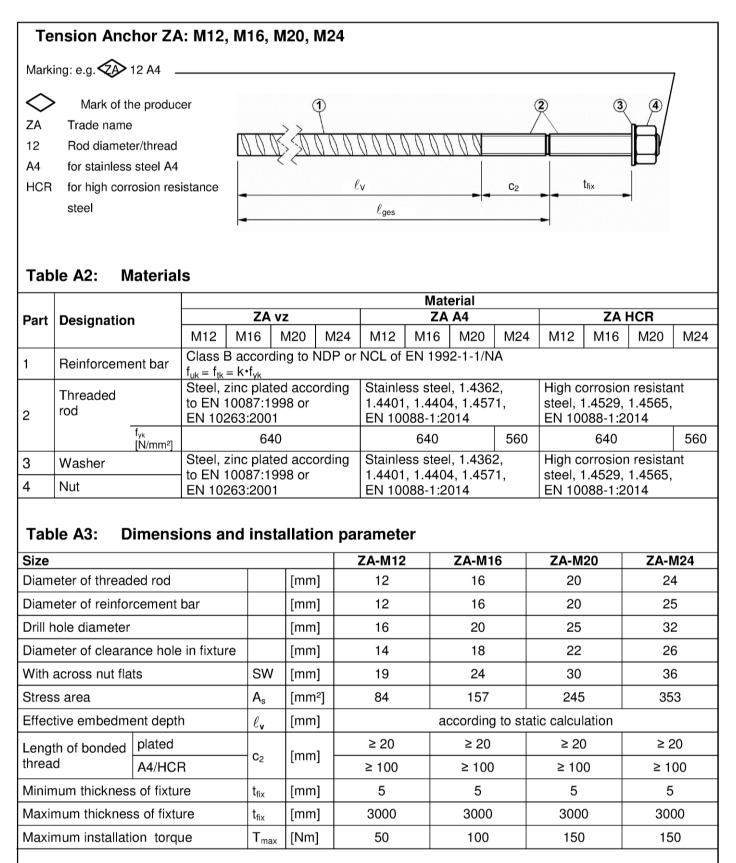


Reinforcing bar (rebar): ø8, ø10, ø12, ø14, ø16, ø20, ø22, ø24, ø25, ø28, ø32				
<ul> <li>Minimum value of related rip area f<sub>R,min</sub> according</li> <li>Rib height of the bar shall be in the range 0,05¢ s (¢: Nominal diameter of the bar; h: Rip height of t</li> <li>Table A1: Materials</li> </ul>	≤ h ≤ 0,07φ			
Designation	Material			
Rebar EN 1992-1-1:2004+AC:2010, Annex C	Bars and de-coiled rods class B or C $f_{yk}$ and k according to NDP or NCL of EN 1992-1-1/NA $f_{uk} = f_{tk} = k \cdot f_{yk}$			

Sormat Injection System ITH-Ve for rebar connection

Product description Specifications Rebar Annex A 4





#### Sormat Injection System ITH-Ve for rebar connection

## Product description

Specifications Tension Anchor ZA

Annex A 5



## Specifications of intended use

#### Anchorages subject to:

- Static and quasi-static loads.
- Fire exposure

#### Base materials:

- Reinforced or unreinforced normal weight concrete according to EN 206-1:2000.
- Strength classes C12/15 to C50/60 according to EN 206-1:2000.
- Maximum chloride concrete of 0,40% (CL 0.40) related to the cement content according to EN 206-1:2000.
- · Non-carbonated concrete.

Note: In case of a carbonated surface of the existing concrete structure the carbonated layer shall be removed in the area of the post-installed rebar connection with a diameter of  $\phi$  + 60 mm prior to the installation of the new rebar.

The depth of concrete to be removed shall correspond to at least the minimum concrete cover in accordance with EN 1992-1-1:2004+AC:2010.

The foregoing may be neglected if building components are new and not carbonated and if building components are in dry conditions.

#### **Temperature Range:**

• - 40°C to +80°C (max. short term temperature +80°C and max long term temperature +50°C).

