



Approval body for construction products and types of construction

Bautechnisches Prüfamt

An institution established by the Federal and Laender Governments



European Technical Assessment

ETA-17/0513 of 5 February 2021

English translation prepared by DIBt - Original version in German language

General Part

Technical Assessment Body issuing the European Technical Assessment:

Trade name of the construction product

Product family to which the construction product belongs

Manufacturer

Manufacturing plant

This European Technical Assessment contains

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of

This version replaces

Deutsches Institut für Bautechnik

Injection System SPIT VIPER XTREM

Systems for post-installed rebar connections with mortar

SPIT Route de Lyon 26500 BOURG-LÉS-VALENCE FRANKREICH

SPIT

20 pages including 3 annexes which form an integral part of this assessment

EAD 330087-01-0601, Edition 01/2021

ETA-17/0513 issued on 27 October 2017



European Technical Assessment ETA-17/0513 English translation prepared by DIBt

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Specific Part

1 Technical description of the product

The subject of this European Technical Assessment is the post-installed connection, by anchoring or overlap connection joint, of reinforcing bars (rebars) in existing structures made of normal weight concrete, using the injection mortar "SPIT VIPER XTREM" or "SPIT VIPER XTREM TR" in accordance with the regulations for reinforced concrete construction.

Ribbed reinforcing bars made of steel with a diameter ϕ from 8 to 32 mm according to Annex A and the injection mortar "SPIT VIPER XTREM" or "SPIT VIPER XTREM TR" are used for rebar connections. The rebar is placed into a drilled hole filled with injection mortar and is anchored via the bond between rebar, injection mortar and concrete.

The product description is given in Annex A.

2 Specification of the intended use in accordance with the applicable European assessment Document

The performances given in Section 3 are only valid if the anchor is used in compliance with the specifications and conditions given in Annex B.

The verifications and assessment methods on which this European Technical Assessment is based lead to the assumption of a working life of the rebar connections of at least 50 and/or 100 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

3 Performance of the product and references to the methods used for its assessment

3.1 Mechanical resistance and stability (BWR 1)

Essential characteristic	Performance
Characteristic resistance under static and quasi-static loading	See Annex C 1 to C3
Characteristic resistance under seismic loading	No performance assessed

3.2 Safety in case of fire (BWR 2)

Essential characteristic	Performance
Reaction to fire	Class A1
Resistance to fire	See Annex C 4

4 Assessment and verification of constancy of performance (AVCP) system applied, with reference to its legal base

In accordance with European Assessment Document EAD No. 330087-01-0601, the applicable European legal act is: [96/582/EC].

The system to be applied is: 1



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5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable European Assessment Document

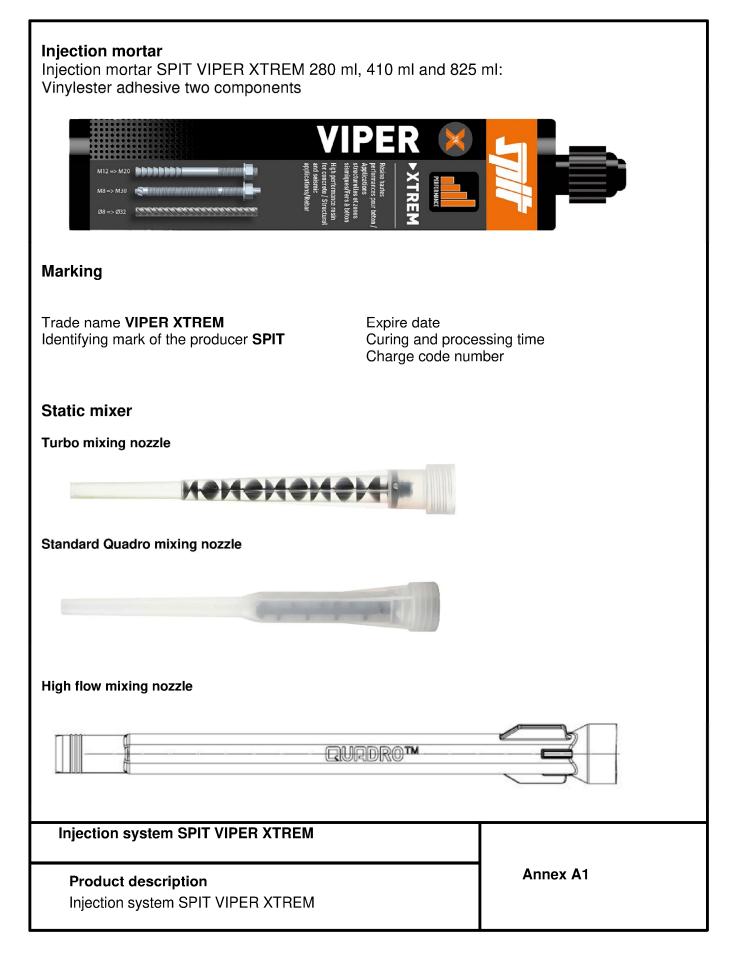
Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited with Deutsches Institut für Bautechnik.

