



Approval body for construction products and types of construction

Bautechnisches Prüfamt

An institution established by the Federal and Laender Governments



European Technical Assessment

ETA-21/0955 of 26 November 2021

English translation prepared by DIBt - Original version in German language

General Part

Technical Assessment Body issuing the European Technical Assessment:

Trade name of the construction product

Product family to which the construction product belongs

Manufacturer

Manufacturing plant

This European Technical Assessment contains

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of

Deutsches Institut für Bautechnik

TILCA® TIM P-E Injection System for rebar connection

Systems for post-installed rebar connections with mortar

EFCO Befestigungstechnik AG Grabenstraße 1 8606 NÄNIKON SCHWEIZ

EFCO Befestigungstechnik AG, Plant 2

24 pages including 3 annexes which form an integral part of this assessment

EAD 330087-01-0601, Edition 06/2021



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Specific Part

1 Technical description of the product

The subject of this European Technical Assessment is the post-installed connection, by anchoring or overlap connection joint, of reinforcing bars (rebars) in existing structures made of normal weight concrete, using the "TILCA® TIM P-E Injection system for rebar connection" in accordance with the regulations for reinforced concrete construction.

Reinforcing bars made of steel with a diameter ϕ from 8 to 40 mm or the tension anchor ZA of sizes M12 to M24 according to Annex A and injection mortar TILCA TIM P-E are used for rebar connections. The rebar is placed into a drilled hole filled with injection mortar and is anchored via the bond between rebar, injection mortar and concrete.

The product description is given in Annex A.

2 Specification of the intended use in accordance with the applicable European assessment Document

The performances given in Section 3 are only valid if the anchor is used in compliance with the specifications and conditions given in Annex B.

The verifications and assessment methods on which this European Technical Assessment is based lead to the assumption of a working life of the rebar connections of at least 50 and/or 100 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

3 Performance of the product and references to the methods used for its assessment

3.1 Mechanical resistance and stability (BWR 1)

Essential characteristic	Performance
Characteristic resistance under static and quasi-static loading	See Annex C 1
Characteristic resistance under seismic loading	See Annex B 4 and C 2

3.2 Safety in case of fire (BWR 2)

Essential characteristic	Performance
Reaction to fire	Class A1
Resistance to fire	See Annex C 3 to C 4

4 Assessment and verification of constancy of performance (AVCP) system applied, with reference to its legal base

In accordance with European Assessment Document EAD No. 330087-01-0601, the applicable European legal act is: [96/582/EC].

The system to be applied is: 1





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5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable European Assessment Document

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited with Deutsches Institut für Bautechnik.

Issued in Berlin on 26 November 2021 by Deutsches Institut für Bautechnik

Dipl.-Ing. Beatrix Wittstock Head of Section beglaubigt: Baderschneider



Installation post installed rebar

Figure A1: Overlapping joint for rebar connections of slabs and beams

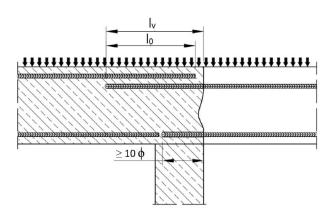


Figure A2: Overlapping joint at a foundation of a wall or column where the rebars are stressed in tension

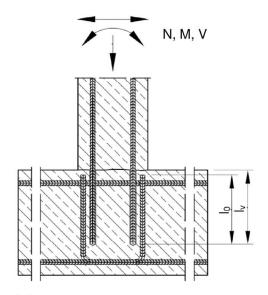


Figure A3: End anchoring of slabs or beams (e.g. designed as simply supported)

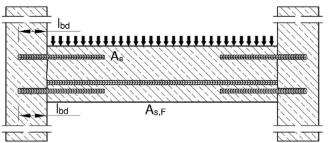


Figure A4: Rebar connection for components stressed primarily in compression. The rebars are stressed in compression

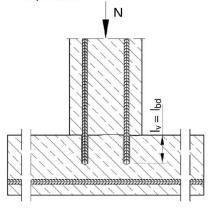
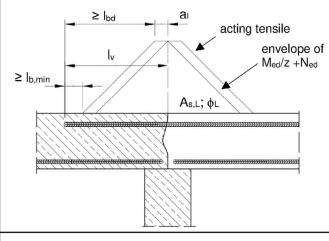


Figure A5: Anchoring of reinforcement to cover the line of acting tensile force



Note to Figure A1 to A5:

In the Figures no transverse reinforcement is plotted, the transverse reinforcement shall comply with EN 1992-1-1:2004+AC:2010.

Preparing of joints according to Annex B 2

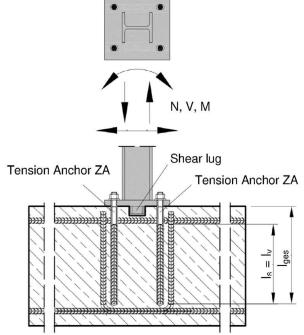
TILCA® TIM P-E Injection System for rebar connection

Product description

Installed condition and examples of use for rebars

Annex A 1

Figure A6: Overlapping joint of a column stressed in bending to a foundation Figure A7: Overlap joint for the anchorage of barrier posts



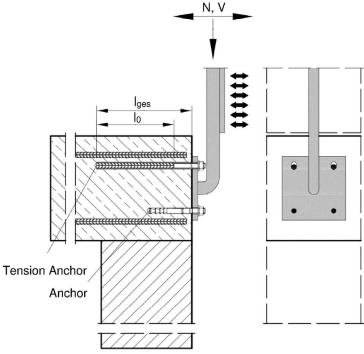
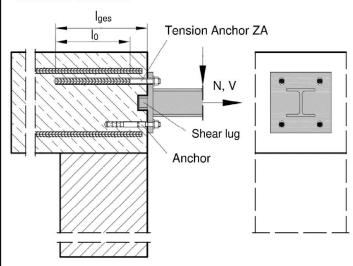