#### Use conditions (Environmental conditions):

• Structures subject to dry internal conditions or subject to external atmospheric exposure (including industrial and marine environment) and to permanently damp internal condition, if no particular aggressive conditions exist

(stainless steel or high corrosion resistant steel).

• Structures subject to external atmospheric exposure and to permanently damp internal condition, if other particular aggressive conditions exist (high corrosion resistant steel).

Note: Particular aggressive conditions are e.g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with extreme chemical pollution (e.g. in desulphurization plants or road tunnels where de-icing materials are used).

#### Design:

- · Anchorages are designed under the responsibility of an engineer experienced in anchorages and concrete work.
- Verifiable calculation notes and drawings are prepared taking account of the forces to be transmitted.
- Design according to EN 1992-1-1:2004+AC:2010, EN 1992-1-2:2004+AC:2008 and Annex B 2 and B 3.
- The actual position of the reinforcement in the existing structure shall be determined on the basis of the construction documentation and taken into account when designing.

#### Installation:

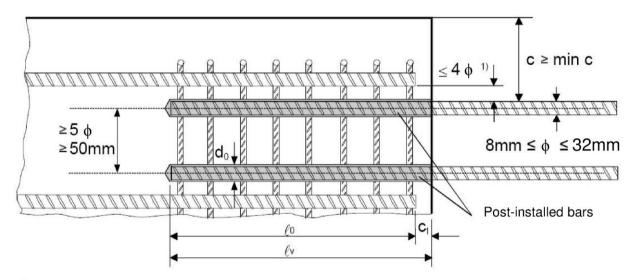
- Dry or wet concrete.
- · It must not be installed in flooded holes.
- Hole drilling by hammer drill (HD), hollow drill (HDB) or compressed air drill mode (CD).
- The installation of post-installed rebar resp. tension anchors shall be done only by suitable trained installer and under supervision on site; the conditions under which an installer may be considered as suitable trained and the conditions for supervision on site are up to the Member States in which the installation is done.
- Check the position of the existing rebars (if the position of existing rebars is not known, it shall be determined using a rebar detector suitable for this purpose as well as on the basis of the construction documentation and then marked on the building component for the overlap joint).

Sormat Injection System ITH-Ve for rebar connection	
Intended use Specifications	Annex B 1



### Figure B1: General construction rules for post-installed rebars

- · Only tension forces in the axis of the rebar may be transmitted
- The transfer of shear forces between new concrete and existing structure shall be designed additionally according to EN 1992-1-1:2004+AC:2010.
- The joints for concreting must be roughened to at least such an extent that aggregate protrude.



<sup>1)</sup> If the clear distance between lapped bars exceeds 4¢, then the lap length shall be increased by the difference between the clear bar distance and 4¢.

The following applies to Figure B1:

- c concrete cover of post-installed rebar
- c1 concrete cover at end-face of existing rebar
- min c minimum concrete cover according to Table B1 and to EN 1992-1-1:2004+AC:2010, Section 4.4.1.2 diameter of post-installed rebar
- $\ell_0$  lap length, according to EN 1992-1-1:2004+AC:2010, Section 8.7.3
- $\ell_v$  effective embedment depth,  $\geq \ell_0 + c_1$
- d<sub>0</sub> nominal drill bit diameter, see Annex B 6

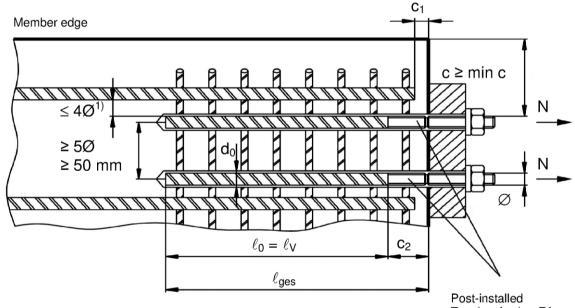
#### Intended use

General construction rules for post-installed rebars



### Figure B2: General construction rules for tension anchors ZA

- The length of the bonded-in thread may be not be accounted as anchorage
- Only tension forces in the direction of the bar axis may be transmitted by the tension anchor ZA
- · The tension force must be transferred via an overlap joint to the reinforcement in the building part.
- The transfer of shear forces shall be ensured by appropriate additional measures, e.g shear lugs or by anchors with an European technical assessment.
- In the anchor plate, the holes for the tension anchors shall be executed as elongated holes with axis in the direction of the shear force.