Issued in Berlin on 5 February 2021 by Deutsches Institut für Bautechnik

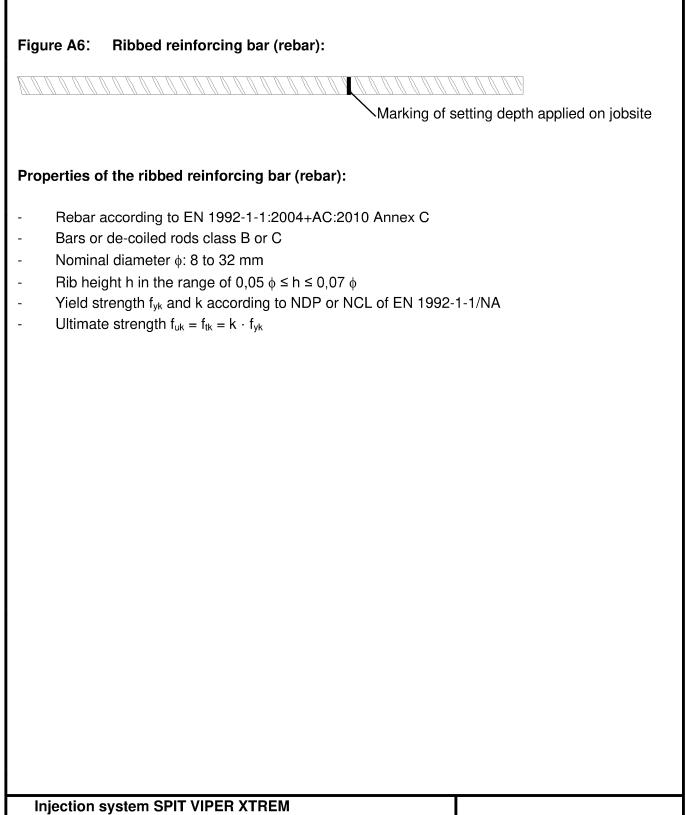
Dipl.-Ing. Beatrix Wittstock Head of Section *beglaubigt:* Baderschneider Page 5 of European Technical Assessment ETA-17/0513 of 5 February 2021

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Product description Specification rebar

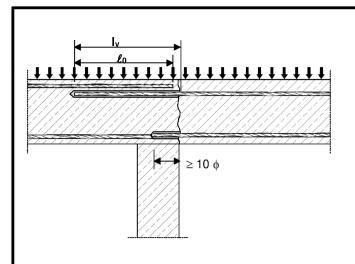
Annex A2

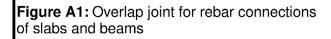
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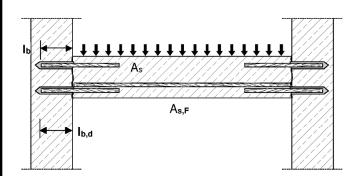