Figure A8: Overlap joint for the anchorage to centilever members



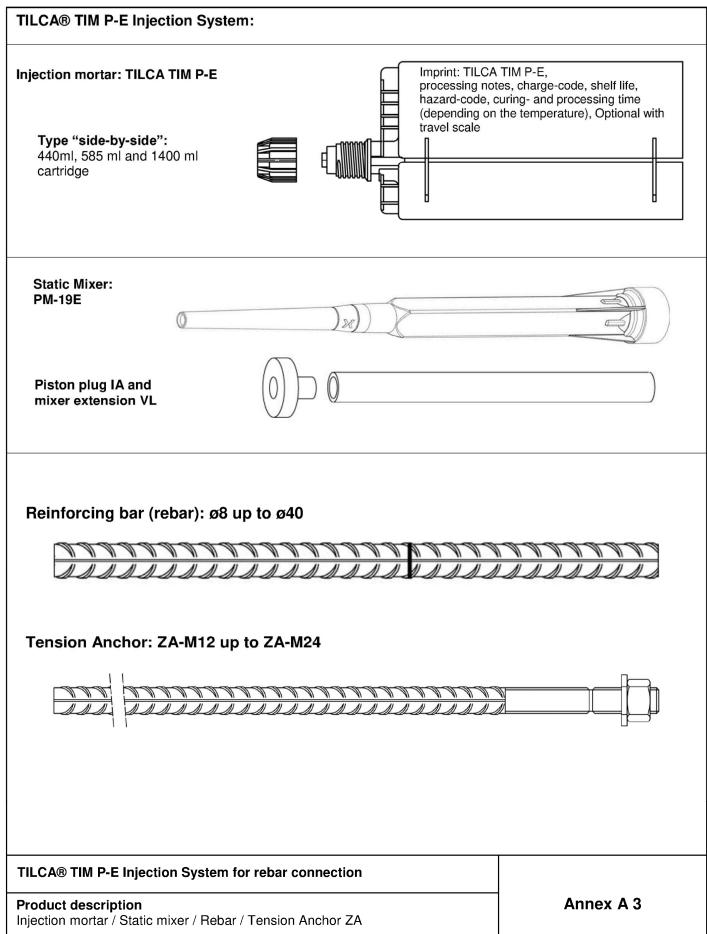
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Note to Figure A6 to A8:

In the Figures no transverse reinforcement is plotted, the transverse reinforcement shall comply with EN 1992-1-1:2002+AC:2010

TILCA® TIM P-E Injection System for rebar connection	
Product description Installed condition and examples of use for tension anchors ZA	Annex A 2





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Reinforcing bar (rebar): ø8 up to ø40



- Minimum value of related rip area f_{R,min} according to EN 1992-1-1:2004+AC:2010
- Rib height of the bar shall be in the range 0,05φ ≤ h_{rib} ≤ 0,07φ
 (φ: Nominal diameter of the bar; h_{rib}: Rib height of the bar)

Table A1: Materials

Designation	Material
Rebar EN 1992-1-1:2004+AC:2010, Annex C	Bars and de-coiled rods class B or C f_{yk} and k according to NDP or NCL of EN 1992-1-1/NA $f_{uk} = f_{tk} = k \cdot f_{yk}$

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TILCA® TIM P-E Injection System for rebar connection	
Product description Materials Rebar	Annex A 4



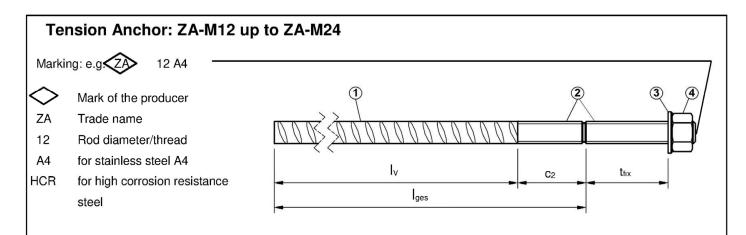


Table A2: Materials

			Material										
Part	Designation ZA vz				ZA A4					ZA HCR			
		M12	M16	M20	M24	M12	M16	M20	M24	M12	M16	M20	M24
1	Reinforcement bar		Class B according to NDP or NCL of EN 1992-1-1/NA						•				
'	f _{yk} [N/mm²]	500				500			500				
2	Threaded rod	Steel, zinc plated according to EN ISO 683-4:2018 or EN 10263:2001				1.4401	ss stee , 1.4404 088-1:20	í, 1.457		steel, 1		resista 1.4565, 014	nt
3	Washer	Steel, zinc plated according			Stainless steel, 1.4362,		High corrosion resistant						
4	Nut	to EN ISO 683-4:2018 or EN 10263:2001				, 1.4404 088-1:20		1,	· ·	1.4529, 088-1:2	1.4565, 014		

Table A3: Dimensions and installation parameter

Size				ZA-M12	ZA-M16	ZA-M20	ZA-M24	
Diameter of thread	led rod	ds	[mm]	12	12 16 20 24			
Diameter of reinfor	cement bar	ф	[mm]	12 16 20 2				
Drill hole diameter		d₀	[mm]	16	16 20 25 32			
Diameter of cleara	nce hole in fixture	df	[mm]	14	14 18 22 26			
With across nut fla	ts	SW	[mm]	19 24 30 36				
Stress area		As	[mm²]	84 157 245 353				
Effective embedme	ent depth	l _v	[mm]	according to static calculation				
Length of bonded	plated		[mm]	≥ 20	≥ 20	≥ 20	≥ 20	
thread	A4/HCR	C 2	[mm]	≥ 100	≥ 100	≥ 100	≥ 100	
Minimum thickness	s of fixture	t _{fix}	[mm]	5	5	5	5	
Maximum thickness of fixture t _{fix} [mm]		3000	3000	3000	3000			
Maximum installati	on torque	T _{max}	[Nm]	50 100 150 15			150	

TILCA® TIM P-E Injection System for rebar connection	
Product description Specifications Tension Anchor ZA	Annex A 5



Specifications of intended use					
Anchorages subject to: static and quasi-static loads seismic actions.					
Hammer drilling (HD),	for a working life of 50 years	Ø8 to Ø40 ZA-M12 bis ZA-M24	Ø10 to Ø40		
Hammer drilling with hollow drill bit (HDB), Compressed air drilling (CD),	for a working life of 100 years	Ø8 to Ø40 ZA-M12 bis ZA-M24	Ø10 to Ø40		
Or Diamond drilling (DD)	Fire exposure	Ø8 to Ø40 ZA-M12 bis ZA-M24	No performance assessed		
Temperature Range:	- 40°C to +80°C (max long-term temperature +50 °C and max short-term temperature +80 °C)				

Base materials:

- Reinforced or unreinforced normal weight concrete according to EN 206:2013 + A1:2016.
- Strength classes C12/15 to C50/60 according to EN 206:2013 + A1:2016.
- Maximum chloride content of 0,40% (CL 0.40) related to the cement content according to EN 206:2013 + A1:2016.
- · Non-carbonated concrete.