Tension Anchor ZA

<sup>1)</sup> If the clear distance between lapped bars exceeds 4¢, then the lap length shall be increased by the difference between the clear bar distance and 4¢.

The following applies to Figure B2:

- c concrete cover of tension anchor ZA
- c1 concrete cover at end-face of existing rebar
- c<sub>2</sub> Length of bonded thread
- min c minimum concrete cover according to Table B1 and to EN 1992-1-1:2004+AC:2010, Section 4.4.1.2
- φ diameter of tension anchor
- $\ell_0$  lap length, according to EN 1992-1-1:2004+AC:2010, Section 8.7.3
- $\ell_v$  effective embedment depth,  $\geq \ell_0 + c_1$
- $\ell_{ges}$  overall embedment depth,  $\geq \ell_0 + c_2$
- d<sub>0</sub> nominal drill bit diameter, see Annex B 6

#### Sormat Injection System ITH-Ve for rebar connection

### Intended use

General construction rules for tension anchors



Table B1: Minimum concrete cover min c <sup>1)</sup> of post-installed rebar depending of drilling method       Drilling aid				
Rebar diameter	Without drilling aid	With drilling aid		
< 25 mm	$30 \text{ mm} + 0,06 \cdot \ell_{v} \ge 2 \phi$	$30 \text{ mm} + 0.02 \cdot \ell_{v} \ge 2 \phi$		
≥ 25 mm	$40 \text{ mm} + 0,06 \cdot \ell_{v} \geq 2 \phi$	$40 \text{ mm} + 0.02 \cdot \ell_{v} \geq 2 \phi$		
< 25 mm	50 mm + 0,08 · $\ell_v$	50 mm + 0,02 · $\ell_v$		
≥ 25 mm	60 mm + 0,08 · <b>ℓ</b> <sub>v</sub>	60 mm + 0,02 · $\ell_v$		
	ebar depending o Rebar diameter < 25 mm ≥ 25 mm < 25 mm	Bebar depending ofRebar diameterWithout drilling aid< 25 mm		

see Annex B2, Figures B1 and Annex B3, Figure B2

Comments: The minimum concrete cover acc. EN 1992-1-1:2004+AC:2010 must be observed

#### Table B2: maximum embedment depth $\ell_{v,max}$

Rebar	Tension anchor	0	
φ	φ	$\ell_{v,max}$ [mm]	
8 mm		1000	
10 mm		1000	
12 mm	M12	1200	
14 mm		1400	
16 mm	M16	1600	
20 mm	M20	2000	
22 mm		2000	
24 mm		2000	
25 mm	M24	2000	
28 mm		1000	
32 mm		1000	

#### Table B3: Base material temperature, gelling time and curing time

Concrete temperature		perature	Gelling working time <sup>1)</sup>	Minimum curing time in dry concrete	Minimum curing time in wet concrete
-10°C	to	-6°C	90 min <sup>2)</sup>	24 h	48 h
- 5 °C	to	- 1 °C	90 min <sup>3)</sup>	14 h	28 h
0 °C	to	+ 4 °C	45 min <sup>3)</sup>	7 h	14 h
+ 5 °C	to	+ 9 °C	25 min <sup>3)</sup>	2 h	4 h
+ 10 °C	to	+ 19 °C	15 min <sup>3)</sup>	80 min	160 min
+ 20 °C	to	+ 24 °C	6 min <sup>3)</sup>	45 min	90 min
+ 25 °C	to	+ 29 °C	4 min <sup>3)</sup>	25 min	50 min
+ 30 °C	to	+ 40 °C	2,5 min <sup>4)</sup>	15 min	30 min