Figure A3: End anchoring of slabs or beams, designed as simply supported

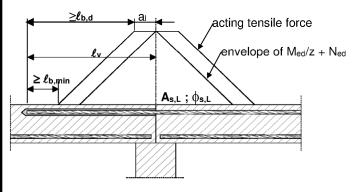


Figure A5: Anchoring of reinforcement to cover the line of acting tensile force

Injection system SPIT VIPER XTREM

Product description Specification rebar

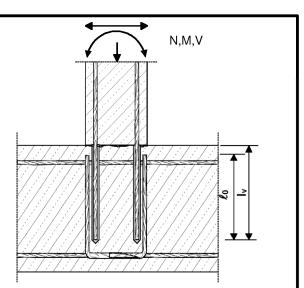


Figure A2: Overlap joint at a foundation of a column or wall where the rebars are stressed in tension

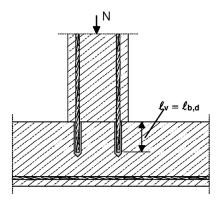


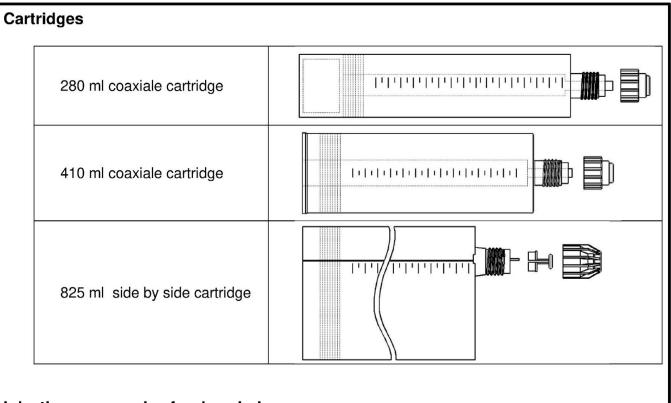
Figure A4: Rebar connection for components stressed primarily in compression. The rebars are stressed in compression

Note to Figure A1 to A5:

- In the Figures no transverse reinforcement is plotted, the transverse reinforcement as required by EN 1992-1-1:2004+AC:2010 shall be present.
- Preparing of joints according to Annex B2

Annex A3





Injection accessories for deep hole



Plastic extension must be use for hole deeper $h_0 > 250 \text{ mm}$ Piston plug for hole deeper must be use for hole deeper $h_0 > 350 \text{ mm}$

Cartridge volume	Mixing Nozzle	Extension for piston plug	Piston plug
All cartridges	Turbo or Standard Quadro	Ø13x1000	
Cartridge 825 ml	High flow	Ø20×1000	

Injection system SPIT VIPER XTREM

Product description

Cartridges

Injection accessories for deep hole

Annex A4



Specifications of intended use

Anchorages subject to:

- Static and quasi static loading
- Fire exposure.

Base material:

- Compacted Reinforced or unreinforced normal weight concrete without fibres of strength classes C 20/25 to C50/60 according to EN 206:2013+A1:2016
- Maximum chloride content of 0,40 % (CL 0.40) related to the cement content according to
- EN 206:2013+A1:2016
- Non-carbonated concrete

Note: In case of a carbonated surface of the existing concrete structure the carbonated layer shall be removed in the area of the post-installed rebar connection with a diameter of ϕ + 60 mm prior to the installation of the new rebar. The depth of concrete to be removed shall correspond to at least the minimum concrete cover in accordance with EN 1992-1-1:2004+AC:2010.The foregoing may be neglected if building components are new and not carbonated and if building components are in dry conditions.

Temperature range:

- 40°C to +80°C: max short term temperature +80°C, max long term temperature +50°C

<u>Design:</u>

Rebar connection must be designed in keeping with good engineering practice:

• Anchorages are designed under the responsibility of an engineer experienced in anchorages and concrete work.

- Verifiable calculation notes and drawings are prepared taking account of the forces to be transmitted.
- Design under static or quasi-static loading in accordance with EN 1992-1-1:2004+AC:2010 and Annex B2

• The actual position of the reinforcement in the existing structure shall be determined on the basis of the construction documentation and taken into account when designing.