Note: In case of a carbonated surface of the existing concrete structure the carbonated layer shall be removed in the area of the post-installed rebar connection with a diameter of ϕ + 60 mm prior to the installation of the new rebar.

The depth of concrete to be removed shall correspond to at least the minimum concrete cover in accordance with EN 1992-1-1:2004+AC:2010. The foregoing may be neglected if building components are new and not carbonated and if building components are in dry conditions.

Use conditions (Environmental conditions) with tension anchor ZA:

- Structures subject to dry internal conditions (all materials).
- For all other conditions according to EN 1993-1-4:2006+A1:2015 corresponding to corrosion resistance class:
 - Stainless steel Stahl A4 according to Annex A 4, Table A1: CRC III
 - High corrosion resistance steel HCR according to Annex A 4, Table A1: CRC V

Design:

- Anchorages are designed under the responsibility of an engineer experienced in anchorages and concrete work.
- · Verifiable calculation notes and drawings are prepared taking account of the forces to be transmitted.
- Design according to EN 1992-1-1:2004+AC:2010, EN 1992-1-2:2004+AC:2008 and Annex B 2 and B 3.
- The actual position of the reinforcement in the existing structure shall be determined on the basis of the construction documentation and taken into account when designing.

Installation:

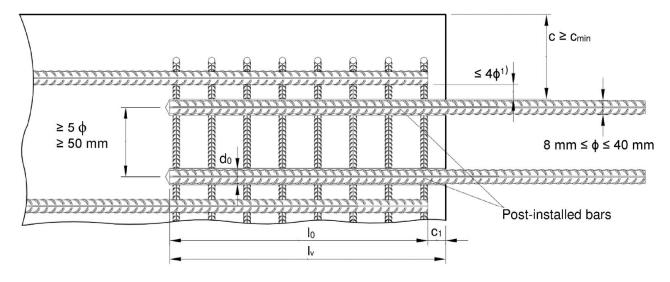
- · Dry or wet concrete. It must not be installed in flooded holes.
- · Overhead installation allowed.
- Hole drilling by hammer drill (HD), hammer drill with hollow drill bit (HDB), diamond drill (DD) or compressed air drill (CD).
- The installation of post-installed rebar resp. tension anchors shall be done only by suitable trained installer and under supervision on site; the conditions under which an installer may be considered as suitable trained and the conditions for supervision on site are up to the Member States in which the installation is done.
- Check the position of the existing rebars (if the position of existing rebars is not known, it shall be determined using a rebar detector suitable for this purpose as well as on the basis of the construction documentation and then marked on the building component for the overlap joint).

TILCA® TIM P-E Injection System for rebar connection	
Intended use Specifications	Annex B 1



Figure B1: General construction rules for post-installed rebars

- · Only tension forces in the axis of the rebar may be transmitted.
- The transfer of shear forces between new concrete and existing structure shall be designed additionally according to EN 1992-1-1:2004+AC:2010.
- The joints for concreting must be roughened to at least such an extent that aggregate protrude.



1) If the clear distance between lapped bars exceeds 4φ, then the lap length shall be increased by the difference between the clear bar distance and 4φ.

The following applies to Figure B1:

- c concrete cover of post-installed rebar
- concrete cover at end-face of existing rebar
- c_{min} minimum concrete cover according to Table B1 and to EN 1992-1-1:2004+AC:2010, Section 4.4.1.2
- φ diameter of post-installed rebar
- lo lap length, according to EN 1992-1-1:2004+AC:2010, Section 8.7.3
- l_v effective embedment depth, $\geq l_0 + c_1$
- d₀ nominal drill bit diameter, see Annex B 5

TILCA® TIM P-E Injection System for rebar connection	
Intended use General construction rules for post-installed rebars	Annex B 2

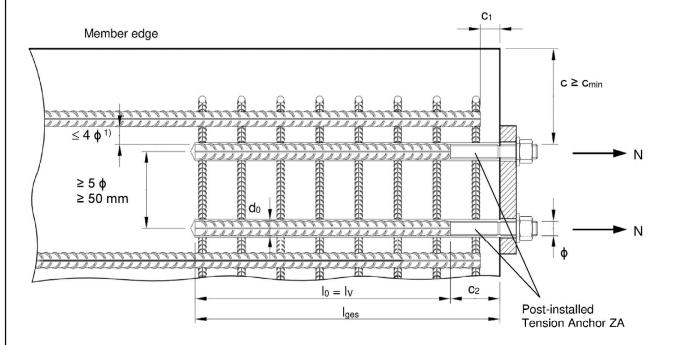
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Figure B2: General construction rules for tension anchors ZA

- The length of the bonded-in thread may be not be accounted as anchorage.
- · Only tension forces in the direction of the bar axis may be transmitted by the tension anchor ZA.
- · The tension force must be transferred via an overlap joint to the reinforcement in the building part.
- The transfer of shear forces shall be ensured by appropriate additional measures, e.g shear lugs or by anchors with an European technical assessment.
- In the anchor plate, the holes for the tension anchors shall be executed as elongated holes with axis in the direction of the shear force.



1) If the clear distance between lapped bars exceeds 4φ, then the lap length shall be increased by the difference between the clear bar distance and 4φ.