<sup>1)</sup>  $t_{gel}$ : maximum time from starting of mortar injection to completing of rebar setting. <sup>2)</sup> Cartridge temperature <u>must</u> be at minimum +15°C <sup>3)</sup> Cartridge temperature <u>must</u> be between +5°C and +25°C

<sup>4)</sup> Cartridge temperature <u>must</u> be below +20°C

#### Sormat Injection System ITH-Ve for rebar connection

## Intended use

Minimum concrete cover Maximum embedment depth / working time and curing times

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Cartridge type/size	Hand tool		Pneumatic tool	
Coaxial cartridges 150, 280, 300 up to 333 ml				
	e.g. Type H	297 or H244C	e.g. Type TS 492 X	
Coaxial cartridges 380 up to 420 ml		R		
	e.g. Type CCM 380/10	e.g. Type H 285 or H244C	e.g. Type TS 485 LX	
Side-by-side cartridges 235, 345 ml		R		
	e.g. Type CBM 330A	e.g. Type H 260	e.g. Type TS 477 LX	
Side-by-side cartridge 825 ml	-	-		
			e.g. Type TS 498X	

All cartridges could also be extruded by a battery tool.

Sormat Injection System ITH-Ve for rebar connection	
Intended Use Dispensing tools	Annex B 5



A) Bore hole	drilling			
	1. Drill a hole into the base material to selected reinforcing bar with carbid (CD). In case of aborted drill hole: t	e hammer drill (HD	) or a compre	essed air drill
		Rebar - φ	ZΑ- Φ	Drill - Ø [mm]
1		8 mm	•	12
· · · · · · · · · · · · · · · · · · ·		10 mm		14
		12 mm	M12	16
Statement of the local division of the local		14 mm		18
		16 mm	M16	20
		20 mm	M20	25
		22 mm		28
		24 mm		32
		25 mm	M24	32
Hammer drill (H		28 mm		35
Hollow drill (HD	В)	32 mm		40
-	cleaning (HD, HDB and CD)			
MAC: Cleaning for	bore hole diameter $d_0 \le 20$ mm and bore h	ole depth $h_0 \le 10c$	3 <sub>s</sub>	
2a 4x	2a. Starting from the bottom or back of the (Annex B 7) a minimum of four times.	bore hole, blow the	e hole clean a	a hand pump
2b 4×	2b. Check brush diameter (Table B5). Brus d <sub>b,min</sub> (Table B5) a minimum of four tin If the bore hole ground is not reached	nes in a twisting mo	otion.	
2c 4x	2c. Finally blow the hole clean again with times.	a hand pump (Ann	ex B 7) a mir	imum of four
CAC: Cleaning for	all bore hole diameter and bore hole dept	h		
2a 4x	2a. Starting from the bottom or back of the compressed air (min. 6 bar) (Annex B stream is free of noticeable dust. If the extension shall be used.	7) a minimum of fo	our times unti	return air
2b 4x	2b. Check brush diameter (Table B5). Brus d <sub>b,min</sub> (Table B5) a minimum of four tin If the bore hole ground is not reached (Table B5).	nes.		
2c 4x	2c. Finally blow the hole clean again with minimum of four times until return air ground is not reached an extension sl	stream is free of no		
Sormat Injection S	stem ITH-Ve for rebar connection			

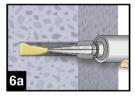
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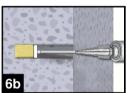