Installation:

- Drilling technique:
 - Hammer drilling technique: all sizes
 - Hammer drilling with hollow drill bit XTD: sizes \$ 12-25
 - Compressed air drilling: all sizes
 - Diamond drilling technique with roughening tool: sizes ϕ 12-32
- Use category:
 - dry or wet concrete (not in flooded holes) for Hammer drilling technique, compressed air drilling and diamond drilling technique with roughening tool
 - Only dry concrete for hammer drilling with hollow drill bit XTD
 - Installation direction downwards, horizontal and overhead

• The installation of post-installed rebar resp. tension anchors shall be done only by suitable trained installer and under supervision on site; the conditions under which an installer may be considered as suitable trained and the conditions for supervision on site are up to the Member States in which the installation is done.

• Check the position of the existing rebars (if the position of existing rebars is not known, it shall be determined using a rebar detector suitable for this purpose as well as on the basis of the construction documentation and then marked on the building component for the overlap joint).

Intended Use

Specifications



Figure B1: Construction rules for post-installed rebars

- Only tension forces in the axis of the rebar may be transmitted.
- The transfer of shear forces between new concrete and existing structure shall be designed additionally according to EN 1992-1-1:2004+AC:2010.
- The joints for concreting must be roughened to at least such an extent that aggregate protrude.

		$\leq 4 \cdot \phi^*)$ $c \geq c_{\min}$
and the second second	-	<u>/////////////////////////////////////</u>
≥ 5 · φ ≥ 50 mm		8 mm ≤ φ ≤ 32
	\prec	ANANANANANA
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	lo	C1
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*) If the clear distance between lapped bars exceeds $4.\phi$, then the lap length shall be increased by the difference between the clear bar distance and $4.\phi$

- c: concrete cover of post-installed rebar
- c1: concrete cover at end-face of existing rebar
- cmin: minimum concrete cover according to Table B1 and to EN 1992-1-1:2004+AC:2010, Section 4.4.1.2
- I₀: lap length, according to EN 1992-1-1:2004+AC:2010, Section 8.7.3
- I_v : effective embedment depth $\ge I_0 + c_1$
- d₀ nominal drill bit diameter, see Annex B3
- Minimum spacing between two post-installed bars $a=50\mbox{ mm}\geq5\varphi$

Injection system SPIT VIPER XTREM

Intended used

General construction rules for post-installed rebars



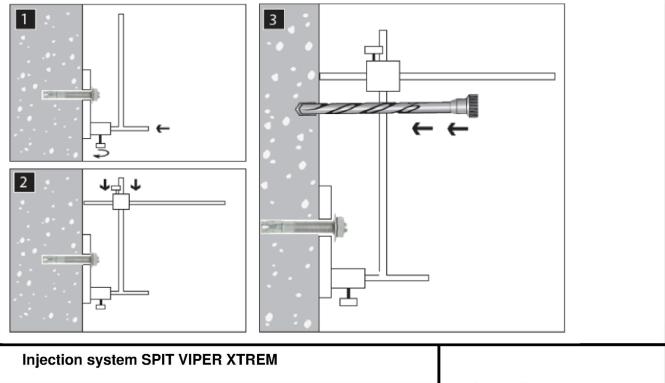
Drilling method	Bar diameter ϕ	Without drilling aid	With drilling aid	
Llommor drilling	< 25 mm	$30 + 0,06 \ I_v \! \geq \! 2\varphi$	$30+0,02\ I_v \!\geq 2\varphi$	
Hammer drilling	≥ 25 mm	$40 + 0,06 \text{ Iv} \geq 2\phi$	$40 + 0,02 \text{ I}_{\text{V}} \ge 2 \phi$	
Hammer drilling with hollow drill	< 25 mm	$30 + 0,06 \text{ lv} \ge 2\phi$	$30 + 0,02 \text{ I}_{v} \ge 2\phi$	
bit XTD	≥ 25 mm	$40 + 0,06 \ I_v \geq 2\varphi$	$40 + 0,02 \ I_v \geq 2\varphi$	
Compressed air	< 25 mm	$50 + 0,08 I_v \ge 2\phi$	50 + 0,02 $I_v \ge 2\phi$	
drilling ≥ 25 mm		$60+0,08\ I_v \!\geq \! 2\varphi$	$60+0,02~I_v \!\geq \! 2\varphi$	
Diamond core	< 25 mm	Drill stand is used	$30 + 0,02 \ I_v \! \geq \! 2\varphi$	
drilling	≥ 25 mm	as drilling aid	$40 + 0,02 \mid_v \geq 2\varphi$	