The following applies to Figure B2:

c concrete cover of tension anchor ZA

c₁ concrete cover at end-face of existing rebar

c₂ Length of bonded thread

c_{min} minimum concrete cover according to Table B1 and to EN 1992-1-1:2004+AC:2010, Section 4.4.1.2

diameter of tension anchor

l₀ lap length, according to EN 1992-1-1:2004+AC:2010, Section 8.7.3

 I_v effective embedment depth, $\geq I_0 + c_1$ I_{des} overall embedment depth, $\geq I_0 + c_2$

d₀ nominal drill bit diameter, see Annex B 4

TILCA® TIM P-E Injection System for rebar connection	
Intended use General construction rules for tension anchors	Annex B 3



Table B1: Minimum concrete cover min c1) of post-installed rebar and tie rod ZA depending of drilling method

Drilling method	Rebar diameter	Without drilling aid	With dri	lling aid
Hammer drilling (HD), Hammer drilling with	< 25 mm	30 mm + 0,06 · l _v ≥ 2 ф	30 mm + 0,02 · l _v ≥ 2 ф	Drilling aid
hollow drill (HDB)	≥ 25 mm	40 mm + 0,06 · l _v ≥ 2 ф	40 mm + 0,02 · l _v ≥ 2 φ	d manufacture Dilling aid
Diamond drilling (DD)	< 25 mm	Drill rig used as drilling	30 mm + 0,02 · l _v ≥ 2 ф	
Diamond drilling (DD)	≥ 25 mm	aid	40 mm + 0,02 · l _ν ≥ 2 φ	
Compressed air	< 25 mm	50 mm + 0,08 · l _v	50 mm + 0,02 · l _v	
drilling (CD)	≥ 25 mm	60 mm + 0,08 · l _v ≥ 2 φ	60 mm + 0,02 · l _v ≥ 2 ф	

¹⁾ see Annex B 2, Figure B1 and Annex B 3, Figure B2 Comments: The minimum concrete cover acc. EN 1992-1-1:2004+AC:2010 must be observed For minimum concrete cover in case of seismic action c_{min.seis} see Table B2.

Table B2: Minimum concrete cover min c_{min,seis}

Drilling method	Design condition	Distance of 1st edge	Distance of 2 nd edge	
Hammer drilling (HD), Hammer drilling with hollow	Edge	≥ 2 ф	≥ 2 ф	
drill (HDB), Compressed air drilling (CD)	Corner	≥ 2 ф	≥ 2 ф	
Diamond drilling (DD)	Edge	≥ 4 ф	≥8 ф	
Diamond drilling (DD)	Corner	≥ 6 ф	≥ 6 ф	

Table B3: Base material temperature, gelling time and curing time TILCA TIM P-E

Temperature in base material	Maximum Gelling- / working time ¹⁾	Initial curing time in dry concrete ²⁾	Minimum curing time in dry concrete ³⁾				
	t _{gel}	t _{cure,ini}	t _{cure}				
0 °C to + 4°C	80 min	30 h	144 h				
+ 5 °C to + 9°C	80 min	20 h	48 h				
+ 10 °C to + 14°C	60 min	15 h	28 h				
+ 15 °C to + 19°C	40 min	9 h	18 h				
+ 20 °C to + 24°C	30 min	6 h	12 h				
+ 25 °C to + 34°C	12 min	4 h	9 h				
+ 35 °C to + 39°C	8 min	3 h	6 h				
+40 °C	8 min	1,5 h	4 h				
Cartridge temperature	+5°C to +40°C						

¹⁾ t_{gel}: maximum time from starting of mortar injection to completing of rebar setting.

³⁾ In wet concrete the curing times must be doubled.

TILCA® TIM P-E Injection System for rebar connection	
Intended use Minimum concrete cover Gelling and curing time	Annex B 4

²⁾ After t_{cure,ini} has elapsed, the installation of the connecting reinforcement and the construction of the formwork can be continued



Table B4: Dispensi		nd tool	Pneumatic tool			
Cartridge type/size Side-by-side cartridges 440, 585 ml	e.g. SA 296C585					
Side-by-side cartridges 1400 ml	e.g. SA 2960363	e.g. Typ H 244 C	e.g. Typ TS 444 KX e.g. Typ TS 471			
Ale cartridges can be use	d with battery tool as well.					
Cleaning and installation tools HDB – Hollow drill bit system The hollow drill bit system contains the Heller Duster Expert hollow drill bit and a class M vacuum with minimum negative pressure of 253 hPa and flow rate of minimum 150 m³/h (42 l/s).						
The hollow drill bit system a class M vacuum with mi	contains the Heller Duster nimum negative pressure of		DOSTER EVERT			
The hollow drill bit system a class M vacuum with mi minimum 150 m³/h (42 l/s	contains the Heller Duster nimum negative pressure of	of 253 hPa <u>and</u> flow rate of SDS Plus Ad	lapter			
The hollow drill bit system a class M vacuum with mi minimum 150 m³/h (42 l/s	contains the Heller Duster nimum negative pressure of	of 253 hPa <u>and</u> flow rate of	apter			
The hollow drill bit system a class M vacuum with mi minimum 150 m³/h (42 l/s	contains the Heller Duster nimum negative pressure of	of 253 hPa <u>and</u> flow rate of SDS Plus Ad	apter			
The hollow drill bit system a class M vacuum with mi minimum 150 m³/h (42 l/s) Brush RB Brush extension RBL	contains the Heller Duster nimum negative pressure of	SDS Plus Ad	apter mpressed air tool de valve (min 6 bar)			
The hollow drill bit system a class M vacuum with mi minimum 150 m³/h (42 l/s Brush RB Brush extension RBL Piston Plug IA	contains the Heller Duster nimum negative pressure of).	SDS Plus Ad d _b Rec. com hand slice	mpressed air tool			



Table B5:	Brushes, p		-		_	-		tens	ion, har	nmer
(HD), diamond (DD) and compressed air (CD) drilling										
			_1							