Table B5 Brush RE	: Cleanin <sup>3T:</sup>	g tools L			₽	SDS Plus Ac	dapter:		
		MAAA	MAAA	<u>baaa</u> a	d d	b			
Brush e	xtension:								
φ Rebar	φ Tension anchor	d₀ Drill bit - Ø		l₀ h - Ø	d <sub>b,min</sub> min. Brush - Ø				
(mm)	(mm)	(mm)		(mm)					
8		12	RBT12	14	12,5	Hand I	pump (volume 750 ml)		
10		14	RBT14	16	14,5	, include			
12	M12	16	RBT16	18	16,5				
14	MAG	18	RBT18	20	18,5				
16 20	M16 M20	20 25	RBT20 RBT25	22 27	20,5				
20	IVIZU	25	RBT28	30	25,5 28,5				
24		32	RBT32	34	32,5		•		
25	M24	32	RBT32	34	32,5				
28		35	RBT35	37	35,5	Rec. c	ompressed air tool		
32		40	RBT40	41,5	40,5		slide valve (min 6 bar)		
C) Pr		the cor For eve	the suppli rect dispe	ed static-i nsing tool g interrup	tion longer tl	han the recom	dge and load the cartridge into nmended working time w static-mixer shall be used.		
4	4 Prior to inserting the reinforcing bar into the filled bore hole, the position of the embedment depth shall be marked (e.g. with tape) on the reinforcing bar and insert bar in empty hole to verify hole and depth $\ell_v$ . The reinforcing bar should be free of dirt, grease, oil or other foreign material.								
5	min. 3 full stroke	shows	a consiste	ent grey co		ninimum of th	It separately the mortar until it iree full strokes, and discard non-		
Sormat Injection System ITH-Ve for rebar connection									
	<b>Jse</b> instruction: ( n of bar and (	Annex B 7							



### D) Filling the bore hole





6. Starting from the bottom or back of the cleaned anchor hole fill the hole up to approximately two-thirds with adhesive. Slowly withdraw the static mixing nozzle as the hole fills to avoid creating air pockets. For embedment larger than 190 mm an extension nozzle shall be used.

For overhead and horizontal installation and bore holes deeper than 240 mm a piston plug and the appropriate mixer extension must be used.

Observe the gel-/ working times given in Table B3.

#### Table B6: Piston plugs, max anchorage depth and mixer extension

	Tension					Cartri All s	Cartridge: side-by-side (825 ml)			
Bar size	anchor			Piston plug	Hand or b	attery tool	Pneumatic tool		Pneumatic tool	
ф	ф	HD, HDB	CD	P5	I <sub>v,max</sub>	Mixer extension	I <sub>v,max</sub>	Mixer extension	I <sub>v,max</sub>	Mixer extension
[mm]	[mm]	[m	m]		[cm]		[cm]		[cm]	
8		12	-	-			80		80	VL 10/0,75
10		14	VS14	VS14					100	
12	M12	1	6	VS16	VS16 70		100		120	-
14		18		VS18					140	
16	M16	2	0	VS20		VL 10/0,75		VL 10/0,75	160	VL 16/1,8
20	M20	25	VS25	VS25			70		200	
22		2	8	VS28						
24		3	2	VS32	50		50			
25	M24	3	2	VS32	50					
28		3	5	VS35					200	
32		4	0	VS40					200	
level mark										
			ℓm							
$\ell_{v}, \ell_{e,ges}$										
Injection tool must be marked by mortar level mark $\ell_m$ and anchorage depth $\ell_v$ resp. $\ell_{e,ges}$ with tape or marker.										
Quick estimation: $\ell_m = 1/3 \cdot \ell_v$										
Continue injection until the mortar level mark $\ell_m$ becomes visible.										
Optimum mortar volume: $\ell_m = \ell_v \text{ resp. } \ell_{e,ges} \cdot \left( 1, 2 \cdot \frac{\phi^2}{d_0^2} - 0, 2 \right) \text{ [mm]}$										
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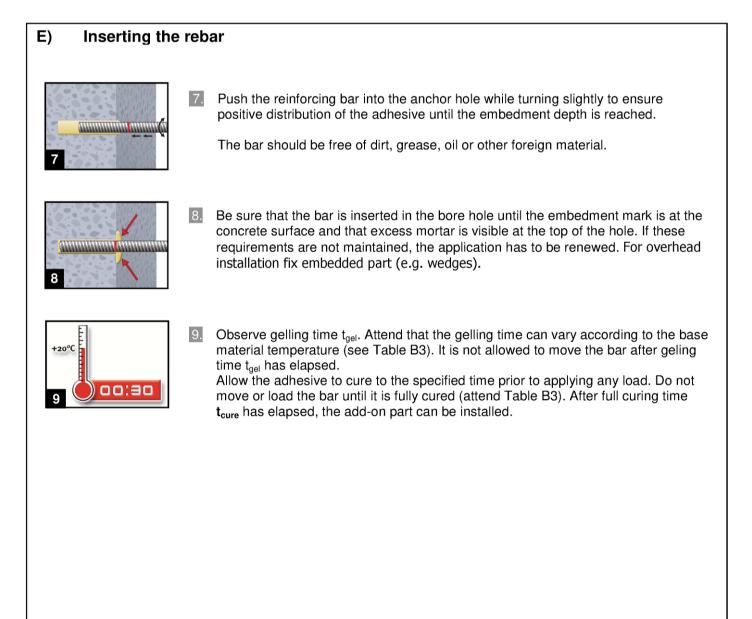
#### Intended Use