Table B1: Minimum concrete cover c_{min} ¹⁾ of post-installed rebar

1) See Annex B2, Figure B1

Note: The minimum concrete cover as specified in EN 1992-1-1:2004+AC:2010 must be observed

Figure B2: Drilling aid system



Intended used

Minimum concrete cover cmin



Rebar diameter ϕ	Maximum embedment length I _{v,max} [mm]				
	Manuel Dispenser	Pneumatic Dispenser			
[mm]	280 ml				
	410 ml	410 ml	825 ml		
	825 ml				
8					
10					
12					
16	500	600	900		
20	500	000	300		
25					
28					
32					

Table B2: Maximum embedment depth I_{v,max} depending on bar diameter and dispenser

Table B3: Installation parameters

				1	
Rebar diameter ϕ	Nominal drilling diameter d _{cut} [mm]				
[mm]	Hammer drilling	Hammer drilling with hollow drill bit XTD ¹⁾	Diamond core	Diamond core and roughening drill bit	
8	10	-	-	-	
10	12	_	-	-	
12	15	16	16	-	
16	20	20	-	20	
20	25	25	-	25	
25	30	30	-	30	
28	35	-	-	35	
32	40	-	-	40	

¹⁾ Maximum working length: 600 mm

Injection system SPIT VIPER XTREM

Intended used

Maximum embedment depth Iv_{max} Installation parameters



Table B4: Parameters for use of Roughening tool

Diamond coring	Roughening tool ¹⁾
d _{cut} [mm]	d _{cut} [mm]
20	20
25	25
30	30
35	35
40	40

¹⁾ For checking the wear of roughening drill bit, a wear gauge is delivered with each roughening tool

Table B5: Dimensions of the cleaning tools for reinforcing bars (rebars)

		Nominal diameter of the reinforcing bars (rebars)							
Dimensions	φ 8	φ 10	φ 12	φ 14	ф 16	φ 20	φ 25	φ 28	ф 32
Ø Brush [mm] ¹⁾	11	13	16	20	22	26	32	37	42
Ø Plastic extension for compress air	6	9	9	13	13	13	13/20	13/20	13/20

¹⁾ The diameter of the round steel brush shall be checked before use. The minimum brush diameter has to be at least equal to the borehole diameter d_0 . The round steel brush shall produce natural resistance as it enters the drill hole. If this is not the case, please use a new brush or a brush with a larger diameter.

Injection system SPIT VIPER XTREM

Intended used

Parameters for using of roughening drill bit

Dimensions of cleaning tools



Table B6: Gel time and curing time for Regular Version

Temperature of base material	Working time	Curing time ¹⁾
-10°C to -5°C	90 min	24 h
-4°C to 0°C	50 min	240 min
1°C to 5°C	25 min	120 min
6°C to 10°C	15 min	90 min
11°C to 20°C	7 min	60 min
21°C to 30°C	4 min	45 min
31°C to 40°C	2 min	30 min

¹⁾ For wet concrete the curing time must be doubled

Table B7: Gel time and curing time for Tropical Version:

Temperature of base material	Working time	Curing time ¹⁾
+ 5°C	60 min	240 min
6°C to 10°C	40 min	180 min
11°C to 20°C	15 min	120 min
21°C to 30°C	8 min	60 min
31°C to 40°C	4 min	60 min

¹⁾ For wet concrete the curing time must be doubled

Injection system SPIT VIPER XTREM

Product description

Minimum curing time and maximum working time

Annex B6

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Drilling the hole:	
	Rotary hammer drilling or compressed air drilling
	Electrical hammer drilling with XTD hollow drill bit used in relation with the SPIT AC 1625 vacuum or the type. This drilling technique allows for cleaning the hole from the dust debris while operating drilling. No further cleaning is then required before injecting resin.
4	Diamond core drilling The roughening tool must be used for core diameter higher than 20 mm.
Cleaning the hole:	

aning

Hammer drilling technique

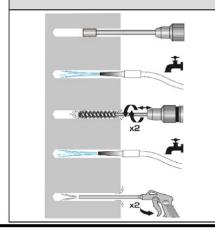
1. Using compress air cleaning (min 6 bars), use the appropriate extension, starting from the top of the hole blow out at least 2 times by moving downward to the bottom of the hole then moving upward to the top of the hole and until no dust is evacuated. (not less than 10s per each blowing).