	(HD), diamond (DD) and compressed an (CD) diming													
	L.		Drill				d _{b,min}		Cartridge: 440 ml or 585 ml Cartridge:			dge: 1400 ml		
Bar size	Tension anchor	bit - Ø			d Brus		min. Brush -	Brush - Piston tool Pneumatic too		· Phelimatic tool		Pne	umatic tool	
ф	ф	HD	DD	CD	Diao	~	Ø	piag	I _{v,max}	Mixer extension	$I_{v,max}$	Mixer extension	$I_{v,max}$	Mixer extension
[mm]	[mm]		[m	m]		[mm]	[mm]		[mm]		[mm]		[mm]	
8	-	1	0	-	RB10	11,5	10,5	-	250		250		250	
_ °	-	1	2	_	RB12	13,5	12,5	_	700		800		800	VL10/0,75
10	-	ı		_	NBIZ	13,5	12,0	•	250		250		250	or
	-	4	4	_	RB14	15,5	14,5	IA14	700		1000		1000	VL16/1,8
12	ZA-M12	I	4	_	ND 14	15,5	14,5	IA 14	250		250		250	
12	ZA-IVI I Z		16		RB16	RB16	16,5	IA16					1200	
14	-		18		RB18	RB18	18,5	IA18	700	VL10/0,75	1300		1400	
16	ZA-M16		20		RB20	RB20	20,5	IA20		or			1600	
20	ZA-M20	2	25	-	RB25	27,0	25,5	IA25		VL16/1,8		VL10/0,75		
20	ZA-IVIZU		-	26	RB26	28,0	26,5	IA25				or VL16/1,8		
22	-		28		RB28	RB28	28,5	IA28				VL10/1,0		
04/05	74 1404		30		RB30	RB30	30,5	IA30	500					VL16/1,8
24/25	ZA-M24		32		RB32	RB32	32,5	IA32			4000		0000	
28	-		35		RB35		35,5	IA35			1000		2000	
32/34	-		40		RB40	RB40	40,5	IA40						
36	-		45		RB45		45,5	IA45						
	-	-	52	52	RB52	54,0	52,5	IA52	_	-				
40	-	55	-	55	RB55		55,5	IA55						

Table B6: Brushes, piston plugs, max anchorage depth and mixer extension, hammer drilling with hollow drill bit system (HDB)

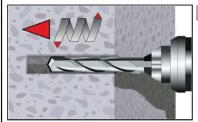
l _	L . I	Drill		d _{b,min}		Cartridge: 440 ml or 585 ml				Cartrid	ge: 1400 ml
Bar size	Tension anchor	bit - Ø	d _b min. Brush -		Piston plug	Hand or	battery tool	Pneu	matic tool	Pneu	matic tool
ф	ф	HDB	-Brush - Ø	Ø	piug	I _{v,max}	Mixer extension	$I_{v,max}$	Mixer extension	$I_{v,max}$	Mixer extension
[mm]	[mm]	[mm]				[mm]		[mm]		[mm]	
8	-	10			-	250		250		250	
	-	12			_	700		800		800	
10	-	12			_	250		250		250	
	-	14			1014	700		1000		1000	
10	74 1410	14			IA14	250		250		250	
12	ZA-M12	16	<u> </u>		IA16		\		\		
14	-	18	No clea Requ		IA18	700	VL10/0,75		VL10/0,75		VL10/0,75
16	ZA-M16	20	nequ	iieu	IA20		or VL16/1,8		or VL16/1,8		or VL16/1,8
20	ZA-M20	25			IA25		VE10/1,0		VE10/1,0		VE10/1,0
22		28			IA28			1000		1000	
04/05	74 1404	30			IA30	500					
24/25	ZA-M24	32			IA32	500					
28		35			IA35						
32/34		40			IA40						

TILCA® TIM P-E Injection System for rebar connection	
Intended use Installation tools	Annex B 6



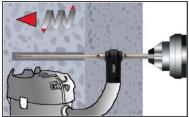
A) Bore hole drilling

Note: Before drilling, remove carbonated concrete and clean contact areas (see Annex B1) In case of aborted drill hole: the drill hole shall be filled with mortar.



Hammer (HD) or compressed air drilling (CD)

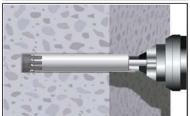
Drill a hole into the base material to the size and embedment depth required by the selected reinforcing bar. Proceed with Step B1 (MAC or CAC).



Hollow drill bit system (HDB) (see Annex B 5)

Drill a hole into the base material to the size and embedment depth required by the selected reinforcing bar. This drilling system removes the dust and cleans the bore hole during drilling.

Proceed with Step C.



Diamond drilling (DD)

1c.

Drill with diamond drill a hole into the base material to the size and embedment depth required by the selected anchor Proceed with Step B2.

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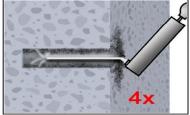
Intended use
Installation instruction: Bore hole drilling (HD, CD, HDB and DD)

Annex B 7



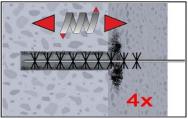
B1) Bore hole cleaning (HD and CD)

MAC: Cleaning for bore hole diameter d₀ ≤ 20mm and bore hole depth h₀ ≤ 10d_s

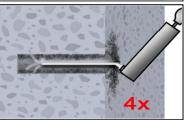




Starting from the bottom or back of the bore hole, blow the hole clean with a hand pump (Annex B 5) a minimum of four times. If the bore hole ground is not reached an extension shall be used.

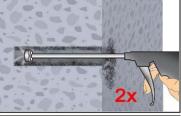


Check brush diameter (Table B5). Brush the hole with an appropriate sized wire brush > d_{b,min} (Table B5) a minimum of four times in a twisting motion. If the bore hole ground is not reached with the brush, a brush extension shall be used.



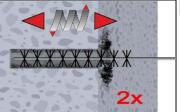
Finally blow the hole clean again with a hand pump (Annex B 5) a minimum of four times. If the bore hole ground is not reached an extension shall be used

CAC: Cleaning for all bore hole diameter and bore hole depth with drilling method HD and CD

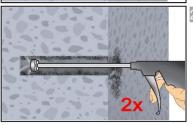


Attention! Standing water in the bore hole must be removed before cleaning.