Installation instruction: Filling the bore hole

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#### Sormat Injection System ITH-Ve for rebar connection

Intended Use Installation instruction: Inserting rebar



#### Minimum anchorage length and minimum lap length The minimum anchorage length $\ell_{b,min}$ and the minimum lap length $\ell_{0,min}$ according to EN 1992-1-1:2004+AC:2010 (*l*<sub>b,min</sub> acc. to Eq. 8.6 and Eq. 8.7 and *l*<sub>0,min</sub> acc. to Eq. 8.11) shall be multiply by the amplification factor $\alpha_{lb}$ according to Table C1. Table C1: Amplification factor α<sub>lb</sub> related to concrete class and drilling method **Concrete class Drilling method** Bar size Amplification factor α<sub>lb</sub> Hammer drilling (HD), hollow 8 mm to 32 mm C12/15 to C50/60 drilling (HDB) and 1,0 ZA-M12 to ZA-M24 compressed air drilling (CD) Table C2: Reduction factor k<sub>b</sub> for all drilling methods Rebar - Ø Concrete class C12/15 C16/20 C20/25 C25/30 C30/37 C35/45 C40/50 C45/55 C50/60 φ 8 to 25 mm 1,0 ZA-M12 to ZA-M24 28 to 32 mm 1,0 0,92 0,86 Table C3: Design values of the ultimate bond stress f<sub>bd.PIR</sub> in N/mm<sup>2</sup> for all drilling methods and for good conditions $\mathbf{f}_{bd,PIR} = \mathbf{k}_b \cdot \mathbf{f}_{bd}$ with $f_{bd}$ : Design value of the ultimate bond stress in N/mm<sup>2</sup> considering the concrete classes and the rebar diameter according to EN 1992-1-1:2004+AC:2010. (for all other bond conditions multiply the values by 0.7) k<sub>b</sub>: Reduction factor according to Table C2 Rebar - Ø Concrete class C12/15 C16/20 C25/30 C30/37 C50/60 φ C20/25 C35/45 C40/50 C45/55 8 to 25 mm 1.6 2.0 2.3 2.7 3.0 3.4 3.7 4.0 4.3 ZA-M12 to ZA-M24 28 to 32 mm 2,0 2,3 3,0 1,6 2,7 3,4 3,7 3,7 3,7 Sormat Injection System ITH-Ve for rebar connection Annex C 1 Performances Amplification factor $\alpha_{lb}$