2. Using the relevant brush and extension fitted on a Spit drilling machine, starting from the top of the hole, move downward to the bottom of the hole then move upward to the top of the hole. Repeat this operation.

3. Using compress air cleaning (min 6 bars), use the appropriate extension, starting from the top of the hole blow out at least 2 times by moving downward to the bottom of the hole then moving upward to the top of the hole and until no dust is evacuated. (not less than 10s per each blowing).

Hammer drilling technique

Electrical hammer drilling with XTD hollow drill bit used in relation with the SPIT AC 1625 vacuum or the type. This drilling technique allows for cleaning the hole from the dust debris while operating drilling. No further cleaning is then required before injecting resin.



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Diamond core drilling technique

1. For core diameter higher than 20 mm, remove water in the hole and use the roughening drill bit before applying cleaning procedure

2. Clean the hole with tap water.

3. Using the relevant brush and extension fitted on a Spit drilling machine, starting from the top of the hole, move downward to the bottom of the hole then move upward to the top of the hole. Repeat this operation.

4. Clean the hole with tap water

5. Using compress air cleaning (mini 6 bars), use the appropriate extension, starting from the top of the hole blow out at least 2 times by moving downward to the bottom of the hole then moving upward to the top of the hole and until no dust is evacuated. (not less than 10s per each blowing).

Injection system SPIT VIPER XTREM

Product description

Installation instruction

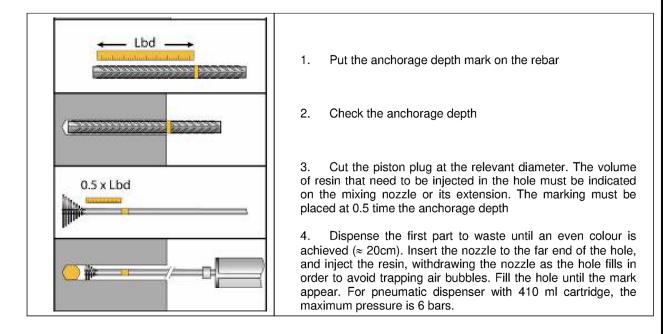


Safety precaution:

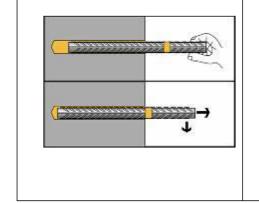
The safety data sheet must be read before using the product and the safety instructions followed.

- Storage temperature of cartridge +0°C to +35 °C
- Cartridge temperature at time of installation: Must be ≥ +5°C
- Base material temperature at time of installation: Must be between -10°C and +40°C
- Check the date of expiry of the cartridge

Dispensing into the hole:



Inserting the rebar:



1. Immediately insert the rebar, slowly and with a slight twisting motion. Remove excess resin from around the mouth of the hole before it sets. Control the embedment depth during the working time (See Annex B6 Table B6 or B7) which varies according to temperature of base material.

2. Leave the rebar undisturbed until the curing time has elapse. (See Annex B6 Table B6 or B7)

Injection system SPIT VIPER XTREM

Product description

Installation instruction



Minimum anchorage length and minimum lap length

The minimum anchorage length $I_{b,min}$ and the minimum lap length $I_{0,min}$ according to EN 1992-1-1:2004+AC:2010 shall be multiplied by the relevant amplification factor $\alpha_{Ib}=\alpha_{Ib,100y}$ given in Table C1.