Starting from the bottom or back of the bore hole, blow the hole clean with compressed air (min. 6 bar) (Annex B 5) a minimum of two times until return air stream is free of noticeable dust. If the bore hole ground is not reached an extension shall be used



Check brush diameter (Table B5). Brush the hole with an appropriate sized wire brush $> d_{b,min}$ (Table B5) a minimum of two times in a twisting motion. If the bore hole ground is not reached with the brush, a brush extension shall be used.



Finally blow the hole clean again with compressed air (min. 6 bar) (Annex B 5) a minimum of two times until return air stream is free of noticeable dust. If the bore hole ground is not reached an extension shall be used.

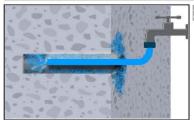
After cleaning, the bore hole has to be protected against re-contamination in an appropriate way, until dispensing the mortar in the bore hole. If necessary, the cleaning has to be repeated directly before dispensing the mortar.

TILCA® TIM P-E Injection System for rebar connection	
Intended use Installation instruction: Bore hole cleaning (HD and CD)	Annex B 8

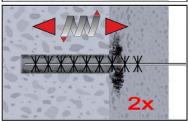


B2) Bore hole cleaning (DD)

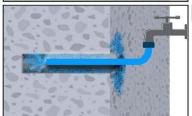
SPCAC: Cleaning for all bore hole diameter and bore hole depth with drilling method DD



2a. Rinsing with water until clear water comes out.

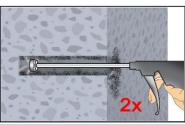


Check brush diameter (Table B5). Brush the hole with an appropriate sized wire brush $> d_{b,min}$ (Table B5) a minimum of two times in a twisting motion. If the bore hole ground is not reached with the brush, a brush extension must be used.

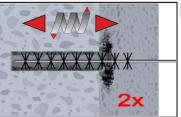


Rinsing again with water until clear water comes out.

Attention! Standing water in the bore hole must be removed before cleaning.



Starting from the bottom or back of the bore hole, blow the hole clean with compressed air (min. 6 bar) (Annex B 5) a minimum of two times until return air stream is free of noticeable dust. If the bore hole ground is not reached an extension shall be used



Check brush diameter (Table B5). Brush the hole with an appropriate sized wire brush $> d_{b,min}$ (Table B5) a minimum of two times in a twisting motion. If the bore hole ground is not reached with the brush, a brush extension shall be used.



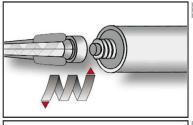
Finally blow the hole clean again with compressed air (min. 6 bar) (Annex B 5) a minimum of two times until return air stream is free of noticeable dust. If the bore hole ground is not reached an extension shall be used.

After cleaning, the bore hole has to be protected against re-contamination in an appropriate way, until dispensing the mortar in the bore hole. If necessary, the cleaning has to be repeated directly before dispensing the mortar.

TILCA® TIM P-E Injection System for rebar connection	
Intended use Installation instruction: Bore hole cleaning (DD)	Annex B 9

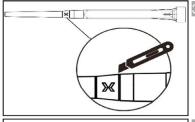


C) Preparation of bar and cartridge

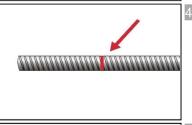


Attach the supplied static-mixing nozzle to the cartridge and load the cartridge into the correct dispensing tool.

For every working interruption longer than the recommended working time (Table B3) as well as for every new cartridges, a new static-mixer shall be used.

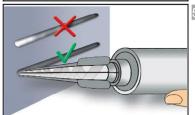


In case of using the mixer extension VL16/1,8, the tip of the mixer nozzle has to be cut off at position "X".



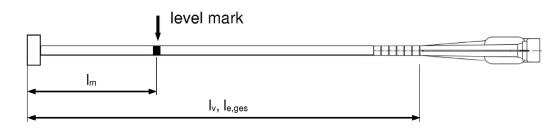
Prior to inserting the reinforcing bar into the filled bore hole, the position of the embedment depth shall be marked (e.g. with tape) on the reinforcing bar and insert bar in empty hole to verify hole and depth $I_{\rm v}$.

The reinforcing bar should be free of dirt, grease, oil or other foreign material.



Prior to dispensing into the bore hole, squeeze out separately the mortar until it shows a consistent grey or red colour, but a minimum of three full strokes, and discard non-uniformly mixed adhesive components.

D) Filling the bore hole



Injection tool must be marked by mortar level mark I_m and anchorage depth I_v resp. $I_{e,ges}$ with tape or marker.

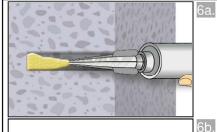
Quick estimation: $I_m = 1/3 \cdot I_v$

Continue injection until the mortar level mark I_{m} becomes visible.

Optimum mortar volume:

$$I_{m} = I_{v} \text{ resp. } I_{e,ges} \cdot \left(1,2 \cdot \frac{\phi^{2}}{d_{0}^{2}} - 0,2\right)$$

TILCA® TIM P-E Inject	ion System for rebar connection	
Intended Use		Annex B 10
Installation instruction:	Preparation of bar and cartridge Filling the bore hole	



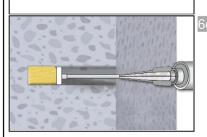
Starting from the bottom or back of the cleaned bore hole fill the hole with adhesive, until the level mark at the mixer extension is visible at the top of the hole. If the bottom or back of the anchor hole is not reached, an appropriate extension nozzle must be used. Slowly withdraw the static mixing nozzle and using a piston plugs during injection of the mortar, helps to avoid creating air pockets. Observe the gel-/ working times given in Table B3.



Piston plugs shall be used according to Table B5 or B6 for the following applications:

- For overhead and horizontal installation
- In vertical downwards direction with bore holes deeper than 250 mm

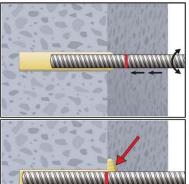
Assemble mixing nozzle, mixer extension and piston plug before injecting mortar.