Design values of ultimate bond resistance fbd.PIR



#### Design value of the ultimate bond stress fbd,fi under fire exposure for concrete classes C12/15 to C50/60, (all drilling methods): The design value of the bond strength f<sub>bd,fi</sub> under fire exposure has to be calculated by the following equation: $\mathbf{f}_{bd,fi} = \mathbf{k}_{fi}(\mathbf{\theta}) \cdot \mathbf{f}_{bd,PIR} \cdot \mathbf{\gamma}_{c} / \mathbf{\gamma}_{M,fi}$ $k_{fi}(\theta) = 18,88 \cdot e^{(\theta \cdot \cdot 0,016)} / (f_{bd,PIR} \cdot 4,3) \leq 1,0$ θ ≤ 243°C: with: $\theta > 243^{\circ}C$ : $k_{fi}(\theta) = 0$ Design value of the ultimate bond stress in case of fire in N/mm<sup>2</sup> f<sub>bd,fi</sub> θ Temperature in °C in the mortar layer. k<sub>fi</sub>(θ) Reduction factor under fire exposure. Design value of the ultimate bond stress in N/mm<sup>2</sup> in cold condition according to Table C3 f<sub>bd,PIR</sub> considering the concrete classes, the rebar diameter and the bond conditions according to EN 1992-1-1:2004+AC:2010. partially safety factor according to EN 1992-1-1:2004+AC:2010 $\gamma_{\rm c}$ partially safety factor according to EN 1992-1-2:2004+AC:2008 ΥM,fi

For evidence under fire exposure the anchorage length shall be calculated according to EN 1992-1-1:2004+AC:2010 Equation 8.3 using the temperature-dependent ultimate bond stress  $f_{bd,fi}$ .

# Example graph of Reduction factor $k_{fi}(\theta)$ for concrete classes C20/25 for good bond conditions:

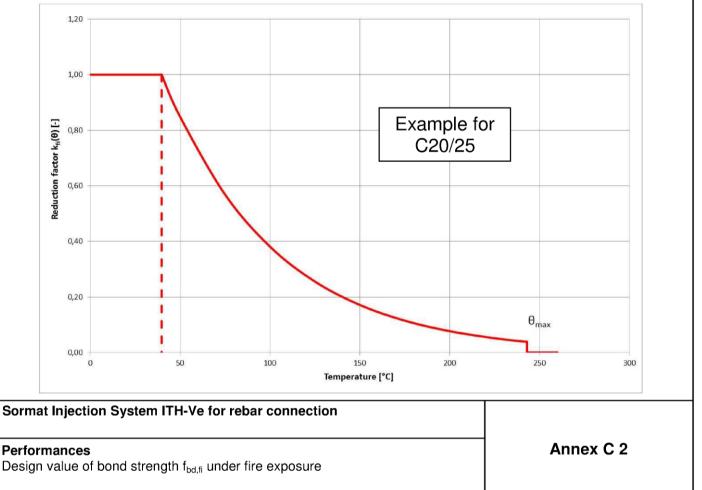




Table C4:	Characteristic tension strength for tension anchor ZA under fire exposure,							
	concrete cl	asses C12/	15 to C50/60,	according to Te	echnical Report T	<sup>-</sup> R 020		
Tension Anch	or			M12	M16	M20	M24	
Steel, zinc plate	ed (ZA vz)						-	
Characteristic steel strength	R30	σ <sub>Rk,s,fi</sub>		20				
	R60		[N1/mm 2]	15				
	R90		[N/mm²]	13				
	R120				1	0		
Stainless Steel	(ZA A4 or Z	A HCR)						
Characteristic steel strength	R30	- <b>σ</b> <sub>Rk,s,fi</sub>			3	0		
	R60		[N1/mm2]	25				
	R90		[N/mm²] —	20				
	R120				1	6		

## Design value of the steel strength $\sigma_{\mbox{\tiny Rd},\mbox{\tiny s,fi}}$ under fire exposure

The design value of the steel strength  $\sigma_{\rm Rd,s,fi}$  under fire exposure has to be calculated by the following equation:

 $\sigma_{\rm Rd,s,fi} = \sigma_{\rm Rk,s,fi} \; / \; \gamma_{\rm M,fi}$ 

with:

$\sigma_{Rk,s,fi}$	characteristic steel strength according to Table C4
ŶM,fi	partially safety factor according to EN 1992-1-2:2004+AC:2008

Sormat Injection System ITH-Ve for rebar connection		
Performances	Annex C 3	
Design value of the steel strength $\sigma_{\rm Rd,s,fi}$ for tension anchor ZA under fire exposure		