Table C1:Amplification factor $\alpha_{lb} = \alpha_{lb,100y}$ related to concrete strength class for Hammer drilling and
compressed air drilling with a working life of 50 or 100 years

Rebar			Am	plificatio	n factor o	<i>ι</i> ιь = αιь,100	ру [-]				
diameter	Concrete strength class										
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60		
¢ 8				1,0							
φ10				1,0							
φ12		1,0									
φ14				1,0				1	,1		
φ16				1,0				1,1			
φ20				1,0			1,1	1,2	1,2		
φ 2 5		1	,0		1	,1	1,2	1,3	1,3		
φ28		1,	,0		1	,1	1,2	1,3	1,4		
φ32		1,	,0		1	,2	1,3	1,4	1,5		

Table C2:Bond efficiency factor $k_b = k_{b,100y}$ for Hammer drilling and compressed air drilling with a
working life of 50 or 100 years.

Rebar			Bon	d efficier	ncy factor	$\mathbf{K}_{b} = \mathbf{K}_{b,10}$	00y [-]		
diameter		Concrete strength class							
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
ф8- ф32	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0

Table C3: Design values of the bond strength fbd,PIR = fbd,PIR,100y in N/mm²

for Hammer drilling and compressed air drilling with a working life of 50 or 100 years $f_{bd,PIR} = k_b \cdot f_{bd}$

 $\mathbf{f}_{bd,PIR,100y} = \mathbf{k}_{b,100y} \cdot \mathbf{f}_{bd}$

fbd: Design value of the bond strength in N/mm² considering the concrete strength classes and the rebar diameter for good bond condition (for all other bond conditions multiply the values by $\eta_1 = 0,7$) and recommended partial factor $\gamma_c = 1,5$ according to EN 1992-1-1:2004+AC:2010

 k_b and $k_{b,100y}$: Bond efficiency factor according to Table C2

		Bond strength fbd,PIR = fbd,PIR,100y [N/mm ²]							
Rebar				Concre	te strengt	h class			
diameter	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
ф8- ф32	1,6	2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3

Injection system SPIT VIPER XTREM

Performance

Minimum anchor length and minimum lap length, amplification factor, bond efficiency factor and design value of bond strength

Annex C1



Minimum anchorage length and minimum lap length

The minimum anchorage length $I_{b,min}$ and the minimum lap length $I_{0,min}$ according to EN 1992-1-1:2004+AC:2010 shall be multiplied by the relevant amplification factor α_{lb} given in Table C4.

Table C4: Amplification factor α_{lb} for Hammer drilling with XTD hollow drill bit with a working life of 50 years

Rebar				Amplifica	ation fac	tor α _{ιь} [-]]		
diameter					te strengt				
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
φ12-φ25					1,5				

Table C5: Bond efficiency value k_b for Hammer drilling with XTD hollow drill bit with a working life of 50 years

Rebar			В	ond effi	ciency fa	actor k _b [-]		
diameter		Concrete strength class							
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
φ12-φ25	1,0								

Table C6: Design values of the bond stregth $f_{bd,PIR}$ in N/mm² for Hammer drilling
with XTD hollow drill bit with a working life of 50 years
 $f_{bd,PIR} = k_b \cdot f_{bd}$

		Bond strength f _{bd,PIR} [N/mm ²]							
Rebar				Concre	te streng	th class			
diameter	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
φ12-φ25	1,6	2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3

Injection system SPIT VIPER XTREM

Performance

Minimum anchor length and minimum lap length, amplification factor, bond efficiency factor and design value of bond strength

Annex C2



Minimum anchorage length and minimum lap length

The minimum anchorage length $I_{b,min}$ and the minimum lap length $I_{0,min}$ according to EN 1992-1-1:2004+AC:2010 shall be multiplied by the relevant amplification factor α_{lb} given in Table C7.

Table C7: Amplification factor α_{lb} for Diamond drilling with a working life of 50 years

Rebar				Amplific	ation fac	tor αιь [-]			
diameter				Concre	te strengt	h class			
andmeter	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
φ12		•		•					
φ14								4 4	1,2
φ16								1,1	
φ20				1,0					1,1
φ25									1,1
φ28								1,0	10
φ32									1,0

Table C8: Bond efficiency value k_b for Diamond drilling with a working life of 50 years

Rebar		Bond efficiency factor k _b [-]									
diameter	Concrete strength class										
diameter	C12/15	C12/15 C16/20 C20/25 C25/30 C30/37 C35/45 C40/50 C45/55 C50/60									
φ12-φ20		1,0									
φ25				1	,0				0,9		
φ 2 8		1,0 0,9						0,9			
φ 3 2	1,0 0,9 0,8 0,9							0,9			