Insert piston plug to back of the hole and inject adhesive. If the bottom or back of the anchor hole is not reached, an appropriate extension nozzle must be used.

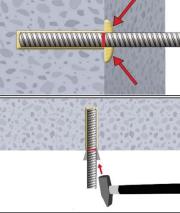
During injection the piston plug will be naturally extruded out of the drill hole by the adhesive pressure. Observe the gel-/ working times given in Table B3.

E) Setting the rebar



Push the reinforcing bar into the bore hole while turning slightly to ensure positive distribution of the adhesive until the embedment depth is reached.

The reinforcing bar should be free of dirt, grease, oil or other foreign material.



Be sure that the bar is inserted in the bore hole until the embedment mark is at the concrete surface and that excess mortar is visible at the top of the hole. If these requirements are not maintained, the application has to be renewed.

For horizontal and overhead installation fix embedded part (e.g. with wedges) until the mortar has started to harden.



Observe gelling and curing time in Table B3.

Slightly adjustment of the reinforcing bar within the gelling time t_{gel} is possible. After the time $t_{\text{cure},\text{ini}}$ has elapsed, the installation of the connecting reinforcement and the formwork can be continued. The full load to the reinforcing bar may be applied after the full curing time t_{cure} has elapsed. Attend that the gelling and curing time can vary according to the base material temperature.

TILCA® TIM P-E Injection System for rebar connection

Intended Use

Installation instruction: Inserting rebar

Annex B 11

Z113562.21

20°C

Electronic copy of the ETA by DIBt: ETA-21/0955

8.06.01-312/21



Table C1: Characteristic	tension r	esistance	for tension	anchor ZA				
Tension Anchor M12 M16 M20 M24								
Steel, zinc plated (ZA vz)								
Characteristic tension resistance	NRk,s	[kN]	67 125 196 282					
Partial factor	γ _{Ms,N}	[-]		1	,4			
Stainless Steel (ZA A4 or ZA HCR	(1)							
Characteristic tension resistance	NRk,s	[kN]	67 125 171 247					
Partial factor	γ _{Ms,N}	[-]	1	,4	1,3	1,4		

Minimum anchorage length and minimum lap length under static or quasi-static loading

The minimum anchorage length $I_{b,min}$ and the minimum lap length $I_{0,min}$ according to EN 1992-1-1:2004+AC:2010 ($I_{b,min}$ acc. to Eq. 8.6 and Eq. 8.7 and $I_{0,min}$ acc. to Eq. 8.11) shall be multiply by the amplification factor $\alpha_{lb} = \alpha_{lb,100y}$ according to Table C2.

Table C2: Amplification factor $\alpha_{lb} = \alpha_{lb,100y}$ related to concrete class and drilling method; working life 50 and 100 years

Concrete class	Drilling method	Bar size	Amplification factor αιь = αιь,100y
C12/15 to C50/60	all drilling methods	8 mm to 40 mm ZA-M12 to ZA-M24	1,0

Table C3: Reduction factor $k_b = k_{b,100y}$ for all drilling methods; working life 50 and 100 years

Rebar				Co	oncrete cla	ss			
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
8 to 40 mm ZA-M12 to ZA-M24					1,0				

Table C4: Design values of the ultimate bond stress fbd,PIR and fbd,PIR,100y in N/mm² for all drilling methods and for good conditions; working life 50 and 100 years

 $f_{bd,PIR} = k_b \cdot f_{bd}$

 $f_{bd,PIR,100v} = K_{b,100v} \cdot f_{bd}$

with

 f_{bd} : Design value of the ultimate bond stress in N/mm² considering the concrete classes, the rebar diameter, the drilling method for good bond condition (for all other bond conditions multiply the values by $\eta_1 = 0.7$) and recommended partial factor $\gamma_c = 1.5$ according to EN 1992-1-1:2004+AC:2010.

k_b, k_{b,100y}: Reduction factor according to Table C3

Rebar	Concrete class								
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
8 to 32 mm ZA-M12 to ZA-M24	1,6	2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3
34 mm	1,6	2,0	2,3	2,6	2,9	3,3	3,6	3,9	4,2
36 mm	1,5	1,9	2,2	2,6	2,9	3,3	3,6	3,8	4,1
40 mm	1,5	1,8	2,1	2,5	2,8	3,1	3,4	3,7	4,0

TILCA® TIM P-E Injection System for rebar connection	
Performances	Annex C 1
Amplification factor $\alpha_{lb} = \alpha_{lb,100y}$, Reduction factor $k_b = k_{b,100y}$,	
Design values of ultimate bond resistance fbd,PIR = fbd,PIR,100y	



Minimum anchorage length and minimum lap length under seismic action

The minimum anchorage length $l_{b,min}$ and the minimum lap length $l_{0,min}$ according to EN 1992-1-1:2004+AC:2010 ($l_{b,min}$ acc. to Eq. 8.6 and Eq. 8.7 and $l_{0,min}$ acc. to Eq. 8.11) shall be multiply by the amplification factor $\alpha_{lb,seis} = \alpha_{lb,seis,100V}$ according to Table C5.