Table C9: Design values of the bond strength $f_{bd,PIR}$ in N/mm² for Diamond drilling With a working life of 50 years $f_{bd,PIR} = k_b \cdot f_{bd}$

- f_{bd} : Design value of the bond strength in N/mm² considering the concrete strength classes and the rebar diameter for good bond condition (for all other bond conditions multiply the values by $\eta_1 = 0,7$) and recommended partial factor $\gamma_c = 1,5$ according to EN 1992-1-1:2004+AC:2010
- k_b: Bond efficiency factor according to Table C8.

		Bond strength fbd,PIR [N/mm ²]							
Rebar				Concre	te strengt	h class	1		
diameter	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
φ12-φ20			2,3					4,0	4,3
φ 2 5	16	2,0		2,7	3,0	3,4	3,7		4,0
ф28	1,6							3,7	4,0
ф 32							3,4	3,4	3,7

Injection system SPIT VIPER XTREM

Performance

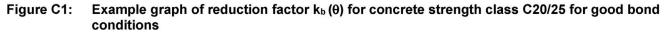
Minimum anchor length and minimum lap length, amplification factor, bond efficiency factor and design value of bond strength

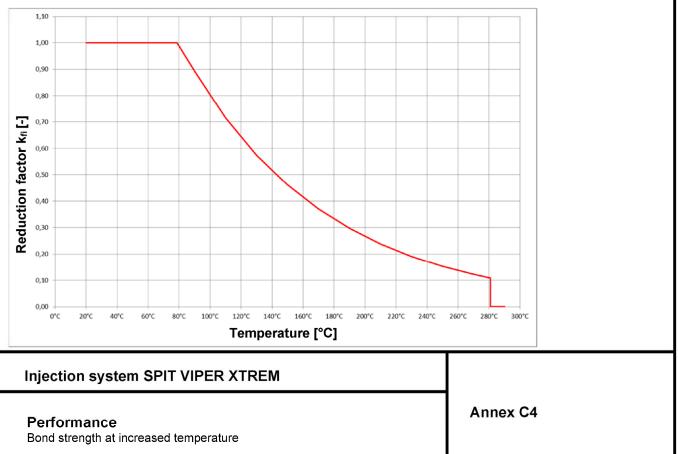
Annex C3



Bond strength	n f _{bk,fi} = f _{bk,fi,100y} at increased temperature for concrete strength classes C12/15 to C50/60
The bond stren	ngth $f_{bk,fi} = f_{bk,fi,100y}$ at increased temperature has to be calculated by the following equation:
f _{bk,fi} = f _{bl}	$k_{\rm fi,100y} = k_{\rm fi}(\theta) \bullet f_{\rm bd,PIR} \bullet \gamma_{\rm c} / \gamma_{\rm M,fi}$
where	
θ < 281 °C:	k _{fi} (θ) = min {1,0; 23,755 e ^{-0,011 • θ} /(f _{bd,PIR} • 4,3)}
θ > 281 °C:	$k_{fi}(\theta) = 0$
f _{bk,fi}	Bond strength at increased temperature in N/mm² for a working life of 50 years (all drilling methods)
f _{bk,fi,100y}	Bond strength at increased temperature in N/mm² for a working life of 100 years (Hammer and compressed air drilling)
(θ)	Temperature in °C in the mortar layer
$k_{fi}(\theta) =$	Reduction factor at increased temperature
k fi,100y (θ)	
f _{bd,PIR}	Design values of the bonds strength in N/mm ² according to Tables C3, C6 and C9 considering the concrete classes, the rebar diameter, the drilling method and the bond condition according to EN 1992-1-1:2004+AC:2010
γс	Partial factor according to EN 1992-1-1:2004+AC:2010
γM,fi	Partial factor according to EN 1992-1-2:2004+AC:2010

For evidence at increased temperature the anchorage length shall be calculated according to EN 1992-1-1:204+AC:2010, Equation 8.3 using the temperature-dependent bond strength $f_{bk,fi}$.





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