Table C5: Amplification factor $\alpha_{lb,seis} = \alpha_{lb,seis,100y}$ related to concrete class and drilling method; working life 50 and 100 years

Concrete class	Drilling method	Bar size	Amplification factor αIb,seis = αIb,seis,100y
C16/20 to C50/60	all drilling methods	10 mm to 40 mm	1,0

Table C6: Reduction factor $k_{b,seis} = k_{b,seis,100y}$ for all drilling methods; working life 50 and 100 years

Rebar				Concre	te class				
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
10 to 40 mm	No parameter assessed				1	,0			

Table C7: Design values of the ultimate bond stress fbd,PIR,seis and fbd,PIR,seis,100y in N/mm² for all drilling methods and for good conditions; working life 50 and 100 years

fbd,PIR,seis = kb,seis · fbd

 $f_{bd,PIR,seis,100y} = k_{b,seis,100y} \cdot f_{bd}$

with

 f_{bd} : Design value of the ultimate bond stress in N/mm² considering the concrete classes, the rebar diameter, the drilling method for good bond condition (for all other bond conditions multiply the values by $\eta_1=0.7$) and recommended partial factor $\gamma_c=1.5$ according to EN 1992-1-1:2004+AC:2010.

k_{b.seis.} k_{b.seis.100v}: Reduction factor according to Table C6

Rebar	Concrete class								
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
10 to 32 mm		2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3
34 mm	No parameter	2,0	2,3	2,6	2,9	3,3	3,6	3,9	4,2
36 mm	assessed	1,9	2,2	2,6	2,9	3,3	3,6	3,8	4,1
40 mm		1,8	2,1	2,5	2,8	3,1	3,4	3,7	4,0

TILCA® TIM P-E Injection System for rebar connection	
Performances	Annex C 2
Amplification factor $\alpha_{lb,seis} = \alpha_{lb,seis,100y}$, Reduction factor $k_{b,seis} = k_{b,seis,100y}$,	
Design values of ultimate bond resistance fbd,PIR,seis = fbd,PIR,seis,100y	

Design value of the ultimate bond stress f_{bd,fi}, f_{bd,fi,100y} at increased temperature for concrete classes C12/15 to C50/60, (all drilling methods); working life 50 and 100 years:

The design value of the bond stress fbd,fi at increased temperature has to be calculated by the following equation:

For working life 50 years: $\mathbf{f}_{bd,fi} = \mathbf{k}_{fi}(\theta) \cdot \mathbf{f}_{bd,PIR} \cdot \gamma_c / \gamma_{M,fi}$

with: $\theta \le 278^{\circ}\text{C}$: $k_{fi}(\theta) = 4673, 8 \cdot \theta^{-1,598} / (f_{bd,PIR} \cdot 4,3) \le 1,0$

 $\theta > 278$ °C: $k_{fi}(\theta) = 0$

For working life 100 years: $f_{bd,fi,100y} = k_{fi,100y}(\theta) \cdot f_{bd,PIR,100y} \cdot \gamma_c / \gamma_{M,fi}$

with: $\theta \le 278^{\circ}\text{C}$: $k_{fi,100y}(\theta) = 4673.8 \cdot \theta^{-1,598} / (f_{bd,PIR,100y} \cdot 4.3) \le 1.0$

 $\theta > 278^{\circ}C$: $k_{fi,100y}(\theta) = 0$

fbd,fi, fbd,fi,100y

Design value of the ultimate bond stress at increased temperature in N/mm²

 $\begin{array}{ll} \theta & \text{Temperature in °C in the mortar layer.} \\ k_{fi}(\theta), \, k_{fi,100y}(\theta) & \text{Reduction factor at increased temperature.} \end{array}$

fbd,PIR, fbd,PIR,100y Design value of the bond stress fbd,PIR = fbd,PIR,100y in N/mm² in cold condition according to

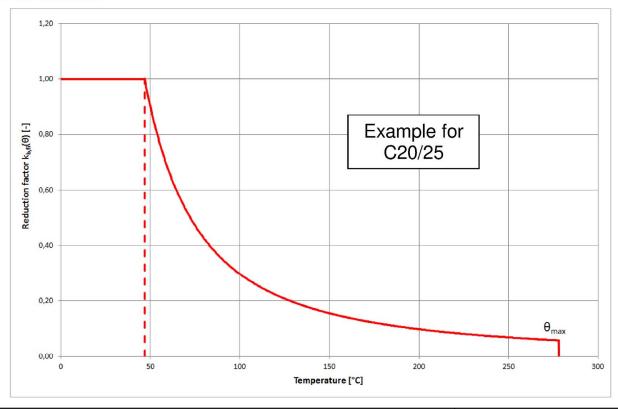
Table C4 considering the concrete classes, the rebar diameter, the drilling method and the bond

conditions according to EN 1992-1-1:2004+AC:2010.

 γ_c = 1,5, recommended partially safety factor according to EN 1992-1-1:2004+AC:2010 $\gamma_{M,fi}$ = 1,0, recommended partially safety factor according to EN 1992-1-2:2004+AC:2008

For evidence at increased temperature the anchorage length shall be calculated according to EN 1992-1-1:2004+AC:2010 Equation 8.3 using the temperature-dependent design value of ultimate bond stress f_{bd fi}.

Example graph of Reduction factor $k_{fi}(\theta)$, $k_{fi,100y}(\theta)$ for concrete classes C20/25 for good bond conditions:



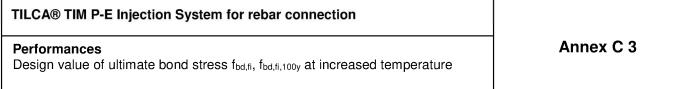




Table C8: Characteristic tension resistance for tension anchor ZA under fire exposure,

concrete classes	C12/15 to	C50/60,	according	to EN	1992-4:2018

Tension Anchor				M12	M16	M20	M24		
Steel, zinc plated	(ZA vz)								
	R30		-	2,3	4,0	6,3	9,0		
Characteristic	R60	N.		1,7	3,0	4,7	6,8		
tension resistance	R90	$N_{\scriptscriptstyleRk,s,fi}$	[kN]	1,5	2,6	4,1	5,9		
	R120			1,1	2,0	3,1	4,5		
Stainless Steel (2	'A A4 or Z	A HCR)							
	R30			3,4	6,0	9,4	13,6		
Characteristic	R60	N	[LANI]	2,8	5,0	7,9	11,3		
tension resistance	R90	$N_{Rk,s,fi}$	IN _{Rk,s,fi}	$N_{Rk,s,fi}$ [kN]	[KIN]	2,3	4,0	6,3	9,0
	R120			1,8	3,2	5,0	7,2		

TILCA® TIM P-E Injection System for rebar connection	
Performances Characteristic tension resistance for tension anchor under fire exposure	Annex C 4